MUNICIPAL SOLID WASTE PERMIT MAJOR AMENDMENT

PART III-ATTACHMENT C FACILITY SURFACE WATER DRAINAGE REPORT



NAME OF PROJECT: Beck Landfill MSW PERMIT APPLICATION NO.: 1848A OWNER: Nido, LTD (CN603075011) OPERATOR: Beck Landfill (RN102310968) CITY, COUNTY: Schertz, Guadalupe County Major Amendment: Revised August 2024

Prepared by:



Civil & Environmental Consultants, Inc.

Texas Registration Number F-38 1221 S MoPac Expressway Suite 350, Austin, Texas 78746 (512) 329-0006



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Civil & Environmental Consultants, Inc.

Beck Landfill – Type IV Revised (8/24) Part III, Attachment C

1.0 NARRATIVE

This facility surface water drainage report has been prepared consistent with the requirements of §330.63(c) and §§330.301 through 330.307. Attachment C-Facility Surface Water Drainage Report is organized to include the drainage analysis and design, flood control and analysis, and drainage system plans and details. The facility design complies with the requirements of §330.303(a)-(b) concerning the management of run on and runoff during peak discharge of a 25-year rainfall event, the prevention of off-site discharge of waste and feedstock materials, and the control of surface water discharge in and around the facility. Surface water drainage in and around the facility will also be controlled to minimize surface water running onto, into and off the treatment area. The following is a brief description of each of the attachments.

1.1 ATTACHMENT C1 – DRAINAGE ANALYSIS AND DESIGN

Attachment C1 is the drainage analysis and design of the facility, which includes calculations and demonstrations consistent with the requirements of §330.63(c), and §§330.301-330.307. This attachment includes a comparison of surface water runoff from the existing permitted condition to the post-development condition at each location where surface water enters or exits the facility boundary for the 25-year and 100-year, 24-hour rainfall event. The results of this comparison for the 25-year storm event are shown below and more detailed information is provided in Attachment C1. The comparison between the existing condition and the post-developed condition demonstrates that the proposed vertical expansion of the Beck Landfill will not adversely alter the existing drainage patterns. In addition, this attachment includes the drainage design for the final cover system, drainage benches, downchutes, perimeter channels, and detention ponds. The drainage design will also provide effective erosional stability to top dome surfaces and external embankment side slopes during all phases of landfill operation, closure, and post-closure care in accordance with these rules.

| Reach Summary | | Q25 (cfs) | Vol25 (ac-ft) | Vel ₂₅ (fps) | Runoff/on |
|----------------------|--------------|-----------|---------------|-------------------------|-----------|
| | existing | 322.7 | 67.2 | 2.9 | |
| Outfall North | proposed | 291.2 | 60.7 | 2.5 | runoff |
| | difference % | -10% | -10% | -1.4% | |
| | existing | 179.3 | 27.7 | 9.6 | |
| Outfall West | proposed | 112.5 | 13.9 | 9.6 | runoff |
| | difference % | -37% | -50% | 0% | |
| | existing | 209.0 | 40.2 | 5.2 | |
| Outfall South | proposed | 183.0 | 40.1 | 5.2 | runoff |
| | difference % | -13% | -0% | 0% | |
| | existing | 739.5 | 151.0 | 7.3 | |
| Outfall East | proposed | 729.5 | 147.1 | 7.3 | runoff |
| | difference % | -1% | -3% | 0% | |
| | | | | | |

1. Peak flowrates and volumes computed using HEC-HMS.

2. Velocities for Outfalls West, South, and East taken from HEC-HMS model of Cibolo Creek and represent the 25-year velocity in the creek at the discharge location.

1.2 ATTACHMENT C2 – FLOOD CONTROL ANALYSIS

Attachment C2 is the flood control analysis, which includes demonstrations consistent with the requirements of §330.63(c)(2). The flood control analysis demonstrates that the proposed expansion of the Beck Landfill will not adversely impact flooding conditions in the area. The landfill is proposed to be protected by an earthen berm, which is constructed at least three feet above the calculated water surface for the 100-year flood. The current FEMA map shows that the 100-year floodplain extends onto a portion of the landfill footprint, however, this map is based on topographic data from before the perimeter berm associated with the current landfill was completed. A Letter of Map Revision (LOMR) application has been approved by FEMA to revise the map to accurately depict the extents of the floodplain. Additional discussion related to the LOMR is included in Attachment C2.

The proposed stormwater pond for the landfill is within the 100 year floodplain and a no-rise certification has been submitted to the City of Schertz for the pond. In order to offset the loss of flow area in the floodplain from the pond berm, the area south of the new pond is proposed to be excavated to enhance flow through Cibolo Creek. Based on the modeling in the no-rise certification, there is no increase in the calculated water surface elevation of the floodplain from the pond construction, since the areas along the creek will be excavated to completely offset any effects of the new pond.

1.3 ATTACHMENT C3 – DRAINAGE SYSTEM PLANS AND DETAILS

This attachment includes the permit level site plans and details for the drainage system consistent with §330.63(c) and §§330.301-330.307.

MUNICIPAL SOLID WASTE PERMIT MAJOR AMENDMENT

PART III-ATTACHMENT C-1 FACILITY SURFACE WATER DRAINAGE REPORT



NAME OF PROJECT: Beck Landfill MSW PERMIT APPLICATION NO.: 1848A OWNER: Nido, LTD (CN603075011) OPERATOR: Beck Landfill (RN102310968) CITY, COUNTY: Schertz, Guadalupe County Major Amendment: Revised September 2023

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APPENDIX C1-A Drainage Maps and Existing/Post-development Comparison

APPENDIX C1-B Existing Condition Hydrologic Calculations

APPENDIX C1-C Post-development Hydrologic Calculations

APPENDIX C1-D Perimeter Drainage System Design

APPENDIX C1-E Final Cover Drainage Structure Design

APPENDIX C1-F Intermediate Cover Erosion and Sedimentation Control Plan

APPENDIX C1-G Intermediate Cover Erosion Control Structure Design



Revised (9/23)

1 INTRODUCTION

1.1 Purpose

30 TAC §330.63(c) and 330.301-330.307

This drainage analysis and design is prepared as part of a permit application for the expansion of the Beck Landfill and includes the demonstrations consistent with the requirements of 30 TAC Chapter §§330.63(c) and §§330.301-307. The drainage analysis and design is organized to include a narrative description of the existing and post-development conditions, the proposed drainage system design, effective erosional stability of top dome surfaces and external embankment side slopes during all phases of landfill operation, and a discussion of the existing/post-development comparison at the facility and property boundaries. Drainage calculations are included in the appendices to this section. Drainage design plans and details are included in Attachment C3. The following is a brief description of each of the appendices.

Appendix C1-A- Drainage Maps and Existing/Post-Development Comparison

Appendix C1-A includes drainage area maps that delineate the drainage areas that contribute surface water run-on and runoff at the facility and property boundaries and provide a summary of the peak flow rates, runoff volumes, and runoff velocities at locations along the facility boundary for the existing and post-development conditions. Appendix C1-A also includes a table summarizing the existing/post-development drainage analysis comparison.

Appendix C1-B- Existing Hydrologic Calculations

The existing hydrologic and hydraulic condition is the final permitted condition depicted in TCEQ MSW Permit 1848. The existing hydrologic and hydraulic evaluation is included in Appendix C1-B. The existing analysis includes delineations of drainage areas that contribute surface water runon and runoff at comparison locations along the facility boundary.

The results of the existing hydrologic evaluation are provided on the existing conditions drainage analysis summary, which shows the 25- and 100-year peak flow rates, runoff volumes, and runoff velocities at comparison locations along the proposed facility boundary.

Appendix C1-C- Post-Development Hydrologic Calculations

The post-development hydrologic and hydraulic evaluation included in Appendix C1-C represents the proposed final closure landfill configuration. The post-development analysis includes delineations of drainage areas that contribute surface water run-on and runoff at comparison points along the proposed facility boundary.

The results of the post-development hydrologic evaluation are provided on the post-development boundary analysis summary, which shows the 25- and 100-year peak flow rates, runoff volumes, and runoff velocities at the comparison locations along the proposed permit boundary.

Appendix C1-D- Perimeter Drainage System Design

Appendix C1-D presents the hydraulic design of the perimeter drainage system. The perimeter drainage plan shows the locations of the perimeter drainage berms and detention ponds. The detention ponds are designed to provide the necessary storage and outlet control to mitigate impacts to the receiving channels downstream of the Beck Landfill. The perimeter berms are designed to convey the 25-year and 100-year, 24-hour storm event.

Appendix C1-E- Final Cover Drainage Structure Design

Appendix C1-E is limited to the design of the permanent final cover drainage structures (i.e., downchute and bench system). The calculations demonstrate that the structures are designed to convey runoff produced from a 25-year storm event, to provide erosion protection, and to minimize sediment loss from the final cover condition.

Appendix C1-F - Intermediate Cover Erosion and Sedimentation Control Plan

Appendix C1-F provides a detailed erosion and sediment control plan during the intermediate cover phase of the landfill development.

Appendix C1-G- Intermediate Cover Erosion Control Structure Design

Appendix C1-G provides the supporting documentation to evaluate and design temporary erosion and sediment control structures for the intermediate cover phase of the landfill development.

2 METHODOLOGY

2.1 Concepts and Methods

30 TAC §330.305(f) and §330.307

The hydrologic and hydraulic methods employed in this study are consistent with the TCEQ regulations. The United States Army Corps of Engineers (COE) HEC-HMS computer program was used to compute peak flow rates and runoff volumes. The HEC-HMS peak flow rates, the NRCS Method, the Universal Soil Loss Equation, and the values defined in the <u>2018 NOAA Atlas</u> <u>14 Precipitation-Frequency Atlas of the United States, Volume 11, Version 2.0:Texas,</u> as required by the TxDOT Hydraulic *Design Manual,* September, 2019, were used to design the final cover drainage system and erosion control features. The drainage analysis proceeded in the following sequence:

- Maps were prepared that provided information about the surface runoff characteristics based on the existing conditions. These maps are included in Appendix C1-B.
- Surface water runoff hydrographs for the existing condition were developed using HEC-HMS. The existing HEC-HMS evaluation is included in Appendix C1-B.
- Maps were prepared that provide information about the surface water runoff characteristics of the post-developed final cover drainage conditions for the Beck Landfill. These maps are included in Appendix C1-C.
- Surface water hydrographs for the post-developed condition, including the perimeter drainage channel and detention ponds, were evaluated using HEC-HMS. The post-developed evaluation is included in Appendix C1-C.
- The final cover system was evaluated for soil loss using the Natural Resources Conservation Service (NRCS) Revised Universal Soil Loss Equation. Final cover drainage systems were evaluated for capacity using the peak flow rates from HEC-HMS, the NRCS Method, and the methods defined in the TxDOT *Hydraulic Design Manual*, October 2011. Final cover drainage systems calculations are included in Appendix C1-E.
- The intermediate cover system was evaluated for soil loss using the Revised Universal Soil Loss Equation. Intermediate cover erosion and sediment control plan and structure design were evaluated for capacity using the NRCS Method and the values defined in the <u>2018 NOAA Atlas 14 Precipitation-Frequency Atlas of the United States, Volume 11,</u> <u>Version 2.0:Texas,</u> as required by the TxDOT Hydraulic *Design Manual,* September, 2019. Intermediate and final cover erosion and sediment control plans are included in

Appendix C1-F and C1-G.

2.2 Hydrologic and Hydraulic Modeling

2.2.1 HEC-HMS

The COE HEC-HMS program was developed to simulate the surface water runoff response of a watershed. The HEC-HMS model represents a watershed as a network of hydrologic and hydraulic components. The modeling process results in the computation of stream-flow hydrographs at desired locations in the watershed. HEC-HMS v4.11 was used to perform the hydrologic modeling. Refer to Appendix C1-B for a detailed discussion of the input parameters used for the existing conditions analysis and Appendix C1-C for a detailed discussion of the input parameters used for the post-developed condition.

2.3 Hydrologic Elements Naming Convention

The following naming convention was used in the existing and post-developed hydrologic evaluations:

- DA-E existing drainage rea associated with current permit 1848 (examples: DA-E1, DA-E2)
- DA-PX existing drainage rea associated with current permit 1848 (examples: DA-P01, DA-P02)
- POND#- pond reservoir element, (examples: POND1)
- Outfall-XX comparison point where surface water runoff exits the property boundaries (examples: Outfall-N, Outfall-W)

3 EXISTING CONDITIONS

30 TAC §330.305(f) and §330.307 The Beck Landfill includes a Type IV municipal solid waste facility located in Guadalupe County, Texas within the city limits of Schertz, Texas. The Beck Landfill site entrance is located at 550 Farm to Market Road 78.

The Beck Landfill permit boundary encompasses about 257 acres. The area within the permit boundary primarily consists of the landfill footprint with the remaining being flat grasslands or the slope of the perimeter berm down toward Cibolo Creek. The property has been historically used as sand and gravel mining dating back at least to the 1970s. The property is bordered by Cibolo Creek on three sides and slopes towards the creek. The northern portion of the property generally slopes to the south toward the creek.

The facility is located on the south side of FM 78, east of Randolph Air Force base. The proposed landfill footprint is 155 acres and the entire footprint has been excavated and is partially filled with waste. No lateral expansion of the landfill is proposed in this application.

As shown on Drawing C1-1, Cibolo Creek enters the area around the site from the north and runs adjacent to the west permit boundary edge and then bends approximately 180 degrees and runs along the south and east permit boundary borders. The only offsite stormwater entering the permit boundary is via the flow in Cibolo Creek and two drainage areas south of FM 78 (OS-1 and OS-2).

Appendix C1-B includes the existing condition hydrologic calculations. Appendix C1-B includes drawings that depict the existing condition drainage areas and comparison points. Refer to Drawing C1-1 for the existing condition drainage area map, including all offsite drainage areas. Refer to drawing C1-1 also for a detailed drainage area map of the property, which includes the area, peak flow rate, and volume for the 25-year 24-hour rainfall event for each drainage area.

The following table includes a summary of the existing conditions drainage analysis, providing the peak flow rate, volume, and velocity at each comparison point for the 25-year, 24-hour rainfall event. The table also identifies the contributing drainage areas, and states that surface water either enters (run-on) or exits (runoff) at each comparison point.

| Reach Summary | | Q25 (cfs) | Vol25 (ac-ft) | Vel25 (fps) | Runoff/on |
|---------------|----------|-----------|---------------|-------------|-----------|
| Outfall North | existing | 322.7 | 67.2 | 2.9 | Runoff |
| Outfall West | existing | 179.3 | 27.7 | 9.6 | Runoff |
| Outfall-South | existing | 209.0 | 40.2 | 5.2 | Runoff |
| Outfall East | existing | 739.5 | 151.0 | 7.3 | Runoff |

1. Peak flowrates and volumes computed using HEC-HMS.

2. Velocities for Outfalls East, West, and South taken from 25-Year HEC-RAS model of Cibolo Creek, these discharge points are all inundated during this storm event.

4 **POST-DEVELOPED CONDITIONS**

30 TAC §330.305(f) and §330.307

The post-developed condition discussion relates to surface water entering and exiting the facility and property boundary, and the comparison points along the facility and property boundary identified in the existing conditions remain unchanged in the post-developed condition. The offsite drainage areas and runoff characteristics outside the Beck Landfill property boundary remain unchanged from the existing conditions. Offsite drainage areas and runoff characteristics that are located within the permit boundary and outside the landfill footprint remain unchanged from existing conditions, except those that are affected by the location of the proposed pond. All drainage areas within the landfill footprint are revised to consider the landfill vertical expansion.

The total drainage area for comparison points Outfall North, Outfall West, Outfall South, and Outfall East remains unaffected by the facility development. However, these drainage areas have been sub-divided where appropriate and runoff characteristics adjusted as appropriate to evaluate the effect of the vertical expansion of the landfill.

The locations where surface water enters and exits the facility and property boundary in the postdevelopment conditions remains unchanged from existing conditions.

Appendix C1-C includes the post-developed hydrologic calculations. Appendix C1-C includes drawings that depict the post-developed drainage areas and comparison points. Refer to drawing C1-2 for the post-developed drainage area map, including all offsite drainage areas. Refer to drawing C1-2 for a detailed drainage area map of the existing property, which includes the area, peak flow rate, and volume for the 25-year and 100-year 24-hour rainfall event for each drainage area. Refer to drawing C1-2 for the post-developed runoff summary for each comparison point.

The following table includes a summary of the post-development conditions drainage analysis, which provides the peak flow rate, volume, and velocity at each comparison point for the 25-year, 24-hour rainfall event. The table also identifies the contributing drainage area, and states that surface water either enters (run-on) or exits (runoff) at each comparison point.

| Reach Summary | | Q25 (cfs) | Vol25 (ac-ft) | Vel25 (fps) | Runoff/on |
|---------------|----------|-----------|---------------|-------------|-----------|
| Outfall North | proposed | 291.2 | 60.7 | 2.5 | Runoff |
| Outfall West | proposed | 112.5 | 13.9 | 9.6 | Runoff |
| Outfall-South | proposed | 183.0 | 40.1 | 5.2 | Runoff |
| Outfall East | proposed | 729.5 | 147.1 | 7.3 | Runoff |

3. Peak flowrates and volumes computed using HEC-HMS.

4. Velocities for Outfalls East, West, and South taken from HEC-RAS model of Cibolo Creek for the 25-year storm event.

5 ANALYSIS OF EXISTING AND PROPOSED CONDITIONS

30 TAC §330.305(f) and §330.307

The tables below provide a comparison of the 25 and 100-year peak flow rates at each outfall. All of the proposed values are lower than the existing values due to the detention and retention effects of the proposed pond on the south side of the landfill.

| Reach Summary | | Q25 (cfs) | Vol25 (ac-ft) | Vel25 (fps) | Runoff/on |
|---------------|--------------|-----------|---------------|-------------|-----------|
| | existing | 322.7 | 67.2 | 2.9 | |
| Outfall North | proposed | 291.2 | 60.7 | 2.5 | runoff |
| | difference % | -10% | -10% | -1.4% | |
| | existing | 179.3 | 27.7 | 9.6 | |
| Outfall West | proposed | 112.5 | 13.9 | 9.6 | runoff |
| | difference % | -37% | -50% | 0% | |
| | existing | 209.0 | 40.2 | 5.2 | |
| Outfall South | proposed | 183.0 | 40.1 | 5.2 | runoff |
| | difference % | -13% | -0% | 0% | |
| | existing | 739.5 | 151.0 | 7.3 | |
| Outfall East | proposed | 729.5 | 147.1 | 7.3 | runoff |
| | difference % | -1% | -3% | 0% | |
| | | | | | |

1. Peak flowrates and volumes computed using HEC-HMS.

2. Velocities for Outfalls West, South, and East taken from 25 Year HEC-RAS model of Cibolo Creek and represent the velocity in the creek at the discharge location.

| Reach Summary | | Q100 (cfs) | Vol100 (ac-ft) | Vel100 (fps) | Runoff/on |
|---------------|---------------------|------------|----------------|--------------|-----------|
| | existing | 491.1 | 102.4 | 3.3 | |
| Outfall North | proposed | 431.4 | 90.7 | 2.8 | runoff |
| | difference % | -12% | -12% | -1.4% | |
| | existing | 281.9 | 43.6 | 12.2 | |
| Outfall West | proposed | 165.7 | 20.8 | 12.2 | runoff |
| | <i>difference %</i> | -41% | -52% | 0% | |
| | existing | 329.8 | 63.4 | 7.0 | |
| Outfall South | proposed | 267.1 | 72.7 | 7.0 | runoff |
| | difference % | -19% | 15% | 0% | |
| | existing | 1,146.8 | 234.4 | 7.3 | |
| Outfall East | proposed | 1075.8 | 232.8 | 7.3 | runoff |
| | difference % | -6% | -1% | 0% | |

100 Year Return Period

- 1. Peak flowrates and volumes computed using HEC-HMS.
- 2. Velocities for Outfalls West, South, and East taken from HEC-RAS model of Cibolo Creek and represent the velocity in the creek at the discharge location.

The proposed drainage system for the Beck Landfill will consist of drainage benches, berms, downchutes, perimeter ditches, detention ponds and outlet structures.

The facility has been designed to prevent discharge of pollutants into waters of the state or waters of the United States, as defined by the Texas Water Code and the Federal Clean Water Act, respectively. Beck Landfill will receive authorization from the TCEQ to discharge stormwater runoff consistent with Texas Pollutant Discharge Elimination System General Permit No. TXR050000 relating to stormwater discharges associated with industrial activity. Landfills are authorized under the General Permit. This stormwater permit must remain in effect throughout the active life of the facility and will contain limitations on stormwater discharge parameters.

5.1 Perimeter Drainage System Design

The perimeter drainage system is designed to convey the 25-year runoff from the developed landfill consistent with TCEQ regulations. In addition, the perimeter berms have been designed to convey the runoff from a 100-year rainfall event. The perimeter channel system design calculations are referenced in Appendix C1-D. The perimeter drainage structure plans are included in Attachment C3.

The detention pond is designed to provide the necessary storage and outlet control to mitigate impacts to the receiving channels downstream of Beck Landfill. Detention pond design parameters are included in the hydrologic modeling for post-developed conditions in Appendix C1-C. The detention pond details are shown in Attachment C3. The detention pond outlet structures are designed as energy dissipaters to reduce the velocity and turbulence of the flow leaving the detention ponds.

5.2 Final Cover Drainage Structure Design

Stormwater runoff will be collected via berms and benches located near the upper grade break on the landfill and on the 4:1 (horizontal to vertical) side slopes, leading to drainage letdown structures or downchutes and to the perimeter drainage system. The perimeter drainage system will be constructed as the landfill is developed.

The final cover drainage system benches and downchutes are designed to convey the 25-year peak flow rate. These benches, channels, and downchutes will also reduce maintenance at the site after closure by minimizing erosion. The final cover erosion control design calculations are included in Appendix C1-E. The final cover design, showing the locations of the drainage benches, downchutes, and final cover drainage structure details, is illustrated in Appendix C1-E.

The downchute/letdown structures are designed to convey the 25-year, 24-hour peak flow rate. The downchutes are designed using Maccaferri gabion mattresses, rock riprap, geomembranes, or articulating concrete blocks to minimize erosive conditions along the downchute and at bench/downchute confluences. The downchute structures convey stormwater into Cibolo Creek or directly into the detention pond. The downchute structures are designed using concrete, Maccaferri gabion mattresses, rock riprap, geomembranes, or articulating concrete blocks to provide erosion protection at the downchute/creek confluence and where downchutes convey stormwater directly into the detention pond. The downchute design calculations are included in Appendix C1-E. Final cover drainage system details, including the downchute details, are shown in Attachment C3.

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6 EROSION AND SEDIMENTATION CONTROL

30 TAC §330.305(f) and §330.307

6.1 Final Cover Stormwater System Control Plan

Perimeter drainage channels and the detention pond will be constructed as the subsequent phased development of the landfill progresses. Erosion will be minimized in these structures by establishment of vegetation or with rock riprap, gabions, or other materials as provided for in the drainage design calculations for these permanent structures as found in Appendix C1-E Final Cover Drainage Structure Design.

Berms, benches, and chutes will be constructed upon placement of the final cover. The final cover includes an erosion layer that is a minimum of 6 inches of earthen material capable of sustaining native plant life and will be seeded with native and introduced grasses immediately following the application of final cover in order to minimize erosion. A soil loss demonstration for the erosion layer is included in Appendix C1-E of this attachment. The benches and chutes include establishment of vegetation, Maccaferri gabion mattress, and other materials as provided in the drainage calculations for these permanent structures.

6.2 Final Cover Stormwater System Maintenance Plan

Beck Landfill will inspect, restore, and repair constructed permanent stormwater systems such as channels, drainage benches, chutes, and flood control structures in the event of washout or failure from extreme storm events. Excessive sediment will be removed, as needed, so that the drainage structures, such as the perimeter channels and detention pond, function as designed. Site inspections by landfill personnel will be performed weekly or within 48 hours of a rainfall event of 0.5 inches or more. The time frame for correction of damaged or deficient items under normal conditions will be within five working days after the inspection identifying these items. Normal conditions are weather, ground and other site-specific conditions that do not impede access to the item, result in additional damage to the site attempting to access or repair the item, or risk equipment or personnel safety. Documentation of the inspection will be included in the site operating record.

The following items will be evaluated during the inspections:

- Erosion of final cover areas, perimeter ditches, chutes, benches, detention pond, berms, and other drainage features
- Settlement of final cover areas, perimeter ditches, chutes, benches, and other drainage features
- Silt and sediment build-up in perimeter ditches, chutes, benches, and the detention pond
- Obstructions in drainage features

- Presence of erosion or sediment discharge at perimeter stormwater discharge locations
- Presence of sediment discharges along the site boundary in areas that have been disturbed by site activities
- Maintenance activities will be performed to correct damaged or deficient items noted during the site inspections. These activities will be performed as soon as reasonably possible after the inspection. The time frame for correction of damaged or deficient items will vary based on weather, ground conditions, and other site-specific conditions.
- Maintenance activities will consist of the following, as needed:
 - Placement of additional temporary or permanent vegetation
 - Placement, grading, and stabilization of additional soils in eroded areas or in areas that have experienced settlement
 - Replacement of Maccaferri gabion mattresses or other structural lining
 - Placement of additional Maccaferri gabion mattresses in eroded areas or in areas that have experienced settlement
 - o Removal of obstructions from drainage features
 - Removal of silt and sediment build-up from drainage features
 - Repairs to erosion and sedimentation controls
 - o Installation of additional erosion and sedimentation controls

6.3 Intermediate Cover Erosion and Sedimentation Control Plan

Erosion and sediment controls have been designed for the intermediate cover phase of landfill development. The intermediate cover erosion and sedimentation control plan includes temporary structures and establishment of vegetation to minimize erosion of the intermediate cover and documentation requirements. Refer to Appendix C1-F-Intermediate Cover Erosion and Sedimentation Control Plan, and Appendix C1-G-Intermediate Cover Erosion Control Structure Design. Details for the interim drainage and sedimentation controls are included in Appendix C-3.

6.4 **Operations Cover Erosion and Sedimentation Control Plan**

Erosion and sediment controls for the operational cover phase of landfill development will be consistent with the requirements of Part IV-Site Operating Plan, Landfill Cover. Operational cover will be placed over all solid waste at the end of each operating week as required by Part IV, Section Landfill Cover. The operational cover will be sloped to drain. Runoff from areas that have intact operational cover constructed of a well-compacted earthen material is considered uncontaminated stormwater runoff. Erosion and sediment controls for operational cover will include the following procedures:

- Areas with operational cover will be inspected daily for erosion that may cause contaminated runoff from the daily cover.
- After each rainfall event, all operational cover areas will be inspected for erosion or other damage and repaired as necessary. Runoff from damaged or eroded areas will be handled as contaminated water until repairs are completed.
- Erosion and sediment controls will be implemented within operational cover areas, including compaction of operational cover to minimize infiltration of stormwater.
- Should erosion of operational cover be observed, the operational cover will be replaced so that no solid waste is exposed at the end of the operating day. In the event that additional soil stabilization or erosion control measures are deemed necessary, one or more of the following measures will be constructed: temporary sediment control fence, silt fence, swales, or filter berms.

7 EXISTING AND POST-DEVELOPMENT COMPARISON

30 TAC §330.305(f) and §330.307

Consistent with 30 TAC §330.63(c)(1)(D)(iii) and §330.305(a), the proposed facility development will not adversely alter existing drainage patterns. Refer to Appendix C1-A for a summary of the existing conditions, post-developed conditions, and a comparison of the peak flow rate, volume, and velocity for each comparison point evaluated. Comparisons are provided for the 25-year and 100-year, 24-hour rainfall events. The comparison points established in the existing condition evaluation remain unchanged in the post-developed condition.

Drawing C1-1 - Existing Drainage Area Map: This drawing depicts the existing locations (comparison points) where surface water enters or exits the facility and property boundaries. Each comparison point is shown on the drawing and the peak flow rate, runoff volume, and runoff velocity is provided for each runoff comparison point.

Drawing C1-2 – Proposed Drainage Map: This drawing depicts the existing locations (comparison points) where surface water enters or exits the facility and property boundaries. Each comparison point is shown on the drawing and the peak flow rate, runoff volume, and runoff velocity is provided for each runoff comparison point.

A table comparing the existing condition runoff summary and the post-developed runoff summary is provided in Section 5 of this Attachment. The existing condition and post-developed peak flow rate, runoff volume, and velocity at each comparison point for both the 25- and 100-year, 24-hour rainfall event is provided. The difference, if any, between the existing and post-developed runoff results is also provided in the table.

Given that: (1) drainage from the permit boundary and/or property boundary does not significantly adversely alter the peak flow rates, velocities, or runoff volumes at the facility and property boundaries and receiving channels, and (2) the stormwater discharge outfalls are consistent with the existing site configuration, it is concluded that the proposed landfill development will not adversely alter existing drainage patterns consistent with §330.305(a).

8 CONCLUSIONS

30 TAC §330.305(f) and §330.307

The following conclusions summarize the results of the drainage analysis and design:

- The drainage design criteria and analyses used for these drainage calculations meet and exceed the requirements of 30 TAC Chapter 330.
- The final cover drainage structures (berms, benches, chutes) are designed in accordance with the rules to convey peak flow rates from the 25-year rainfall event.
- Perimeter channels are designed in accordance with the rules for the 25-year rainfall event and will also accommodate the peak flow rate from the 100-year rainfall event.
- Detention pond capacities and outlets are designed in accordance with the rules for the 25year rainfall event, will also accommodate the peak runoff from the 100-year rainfall event.
- Erosion will be minimized by using Best Management Practices.
- The proposed landfill development will not significantly adversely alter existing drainage patterns at the facility and property boundaries.

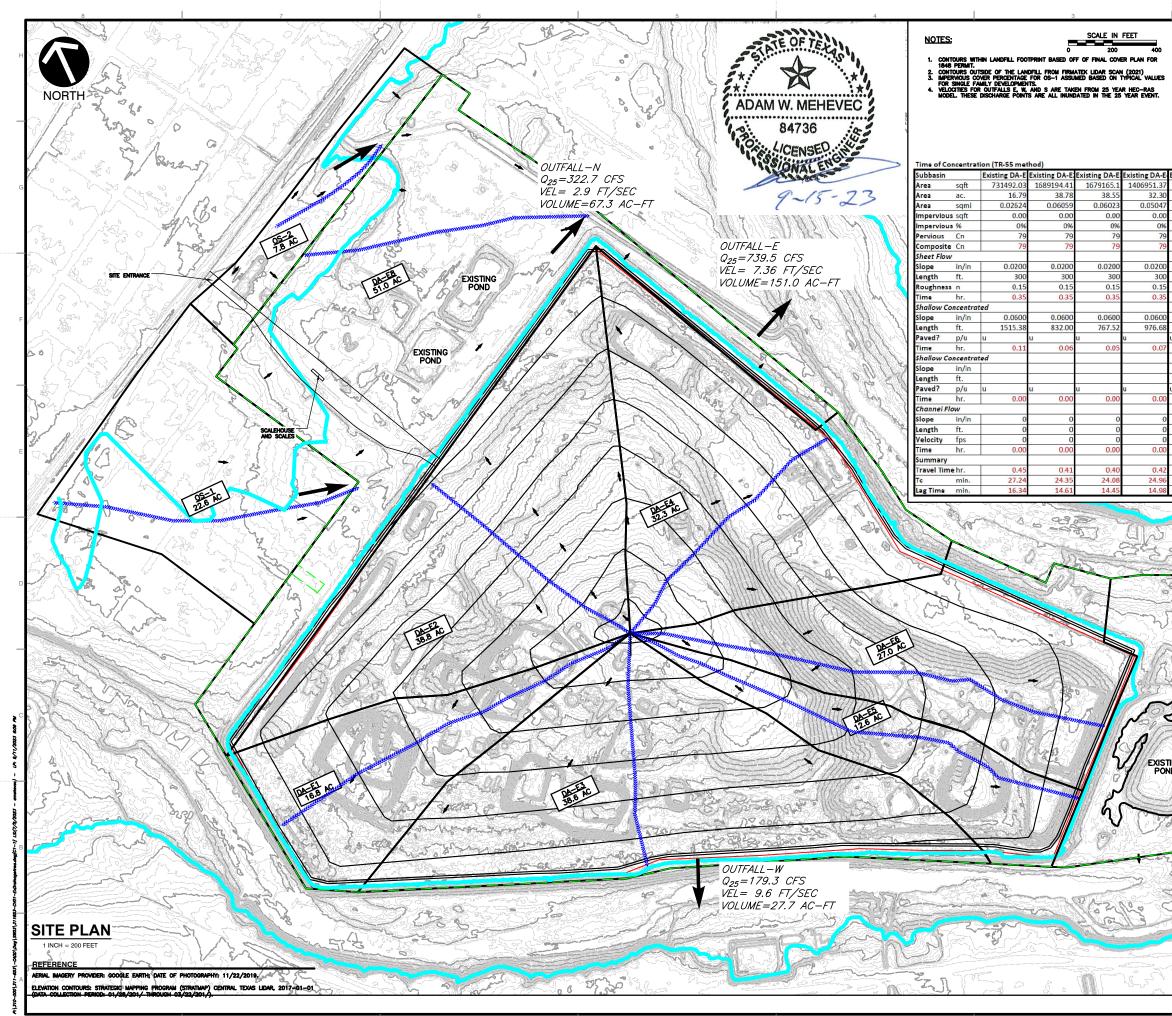
BECK LANDFILL APPENDIX C1-A FACILITY SURFACE WATER DRAINAGE REPORT EXISTING/POST-DEVELOPMENT COMPARISON

Includes pages C1-A-1 through C1-A-6



Civil & Environmental Consultants, Inc.

Beck Landfill Initial Submittal (9/23) Part III, Attachment C1-A



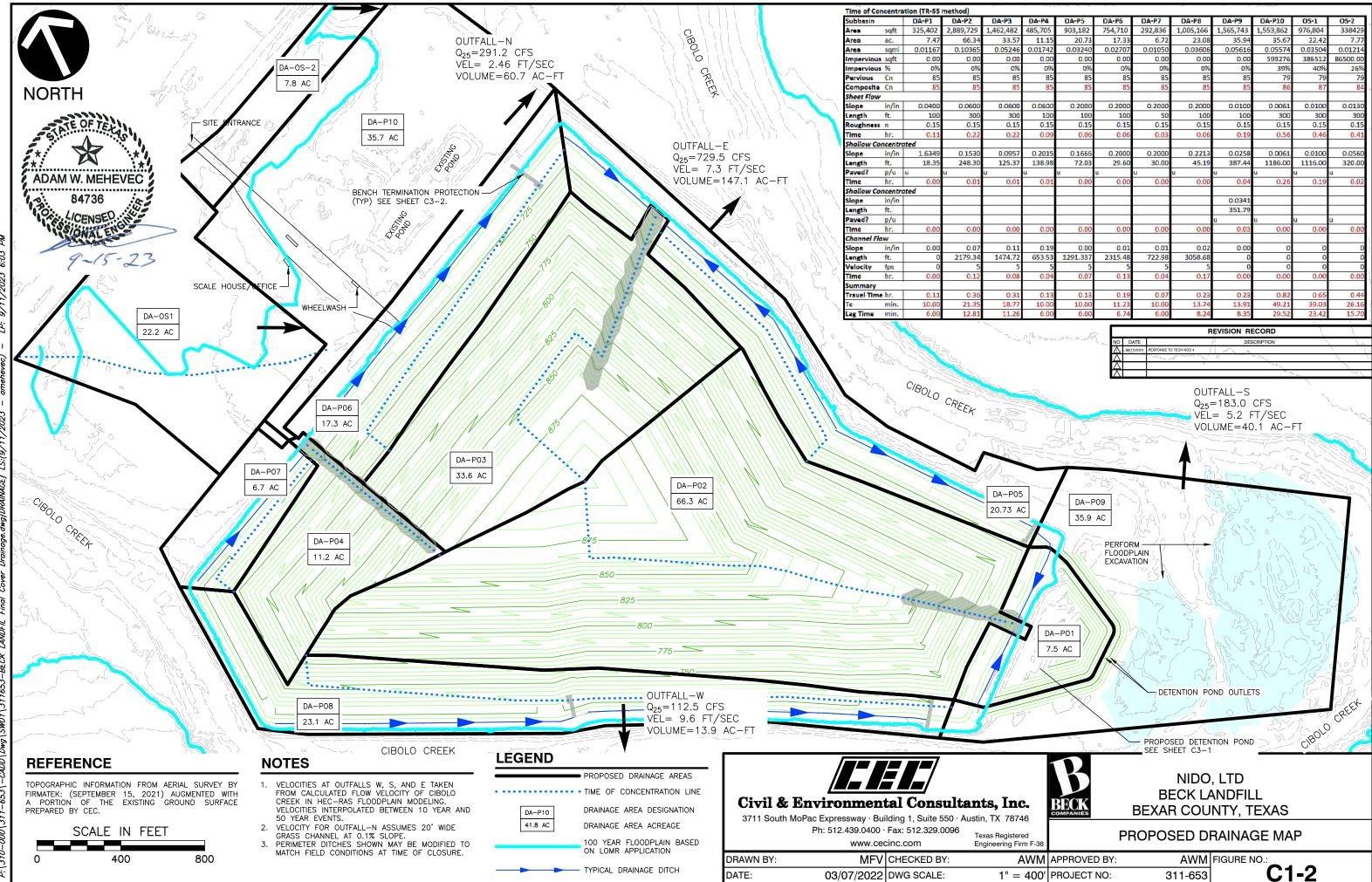
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| | 48751.391 12.60 | 1178062.52 27.04 | 1789193.1 41.07 | 2220496.38 50.98 | 976803.8 22.42 | 338429.02 7.77 | | 50 | NOD 4 RESPONSE | | | | | |
| | 0.01968 | 0.04226 | 0.06418 | 0.07965 599276.00 | 0.03504 386512.00 | 0.01214 86500.00 | | TECH NOD 3 | NOD 4 R | | | | Ц | |
| | 0% | 0% | 0% | 27% | 40% | 26% | | DATE | 09/15/2023 | | | | Π | |
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| _ | 0.15 0.35 | 0.15 0.35 | 0.15 | 0.15 0.56 | 0.15 0.46 | 0.15 0.41 | | | | £ | ļ | 7874 | | |
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| | 0.12 | 0.13 | 0.21 | 0.20 | 0.19 | 0.02 | | | | g Fimi | 3 | 1, Suft | Ph: 512.439.0400 · Fax: 512.329.0096 | ┋ |
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| 14. 1) 'JHE K | 0.00 | 0.00 | 0.73 44.08 26.45 | 0.82 49.21 29.52 | 0.65 39.03 23.42 | 0.44 26.16 15.70 | | | | Texas Registered Engineering Firm F-38 | | 3711 South MoPac Expressway · Building 1, Suite 550 · Austin, TX 78746 | | |
| | | 0.47 28.42 | 0.73 44.08 26.45 00 00 00 00 00 00 00 00 00 00 00 00 00 | 0.82 49.21 29.52 | 0.65 39.03 23.42 CFS FT/SEC | 0.44 26.16 15.70 | | | | | | | | |
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| | | 0.47 28.42 | 0.73 44.08 26.45 | 0.82 49.21 29.52 UTFALL – S 225 = 209.0 L = 5.2 | 0.65 39.03 23.42 CFS FT/SEC | 0.44 26.16 15.70 | | EXISTING DRAINAGE AREA MAP | | | 7/5/2023 DRWN BY SP 6000 FW /8, SCHERL XZ, IEXAS /8154 | | 311-653.SITE | APPROVEDBY: AWM |

25 Year Storm Existing Condition Runoff Summary

| Reach Summary | | Q25 (cfs) | Vol25 (ac-ft) | Vel25 (fps) | Runoff/on |
|---------------|----------|-----------|---------------|-------------|-----------|
| Outfall North | existing | 322.7 | 67.2 | 2.9 | Runoff |
| Outfall West | existing | 179.3 | 27.7 | 9.6 | Runoff |
| Outfall-South | existing | 209.0 | 40.2 | 5.2 | Runoff |
| Outfall East | existing | 739.5 | 151.0 | 7.3 | Runoff |

1. Peak flowrates and volumes computed using HEC-HMS.

2. Velocities for Outfalls East, West, and South taken from 25 Year HEC-RAS model of Cibolo Creek.



| | DA-P4 | DA-P5 | DA-P6 | DA-P7 | DA-P8 | DA-P9 | DA-P10 | OS-1 | OS-2 |
|----------|---------|----------|---------|---------|-----------|------------|-----------|---------------------------------------|----------|
| 2 | 485,705 | 903,182 | 754,710 | 292,836 | 1,005,166 | 1,565,743 | 1,553,862 | 976,804 | 338429 |
| 57 | 11.15 | 20.73 | 17.33 | 6.72 | 23.08 | 35.94 | 35.67 | 22.42 | 7.77 |
| 16 | 0.01742 | 0.03240 | 0.02707 | 0.01050 | 0.03606 | 0.05616 | 0.05574 | 0.03504 | 0.01214 |
| 00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 599276 | 386512 | 86500.00 |
| 1% | 0% | 0% | 0% | D% | 0% | 0% | 39% | 40% | 26% |
| 1% 85 | 85 | 85 | 85 | 85 | 85 | 85 | 79 | 79 | 79 |
| 35 | 85 | 85 | 85 | 85 | 85 | 85 | 86 | 87 | 84 |
| | | | | | | | | | |
| 00 | 0.0600 | 0.2000 | 0.2000 | 0.2000 | 0.2000 | 0.0100 | 0.0061 | 0.0100 | 0.0130 |
| 00 | 10D | 100 | 100 | 50 | 100 | 100 | 300 | 300 | 300 |
| 15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| 22 | 0.09 | 0.06 | 0.06 | 0.03 | 0.06 | 0.19 | 0.56 | 0.46 | 0.41 |
| | | | | | | | | | |
| 57 | 0.2015 | 0.1666 | 0.2000 | 0.2000 | 0.2213 | 0.0258 | D.0061 | 0.0100 | 0.0560 |
| 37 | 138.98 | 72.03 | 29.60 | 30.00 | 45.19 | 387.44 | 1186.00 | 1116.00 | 320.00 |
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| 01 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.04 | 0.26 | 0.19 | 0.02 |
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| | | | | | | 351.79 | | | |
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| 00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.03 | 0.00 | 0.00 | 0.00 |
| | | | | | | | | | |
| 11 | 0.19 | 0.00 | 0.01 | 0.01 | 0.02 | 0.00 | 0 | 0 | D |
| 72 5 | 653.53 | 1291.337 | 2315.48 | 722.98 | 3058.68 | 0 | 0 | 0 | 0 |
| 5 | 5 | 5 | 5 | 5 | 5 | 0 | 0 | 0 | 0 |
| 80 | 0.04 | 0.07 | 0.13 | 0.04 | 0.17 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | | | | | | | | |
| 31 | 0.13 | 0.13 | 0.19 | 0.07 | 0.23 | 0.23 | 0.82 | 0.65 | 0.44 |
| 77 | 10.00 | 10.00 | 11.23 | 10.00 | 13.74 | 13.91 | 49.21 | 39.03 | 26.16 |
| 26 | 6.00 | 6.00 | 6.74 | 6.00 | 8.24 | 8.35 | 29.52 | 23.42 | 15.70 |
| | | | | | _ | | | · · · · · · · · · · · · · · · · · · · | 1 |
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| AWM | APPROVED BY: | AWM | FIGURE NO.: |
|--------|--------------|---------|-------------|
| = 400' | PROJECT NO: | 311-653 | <u>C1-2</u> |
| | | | |

| Reach Summary | | Q25 (cfs) | Vol25 (ac-ft) | Vel25 (fps) | Runoff/on |
|---------------|----------|-----------|---------------|-------------|-----------|
| Outfall North | proposed | 291.2 | 60.7 | 2.5 | Runoff |
| Outfall West | proposed | 112.5 | 13.9 | 9.6 | Runoff |
| Outfall-South | proposed | 183.0 | 40.1 | 5.2 | Runoff |
| Outfall East | proposed | 729.5 | 147.1 | 7.3 | Runoff |

25 Year Storm Post-Developed Condition Runoff Summary

1. Peak flowrates and volumes computed using HEC-HMS.

2. Velocities for Outfalls East, West, and South taken from 25- Year HEC-RAS model of Cibolo Creek.

| Reach Summary | | Q25 (cfs) | Vol25 (ac-ft) | Vel25 (fps) | Runoff/on |
|---------------|--------------|-----------|---------------|-------------|-----------|
| Outfall North | existing | 322.7 | 67.2 | 2.9 | |
| | proposed | 291.2 | 60.7 | 2.5 | runoff |
| | difference % | -10% | -10% | -1.4% | |
| Outfall West | existing | 179.3 | 27.7 | 9.6 | |
| | proposed | 112.5 | 13.9 | 9.6 | runoff |
| | difference % | -37% | -50% | 0% | |
| Outfall South | existing | 209.9 | 40.2 | 5.2 | |
| | proposed | 183.0 | 40.1 | 5.2 | runoff |
| | difference % | -13% | -0% | 0% | |
| Outfall East | existing | 739.5 | 151.0 | 7.3 | |
| | proposed | 729.5 | 147.1 | 7.3 | runoff |
| | difference % | -1% | -3% | 0% | |

25 Year Return Period

Existing/Post-Developed Drainage Analysis Summary Tables

1. Peak flowrates and volumes computed using HEC-HMS.

2. Velocities for Outfalls West, South, and East taken from 25 Year HEC-RAS model of Cibolo Creek and represent the velocity in the creek at the discharge location.

100 Year Return Period

| Reach Summary | | Q100 (cfs) | Vol100 (ac-ft) | Vel100 (fps) | Runoff/on |
|---------------|--------------|------------|----------------|--------------|-----------|
| Outfall North | existing | 491.1 | 102.4 | 3.3 | |
| | proposed | 431.4 | 90.7 | 2.8 | runoff |
| | difference % | -12% | -12% | -1.4% | |
| Outfall West | existing | 281.9 | 43.6 | 12.2 | |
| | proposed | 165.7 | 20.8 | 12.2 | runoff |
| | difference % | -41% | -52% | 0% | |
| Outfall South | existing | 329.8 | 63.4 | 7.0 | |
| | proposed | 267.1 | 72.7 | 7.0 | runoff |
| | difference % | -19% | 15% | 0% | |
| Outfall East | existing | 1,146.8 | 234.4 | 7.3 | |
| | proposed | 1075.8 | 232.8 | 7.3 | runoff |
| | difference % | -6% | -1% | 0% | |

1. Peak flowrates and volumes computed using HEC-HMS.

2. Velocities for Outfalls West, South, and East taken from the 100-year HEC-RAS model of Cibolo Creek and represent the velocity in the creek at the discharge location.

BECK LANDFILL

APPENDIX C1-B FACILITY SURFACE WATER DRAINAGE REPORT EXISTING CONDITION HYDROLOGIC CALCULATIONS

Includes pages C1-B-1 through C1-B-14



Civil & Environmental Consultants, Inc.

Beck Landfill Initial Submittal (9/23) Part III, Attachment C1-B

EXISTING CONDITION NARRATIVE

30 TAC §330.305 This existing condition site evaluation represents the hydrologic calculations for Beck Landfill, in accordance with §330.305.

EXISTING CONDITION DRAINAGE AREA DRAWINGS

The existing condition drainage area maps depict the Beck Landfill property, facility boundary, and surrounding contributing areas. These maps reflect each individual drainage area, peak runoff, velocity, and volume for the 25-year rainfall event. Further, the existing condition runoff summary provides the peak flow rate, volume, and velocity at each comparison point along the property boundary. Offsite drainage areas are designated by the prefix "DA". Refer to Drawing C1-1 for the existing condition offsite drainage areas map.

The figure below is a soils map that depicts Beck Landfill drainage areas and the existing soil types. The Soil Survey of Guadalupe County, Texas, published by the Natural Resource Conservation Service is the reference for the base map and soils information. Based on the soils types, most of the soils surrounding the landfill are Hydrologic Group B. The map unit legend following the soils map list the various soil types within the contributing drainage area.



| Map Unit Symbol Map Unit Name | | Acres in AOI | Percent of AOI | | |
|--------------------------------|--|--------------|----------------|--|--|
| Tf | Tinn and Frio soils, 0 to 1 percent slopes, frequently flooded | 6.5 | 1.8% | | |
| Subtotals for Soil Survey Area | | 6.5 | 1.8% | | |
| Totals for Area of Interest | | 370.5 | 100.0% | | |
| | · | · | | | |
| Map Unit Symbol | Map Unit Name | Acres in AOI | Percent of AOI | | |
| BaA | Barbarosa silty clay, 0 to 1 percent slopes | 50.2 | 13.5% | | |
| Во | Bosque and Seguin soils, frequently flooded | 90.0 | 24.3% | | |
| SuA | Sunev loam, 0 to 1 percent slopes | 210.8 | 56.9% | | |
| SuB | Sunev loam, 1 to 3 percent slopes | 0.6 | 0.2% | | |
| SuC3 | Sunev loam, 3 to 5 percent slopes, eroded | 12.3 | 3.3% | | |
| Subtotals for Soil Survey Area | | 364.0 | 98.2% | | |
| Totals for Area of Interest | | 370.5 | 100.0% | | |

Map Unit Legend

WATERSHED CHARACTERISTICS

Watershed characteristics have been developed for the existing condition hydrologic evaluation. The watershed characteristics address drainage area runoff characteristics, unit hydrograph data, and reach characteristics.

The Existing Condition Watershed Characteristics, provides the summary of drainage areas, soil types, Curve Numbers (CN) values, initial loss, reach slope calculations, and determination of Manning's "n" values. The Soil Conservation Service (NRCS) CN were derived from watershed characteristic tables from the Urban Hydrology for Small Watersheds, Technical Report 55 (TR-55), which included evaluation of soil and surface cover/condition characteristics.

RAINFALL DATA

The rainfall depth, duration, and frequency relationships for the storm event for the facility was taken from the <u>2018 NOAA Atlas 14 Precipitation-Frequency Atlas of the United States, Volume 11, Version 2.0: Texas</u>. Return periods of 25 and 100 years and a duration of 24 hours were used for the design storms. The synthetic rainfall distribution is the NRCS 24-hour Type III storm. The Depth-Duration Frequency rainfall depths for the facility located in Guadalupe County, Texas are 8.56" for the 25-year storm event and 12.2" for the 100-year storm event. The maximum Tc for the model is sub-basins DA-E8 with 49.21 minutes and the minimum for is DA-E3 with 24.1 minutes.

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HEC-HMS SCHEMATIC

The schematic for the HEC-HMS model is included in the appendix to this section. The schematic provides the hydrologic element number and routing used for evaluating the existing condition in HEC-HMS.

HYDROLOGIC ANALYSIS

For the hydrologic evaluation, HEC-HMS version 4.11 was used for the precipitation-runoff simulation for the existing condition.

Watershed Subareas and Schematization

The drainage areas that contribute flow to Beck Landfill were delineated into subareas to derive peak flows to determine existing entering and exiting flows. Hydrographs are developed for each subarea and appropriately combined and routed through existing surface drainage features. The subareas are shown on Drawings C1-1 and C1-2 - Existing Condition Offsite Drainage Areas.

Time Step

The time step, or the program computation interval, selected for the analysis is 1 minute, which results in 1,440 hydrograph ordinates in 24 hours.

Hypothetical Precipitation

Return periods of 25 and 100 years and duration of 24 hours were used for the design storms. The precipitation is assumed to be evenly distributed over the entire basin for each time interval.

Precipitation Losses

Precipitation losses (the precipitation which does not contribute to the runoff) are calculated using the Soil Conservation Service (NRCS) Curve Number (CN) method. CN is a function of soil cover, land use, and antecedent moisture conditions. The CN values used for each drainage area are shown in the Watershed Characteristics tables.

Synthetic Unit Hydrographs and Routing

The rainfall/runoff transformation was performed with the NRCS method. The parameters and input values for this model are included in the Watershed Characteristics tables.

The Lag Method was used for routing flow through the existing drainage channels. A minimum 6-minute lag time was used to reflect a minimum 10 minute time of concentration.

EXISTING CONDITION FLOW SUMMARY

The existing condition flow summary table lists the peak flow rate and volume of runoff for each drainage area for the 25- and 100-year rainfall event. This table summarizes the results of the hydrologic evaluation.

EXISTING CONDITION VELOCITY SUMMARY

Surface water velocities were determined for each discharge point where the surface water exits the facility boundary. For Outfalls West, South, and East, which discharge directly into Cibolo Creek, the calculated 25-year flow velocity of the creek from the HEC-RAS model was used for both existing and proposed conditions. For Outfall North, the 25- and 100-year, 24-hour peak flow rates were used to determine the velocity at the drainage area boundary. Manning's Equation via the Flowmaster software was used to evaluate the velocities. Refer to the appendix to this report section for the existing condition velocity calculations.

EXISTING CONDITION DRAINAGE ANALYSIS SUMMARY

The analysis summary for the existing condition for each comparison point (Outfall-W, Outfall-S, Outfall-N, and Outfall-E) the peak flow rate, velocity, and volume resulting from the HEC-HMS evaluation for the 25- and 100-year, 24 hour rainfall is shown in the appendix to this report section.

WATERSHED CHARACTERISTICS

The curve numbers (Cn) used in the HEC-HMS model for non-landfill and the existing condition landfill were taken from Table 4-18 in the <u>TxDOT Hydraulic Design Manual</u>, September 2019. The curve numbers assume Hydrologic Soil Group B and Poor Condition grass coverage. See Table 4-18 below. The Cn for the proposed landfill was taken from the <u>TCEQ Surface Water Drainage and</u> <u>Erosional Stability Guidelines for a Municipal Solid Waste Landfills</u> Section 1.4.3, which recommends a range between 85 and 90 for the landfill final cover. Since the soils surrounding the Beck Landfill are predominately Hydrologic Group B and there is no synthetic component to the final cover to limit infiltration, a Curve Number of 85 was selected. The table below summarizes the selected Curve Numbers.

| Cn Values Selected | |
|---|----|
| Offsite and Onsite Areas Outside of Landfill Footprint and Existing Landfill Final Cover | 79 |
| Area Within Landfill Footprint Affected by Vertical Expansion | 85 |

Note: Curve numbers were adjusted to account for impervious cover within drainage area. Impervious areas were assigned a Cn of 98.

Table 4-18: Runoff Curve Numbers For Urban Areas

| Cover type and hydrologic condition | Average percent impervious area | A | в | с | D |
|---|--|----------|----|----|------|
| Open space (lawns, parks, golf courses, cemeteries, etc.): | | | | | |
| Notes: Values are for average runoff condition, and $I_a = 0.2S$. The average percent impervious area shown was used to develop th Other assumptions are: impervious areas are directly connected to t CN of 98, and pervious areas are considered equivalent to open spa | the drainage syste | em, impo | | | ve a |
| Cover type and hydrologic condition | Average percent impervious area | A | в | с | D |
| Poor condition (grass cover < 50%) | | 68 | 79 | 86 | 89 |
| Fair condition (grass cover 50% to 75%) | | 49 | 69 | 79 | 84 |
| Good condition (grass cover > 75%) | | 39 | 61 | 74 | 80 |
| Paved parking lots, roofs, driveways, etc. (excluding right-of- way) | | 98 | 98 | 98 | 98 |
| Streets and roads: | | • | | | |
| Paved; curbs and storm drains (excluding right-of-way) | | 98 | 98 | 98 | 98 |
| Paved; open ditches (including right-of-way) | | 83 | 89 | 92 | 93 |
| Gravel (including right-of-way) | | 76 | 85 | 89 | 91 |
| Dirt (including right-of-way) | | 72 | 82 | 87 | 89 |
| Western desert urban areas: | • | • | | | |
| Natural desert landscaping (pervious areas only) | | 63 | 77 | 85 | 88 |
| Artificial desert landscaping (impervious weed barrier, desert shrub with 1- to 2-in. sand or gravel mulch and basin borders) | | 96 | 96 | 96 | 96 |
| Urban districts: | | | | | |
| Commercial and business | 85 | 89 | 92 | 94 | 95 |
| Industrial | 72 | 81 | 88 | 91 | 93 |
| Residential districts by average lot size: | | | | | |
| 1/8 acre or less (townhouses) | 65 | 77 | 85 | 90 | 92 |
| 1/4 acre | 38 | 61 | 75 | 83 | 87 |
| 1/3 acre | 30 | 57 | 72 | 81 | 86 |
| 1/2 acre | 25 | 54 | 70 | 80 | 85 |
| 1 acre | 20 | 51 | 68 | 79 | 84 |
| 2 acres | 12 | 46 | 65 | 77 | 82 |
| Developing urban areas: Newly graded areas (pervious area only, no vegetation) | | 77 | 86 | 91 | 94 |
| Notes: Values are for average runoff condition, and $I_a = 0.2S$. The average percent impervious area shown was used to develop the Other assumptions are: impervious areas are directly connected to CN of 98, and pervious areas are considered equivalent to open spa | the drainage syste | em, imp | | | ve a |

RAINFALL DATA



NOAA Atlas 14, Volume 11, Version 2 Location name: Schertz, Texas, USA* Latitude: 29.5483°, Longitude: -98.2639° Elevation: 706.71 ft** * source: ESRIMaps * source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials_

PF tabular

| PDS-b | ased poin | t precipita | ation frequ | | | | | ce interv | als (in in | ches) ¹ |
|----------|------------------------|------------------------|--------------|---------------|-----------------------|-------------------|----------------------|-------------|----------------------|--------------------|
| Duration | 1 | 2 | 5 | Average 10 | 25 | interval (y 50 | ears) 100 | 200 | 500 | 1000 |
| 5-min | 0.443 (0.336-0.585) | 0.524 (0.400-0.684) | 0.655 | 0.765 | 0.918 (0.667-1.26) | 1.04 | 1.16 (0.798-1.68) | 1.29 | 1.46 (0.949-2.25) | 1.60 |
| 10-min | 0.705 | 0.835 | 1.05 | 1.22 | 1.47 | 1.66 | 1.86 | 2.05 | 2.31 | 2.50 |
| | (0.534-0.931) | (0.637-1.09) | (0.796-1.37) | (0.918-1.63) | (1.07-2.02) | (1.18-2.35) | (1.28-2.69) | (1.38-3.05) | (1.50-3.55) | (1.58-3.95) |
| 15-min | 0.902 | 1.06 | 1.32 | 1.53 | 1.83 | 2.06 | 2.29 | 2.54 | 2.88 | 3.15 |
| | (0.683-1.19) | (0.808-1.38) | (1.00-1.73) | (1.15-2.04) | (1.33-2.51) | (1.46-2.90) | (1.58-3.33) | (1.71-3.78) | (1.87-4.44) | (1.99-4.98) |
| 30-min | 1.27 | 1.49 | 1.84 | 2.14 | 2.54 | 2.85 | 3.17 | 3.53 | 4.03 | 4.43 |
| | (0.962-1.68) | (1.14-1.95) | (1.40-2.42) | (1.60-2.85) | (1.84-3.48) | (2.02-4.02) | (2.19-4.60) | (2.37-5.25) | (2.62-6.21) | (2.80-7.00) |
| 60-min | 1.64 | 1.93 | 2.42 | 2.82 | 3.39 | 3.81 | 4.27 | 4.78 | 5.53 | 6.14 |
| | (1.24-2.16) | (1.48-2.52) | (1.84-3.17) | (2.12-3.76) | (2.45-4.63) | (2.69-5.37) | (2.94-6.19) | (3.22-7.12) | (3.59-8.53) | (3.89-9.70) |
| 2-hr | 1.95 | 2.38 | 3.04 | 3.62 | 4.46 | 5.14 | 5.88 | 6.73 | 7.98 | 9.03 |
| | (1.48-2.56) | (1.81-3.05) | (2.32-3.95) | (2.73-4.80) | (3.26-6.09) | (3.65-7.21) | (4.07-8.48) | (4.54-9.96) | (5.20-12.3) | (5.74-14.2) |
| 3-hr | 2.11 | 2.64 | 3.42 | 4.13 | 5.18 | 6.05 | 7.02 | 8.14 | 9.80 | 11.2 |
| | (1.61-2.76) | (1.99-3.33) | (2.61-4.42) | (3.12-5.45) | (3.79-7.05) | (4.31-8.47) | (4.87-10.1) | (5.50-12.0) | (6.40-15.0) | (7.13-17.5) |
| 6-hr | 2.40 | 3.08 | 4.06 | 4.98 | 6.38 | 7.57 | 8.92 | 10.5 | 12.8 | 14.8 |
| | (1.84-3.12) | (2.32-3.83) | (3.11-5.21) | (3.79-6.54) | (4.70-8.65) | (5.43-10.6) | (6.22-12.8) | (7.12-15.4) | (8.42-19.6) | (9.49-23.1) |
| 12-hr | 2.71 | 3.52 | 4.67 | 5.77 | 7.46 | 8.91 | 10.6 | 12.6 | 15.6 | 18.1 |
| | (2.09-3.50) | (2.65-4.32) | (3.60-5.95) | (4.41-7.53) | (5.53-10.1) | (6.43-12.4) | (7.42-15.0) | (8.55-18.3) | (10.2-23.6) | (11.6-28.1) |
| 24-hr | 3.05 | 3.99 | 5.31 | 6.60 | 8.56 | 10.3 | 12.2 | 14.6 | 18.2 | 21.2 |
| | (2.36-3.91) | (3.01-4.85) | (4.11-6.73) | (5.06-8.55) | (6.38-11.5) | (7.44-14.2) | (8.61-17.3) | (9.96-21.1) | (12.0-27.3) | (13.7-32.7) |
| 2-day | 3.46 | 4.54 | 6.07 | 7.54 | 9.78 | 11.7 | 14.0 | 16.6 | 20.7 | 24.1 |
| | (2.70-4.42) | (3.45-5.50) | (4.72-7.64) | (5.81-9.71) | (7.32-13.0) | (8.53-16.1) | (9.87-19.6) | (11.4-23.9) | (13.7-30.9) | (15.6-37.0) |
| 3-day | 3.77 | 4.93 | 6.58 | 8.15 | 10.5 | 12.6 | 15.0 | 17.7 | 21.9 | 25.5 |
| | (2.94-4.80) | (3.76-5.95) | (5.13-8.25) | (6.30-10.5) | (7.91-14.0) | (9.20-17.2) | (10.6-21.0) | (12.2-25.5) | (14.6-32.7) | (16.5-39.0) |
| 4-day | 4.02 | 5.22 | 6.96 | 8.60 | 11.1 | 13.2 | 15.6 | 18.5 | 22.7 | 26.3 |
| | (3.14-5.10) | (4.01-6.32) | (5.45-8.71) | (6.67-11.0) | (8.33-14.7) | (9.65-18.0) | (11.1-21.8) | (12.7-26.4) | (15.1-33.7) | (17.0-40.0) |
| 7-day | 4.60 | 5.90 | 7.80 | 9.56 | 12.2 | 14.4 | 16.9 | 19.7 | 23.9 | 27.5 |
| | (3.62-5.81) | (4.57-7.15) | (6.14-9.73) | (7.44-12.2) | (9.19-16.1) | (10.6-19.5) | (12.0-23.5) | (13.7-28.1) | (16.0-35.5) | (17.9-41.7) |
| 10-day | 5.09 | 6.45 | 8.48 | 10.3 | 13.1 | 15.3 | 17.9 | 20.7 | 24.9 | 28.4 |
| | (4.01-6.41) | (5.03-7.83) | (6.69-10.6) | (8.06-13.1) | (9.87-17.1) | (11.3-20.7) | (12.7-24.7) | (14.4-29.5) | (16.6-36.7) | (18.5-42.9) |
| 20-day | 6.56 | 8.08 | 10.5 | 12.5 | 15.5 | 17.8 | 20.4 | 23.1 | 27.1 | 30.4 |
| | (5.19-8.21) | (6.40-9.88) | (8.31-13.0) | (9.81-15.8) | (11.7-20.1) | (13.1-23.9) | (14.6-28.0) | (16.1-32.8) | (18.2-39.8) | (19.9-45.8) |
| 30-day | 7.76 | 9.40 | 12.0 | 14.3 | 17.4 | 19.8 | 22.4 | 25.1 | 29.0 | 32.1 |
| | (6.16-9.66) | (7.51-11.5) | (9.61-14.9) | (11.2-17.9) | (13.2-22.6) | (14.6-26.5) | (16.1-30.7) | (17.6-35.4) | (19.5-42.4) | (21.0-48.1) |
| 45-day | 9.40 | 11.2 | 14.2 | 16.7 | 20.1 | 22.7 | 25.4 | 28.2 | 32.1 | 35.1 |
| | (7.48-11.7) | (9.04-13.8) | (11.4-17.6) | (13.2-20.9) | (15.3-26.0) | (16.8-30.2) | (18.3-34.8) | (19.8-39.7) | (21.7-46.8) | (23.1-52.5) |
| 60-day | 10.8 | 12.8 | 16.2 | 18.9 | 22.6 | 25.4 | 28.2 | 31.1 | 35.0 | 38.0 |
| | (8.65-13.4) | (10.4-15.8) | (13.0-19.9) | (14.9-23.6) | (17.2-29.1) | (18.8-33.6) | (20.3-38.4) | (21.8-43.6) | (23.7-50.8) | (25.0-56.7) |

Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

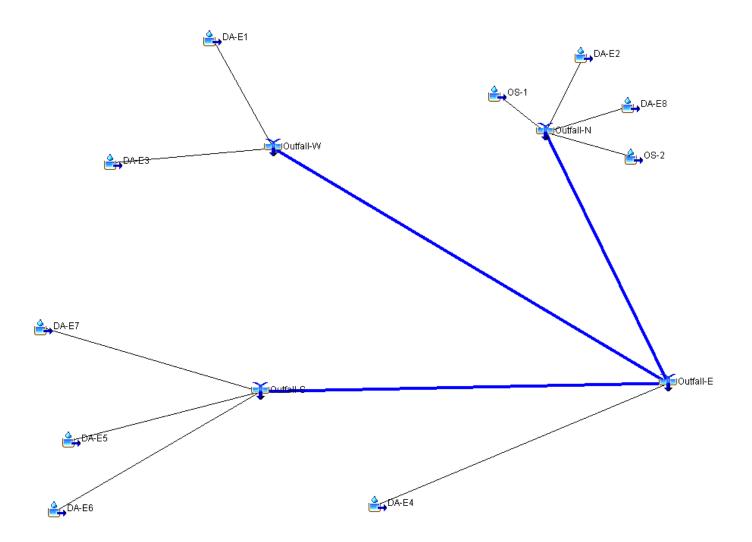
Device Terr

EXISTING CONDITIONS TIME OF CONCENTRATION TABLE C1-B-1

Time of Concentration (TR-55 method)

| Carla Inc. | | Endedline D.A. E | Futurity - DA F | Fulletter DA F | Full Aligner D.A. F | Full March 19 A | Fulleting DA F | Future DA F | Full-Alian D.A. Fr | 00.1 | 00.0 |
|--------------|----------|------------------|-----------------|----------------|---------------------|-----------------|----------------|-------------|--------------------|-----------|----------|
| Subbasin | | | | | | Existing DA-E | | | | | OS-2 |
| | sqft | 731492.03 | 1689194.41 | 1679165.1 | | | 1178062.52 | 1789193.1 | 2220496.38 | | |
| Area | ac. | 16.79 | 38.78 | 38.55 | 32.30 | | 27.04 | 41.07 | 50.98 | 22.42 | 7.77 |
| Area | sqmi | 0.02624 | 0.06059 | 0.06023 | 0.05047 | 0.01968 | 0.04226 | 0.06418 | 0.07965 | 0.03504 | 0.01214 |
| Impervious | sqft | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 599276.00 | 386512.00 | 86500.00 |
| Impervious | % | 0% | 0% | 0% | 0% | | 0% | 0% | 27% | 40% | 26% |
| | Cn | 79 | 79 | 79 | 79 | 79 | 79 | 79 | 79 | 79 | 79 |
| Composite | Cn | 79 | 79 | 79 | 79 | 79 | 79 | 79 | 84 | 87 | 84 |
| Sheet Flow | | | | | | | | | | | |
| Slope | in/in | 0.0200 | 0.0200 | 0.0200 | 0.0200 | 0.0200 | 0.0200 | 0.0073 | 0.0061 | 0.0100 | 0.0130 |
| Length | ft. | 300 | 300 | 300 | 300 | 300 | 300 | 300 | 300 | 300 | 300 |
| Roughness | n | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| Time | hr. | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | 0.35 | 0.52 | 0.56 | 0.46 | 0.41 |
| Shallow Con | ncentrat | ed | | | | | | | | | |
| Slope | in/in | 0.0600 | 0.0600 | 0.0600 | 0.0600 | 0.0600 | 0.0600 | 0.0073 | 0.0061 | 0.0100 | 0.0560 |
| Length | ft. | 1515.38 | 832.00 | 767.52 | 976.68 | 1678.79 | 1795.48 | 1066.00 | 1186.00 | 1116.00 | 320.00 |
| Paved? | p/u | u | u | u | u | u | u | u | u | u | u |
| Time | hr. | 0.11 | 0.06 | 0.05 | 0.07 | 0.12 | 0.13 | 0.21 | 0.26 | 0.19 | 0.02 |
| Shallow Con | ncentrat | ed | | | | | | | | | |
| Slope | in/in | | | | | | | | | | |
| Length | ft. | | | | | | | | | | |
| Paved? | p/u | u | u | u | u | u | u | u | u | u | u |
| Time | hr. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Channel Flow | w | | | | | | | | | | |
| Slope | in/in | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Length | ft. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Velocity | fps | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Time | hr. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Summary | | | | | | | | | | | |
| Travel Time | hr. | 0.45 | 0.41 | 0.40 | 0.42 | 0.47 | 0.47 | 0.73 | 0.82 | 0.65 | 0.44 |
| Tc | min. | 27.24 | 24.35 | 24.08 | 24.96 | 27.93 | 28.42 | 44.08 | 49.21 | 39.03 | 26.16 |
| Lag Time | min. | 16.34 | 14.61 | 14.45 | 14.98 | 16.76 | 17.05 | 26.45 | 29.52 | 23.42 | 15.70 |

EXISTING CONDITION HEC-HMS SCHEMATIC



HYDROLOGIC ANALYSIS

25-YEAR, TYPE III, NRCS, 24-HOUR STORM EVENT 100-YEAR, TYPE III, NRCS, 24-HOUR STORM EVENT

EXISTING CONDITION FLOW SUMMARY

25-Year Results

| | E | tart of Run: 01Jan2001 nd of Run: 02Jan2001 compute Time:08Sep2023 | , 00:02 Meteorologic Model: 100 | |
|-----------------------------|------------------------|--|---------------------------------|--------------------------------|
| Show Elements: All Elements | ents \sim | Volu | me Units: 🔿 IN 💿 ACRE-FT | Sorting: Watershed Explorer $$ |
| Hydrologic Element | Drainage Area (MI2) | Peak Discharge (CFS) | Time of Peak | Volume (ACRE-FT) |
| DA-E3 | 0.1 | 200.4 | 1 January 2001, 10:08 | 30.4 |
| DA-E1 | 0.0 | 82.5 | 1 January 2001, 10:10 | 13.2 |
| Outfall-W | 0.1 | 281.9 | 1 January 2001, 10:09 | 43.6 |
| DA-E8 | 0.1 | 196.5 | 1 January 2001, 10:23 | 44.8 |
| DA-E2 | 0.1 | 201.0 | 1 January 2001, 10:08 | 30.6 |
| OS-1 | 0.0 | 100.1 | 1 January 2001, 10:16 | 20.2 |
| OS-2 | 0.0 | 41.7 | 1 January 2001, 10:09 | 6.8 |
| Outfall-N | 0.2 | 491.1 | 1 January 2001, 10:12 | 102.4 |
| E to N reach | 0.2 | 491.1 | 1 January 2001, 10:15 | 102.3 |
| DA-E7 | 0.1 | 155.5 | 1 January 2001, 10:20 | 32.2 |
| DA-E6 | 0.0 | 129.6 | 1 January 2001, 10:11 | 21.3 |
| DA-E5 | 0.0 | 60.9 | 1 January 2001, 10:10 | 9.9 |
| Outfall-S | 0.1 | 329.8 | 1 January 2001, 10:13 | 63.4 |
| S to E | 0.1 | 329.8 | 1 January 2001, 10:19 | 63.3 |
| W to E Reach | 0.1 | 281.9 | 1 January 2001, 10:27 | 43.4 |
| DA-E4 | 0.1 | 165.1 | 1 January 2001, 10:09 | 25.4 |
| Outfall-E | 0.5 | 1146.8 | 1 January 2001, 10:20 | 234.4 |

Project: Beck with Southern Outfall Simulation Run: FX 100-YR

Civil & Environmental Consultants, Inc.

100-Year Results

| | | Project: Beck with S | outhern Outfall Simulation Run: EX 100 | -YR |
|-------------------------|------------------------|---|--|--------------------------------|
| | E | tart of Run: 01Jan2001 ind of Run: 02Jan2001 compute Time:08Sep2023 | , 00:02 Meteorologic Model: 100 | |
| Show Elements: All Elem | ents \sim | Volu | me Units: 🔿 IN 💿 ACRE-FT | Sorting: Watershed Explorer $$ |
| Hydrologic Element | Drainage Area (MI2) | Peak Discharge (CFS) | Time of Peak | Volume (ACRE-FT) |
| DA-E3 | 0.1 | 200.4 | 1 January 2001, 10:08 | 30.4 |
| DA-E1 | 0.0 | 82.5 | 1 January 2001, 10:10 | 13.2 |
| Outfall-W | 0.1 | 281.9 | 1 January 2001, 10:09 | 43.6 |
| DA-E8 | 0.1 | 196.5 | 1 January 2001, 10:23 | 44.8 |
| DA-E2 | 0.1 | 201.0 | 1 January 2001, 10:08 | 30.6 |
| OS-1 | 0.0 | 100.1 | 1 January 2001, 10:16 | 20.2 |
| OS-2 | 0.0 | 41.7 | 1 January 2001, 10:09 | 6.8 |
| Outfall-N | 0.2 | 491.1 | 1 January 2001, 10:12 | 102.4 |
| E to N reach | 0.2 | 491.1 | 1 January 2001, 10:15 | 102.3 |
| DA-E7 | 0.1 | 155.5 | 1 January 2001, 10:20 | 32.2 |
| DA-E6 | 0.0 | 129.6 | 1 January 2001, 10:11 | 21.3 |
| DA-E5 | 0.0 | 60.9 | 1 January 2001, 10:10 | 9.9 |
| Outfall-S | 0.1 | 329.8 | 1 January 2001, 10:13 | 63.4 |
| S to E | 0.1 | 329.8 | 1 January 2001, 10:19 | 63.3 |
| W to E Reach | 0.1 | 281.9 | 1 January 2001, 10:27 | 43.4 |
| DA-E4 | 0.1 | 165.1 | 1 January 2001, 10:09 | 25.4 |
| Outfall-E | 0.5 | 1146.8 | 1 January 2001, 10:20 | 234.4 |

BECK LANDFILL

APPENDIX C1-C FACILITY SURFACE WATER DRAINAGE REPORT POST-DEVELOPMENT HYDROLOGIC CALCULATIONS

Includes pages C1-C-1 through C1-C-14



Civil & Environmental Consultants, Inc.

POST-DEVELOPMENT NARRATIVE

30 TAC § 330.305The post-development hydrologic analysis represents the hydrologic calculations after the proposed landfill is developed in accordance with §330.305(a)-(d).

POST-DEVELOPMENT DRAINAGE AREA DRAWINGS

The post-development drainage area drawings depict Beck Landfill facility development and the offsite drainage areas. These drawings depict the drainage areas for the facility development including the entrance facilities, storage and processing facilities, and the landfill development. Further, the post-development runoff summary provides peak discharge, volume, and velocity for the 25- and 100-year rainfall events at each comparison point along the facility and property boundary. Offsite and onsite drainage areas are designated by the prefix "DA".

WATERSHED CHARACTERISTICS

Watershed characteristics have been developed for the post-development hydrologic evaluation. The watershed characteristics address drainage area runoff characteristics, unit hydrograph data, reach characteristics, and the proposed final condition drainage system including the detention pond.

The first table, Post-development Watershed Characteristics, provides the summary of drainage areas, soil types, Curve Number (CN) values, initial loss, reach slope calculations, and determination of Manning's "n" values. The Soil Conservation Service (NRCS) CN were derived from watershed characteristic tables from the <u>TxDOT Hydraulic Design Manual</u>, <u>September 2019</u>, as discussed in Appendix C1-B, which included evaluation of anticipated post-development soil and surface cover/condition characteristics. The runoff characteristics for the offsite drainage areas did not change from the existing condition.

POST-DEVELOPMENT SURFACE WATER IMPOUNDMENT DESIGN PARAMETERS

This appendix to this section of the report includes pond and outlet structure data for the surface water impoundment incorporated in the hydrologic model.

HEC-HMS SCHEMATIC

The schematic for the HEC-HMS model provides the hydrologic element number and routing used for evaluating the post-development condition in HEC-HMS.

HYDROLOGIC ANALYSIS

For the hydrologic evaluation, HEC-HMS was used for the precipitation runoff simulation for the post-development condition. The following describes the various modeling components.

Watershed Subareas and Schematization

The landfill area that contributes flow to Cibolo Creek and the detention pond was delineated into sub basins to derive peak discharge and hydrographs. Hydrographs developed for each sub basin are appropriately combined and routed through the benches and perimeter channels. The sub basins are shown on Figure C1-2, and the HEC-HMS schematic of the post-development condition.

Time Step

The time step, or the program computation interval, selected for the analysis is 1 minute, which results in 1,440 hydrograph ordinates in 24 hours.

Hypothetical Precipitation

Return periods of 25, and 100 years and duration of 24 hours are used for the design storm. The rainfall distribution is the NRCS 24-hour Type III storm. The precipitation is assumed to be evenly distributed over the entire basin for each time interval.

Precipitation Losses

Precipitation losses (precipitation that does not contribute to the runoff) are calculated using the Soil Conservation Service (NRCS) Curve Number (CN) method. CN is a function of soil cover, land use, and antecedent moisture conditions. The CN values used for each drainage area are shown in the Watershed Characteristics table.

Synthetic Unit Hydrographs and Routing

The rainfall/runoff transformation was performed with the NRCS Method as described in detail in Urban Hydrology for Small Watersheds, (TR-55). The parameters and input values for this model are included in the Watershed Characteristics tables.

The Lag Method was used for routing through the existing and proposed drainage channels.

POST-DEVELOPMENT FLOW SUMMARY

The post-development flow summary table lists the peak flow rate and volume of runoff for each drainage area for the 25- and 100-year rainfall event. This table summarizes the results of the post-development hydrologic evaluation.

POST-DEVELOPMENT VELOCITY SUMMARY

Surface water velocities were determined for each discharge point where the surface water exits the facility boundary. For Outfalls West, South, and East, which discharge directly into Cibolo Creek, the calculated 25-year flow velocity of the creek from the HEC-RAS model was used for both existing and proposed conditions. For Outfall North, the 25- and 100-year, 24-hour peak flow rates were used to determine the velocity at the drainage area boundary.

Manning's Equation via the Flowmaster software was used to evaluate the velocities. Refer to the appendix to this report section for the proposed condition velocity calculations.

POST-DEVELOPMENT DRAINAGE ANALYSIS SUMMARY

The analysis summary for the proposed condition for each comparison point (Outfall-W, Outfall-S, Outfall-N, and Outfall-E) the peak flow rate, velocity, and volume resulting from the HEC-HMS evaluation for the 25- and 100-year, 24 hour rainfall is shown in the appendix to this report section.

WATERSHED CHARACTERISTICS

The curve numbers (Cn) used in the HEC-HMS model for non-landfill and the existing condition landfill were taken from Table 4-18 in the <u>TxDOT Hydraulic Design Manual</u>, <u>September 2019</u>. The curve numbers assume Hydrologic Soil Group B and Poor Condition grass coverage. See Table 4-18 below. The Cn for the proposed landfill was taken from the <u>TCEQ Surface Water Drainage and Erosional Stability Guidelines for a Municipal Solid</u> <u>Waste Landfill</u> Section 1.4.3, which recommends a range between 85 and 90 for the landfill final cover. Since the soils surrounding the Beck Landfill are predominately Hydrologic Group B and there is no synthetic component to the final cover to limit infiltration, a Curve Number of 85 was selected. The table below summarizes the selected Curve Numbers.

| Cn Values Selected | |
|---|----|
| Offsite and Onsite Areas Outside of Landfill Footprint and Existing | 79 |
| Landfill Final Cover | |
| Area Within Landfill Footprint Affected by Vertical Expansion | 85 |

Note: Curve numbers were adjusted to account for impervious cover within drainage area. Impervious areas were assigned a Cn of 98.

Table 4-18: Runoff Curve Numbers For Urban Areas

| Cover type and hydrologic condition | Average percent impervious area | A | В | с | D |
|--|--|----------|----|----|-------|
| Open space (lawns, parks, golf courses, cemeteries, etc.): | | | | | |
| Notes: Values are for average runoff condition, and $I_a = 0.2S$. The average percent impervious area shown was used to develop th Other assumptions are: impervious areas are directly connected to to CN of 98, and pervious areas are considered equivalent to open spa | the drainage syste | em, impe | | | ve a |
| Cover type and hydrologic condition | Average percent impervious area | A | в | с | D |
| Poor condition (grass cover < 50%) | | 68 | 79 | 86 | 89 |
| Fair condition (grass cover 50% to 75%) | | 49 | 69 | 79 | 84 |
| Good condition (grass cover > 75%) | | 39 | 61 | 74 | 80 |
| Paved parking lots, roofs, driveways, etc. (excluding right-of- way) | | 98 | 98 | 98 | 98 |
| Streets and roads: | • | • | | | |
| Paved; curbs and storm drains (excluding right-of-way) | | 98 | 98 | 98 | 98 |
| Paved; open ditches (including right-of-way) | | 83 | 89 | 92 | 93 |
| Gravel (including right-of-way) | | 76 | 85 | 89 | 91 |
| Dirt (including right-of-way) | | 72 | 82 | 87 | 89 |
| Western desert urban areas: | • | • | | • | |
| Natural desert landscaping (pervious areas only) | | 63 | 77 | 85 | 88 |
| Artificial desert landscaping (impervious weed barrier, desert shrub with 1- to 2-in. sand or gravel mulch and basin borders) | | 96 | 96 | 96 | 96 |
| Urban districts: | | | | | |
| Commercial and business | 85 | 89 | 92 | 94 | 95 |
| Industrial | 72 | 81 | 88 | 91 | 93 |
| Residential districts by average lot size: | | | | | |
| 1/8 acre or less (townhouses) | 65 | 77 | 85 | 90 | 92 |
| 1/4 acre | 38 | 61 | 75 | 83 | 87 |
| 1/3 acre | 30 | 57 | 72 | 81 | 86 |
| 1/2 acre | 25 | 54 | 70 | 80 | 85 |
| 1 acre | 20 | 51 | 68 | 79 | 84 |
| 2 acres | 12 | 46 | 65 | 77 | 82 |
| Developing urban areas: Newly graded areas (pervious area only, no vegetation) | | 77 | 86 | 91 | 94 |
| Notes: Values are for average runoff condition, and $I_a = 0.2S$. The average percent impervious area shown was used to develop the Other assumptions are: impervious areas are directly connected to CN of 98, and pervious areas are considered equivalent to open space. | the drainage syste | em, imp | | | ive a |

RAINFALL DATA



NOAA Atlas 14, Volume 11, Version 2 Location name: Schertz, Texas, USA* Latitude: 29.5483°, Longitude: -98.2639° Elevation: 706.71 ft** * source: ESRI Maps * source: USSS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials_

PF tabular

| PDS-b | ased poin | t precipita | ation frequ | uency es | timates v | vith 90% | confiden | ce interv | als (in in | ches) ¹ |
|----------|---------------------|-------------------------|---------------------|---------------------|---------------------|---------------------|-------------------------|---------------------|---------------------|---------------------|
| Duration | | | | Average | recurrence | interval (y | ears) | | | |
| Duration | 1 | 2 | 5 | 10 | 25 | 50 | 100 | 200 | 500 | 1000 |
| 5-min | 0.443 | 0.524 | 0.655 | 0.765 | 0.918 | 1.04 | 1.16 | 1.29 | 1.46 | 1.60 |
| | (0.336-0.585) | (0.400-0.684) | (0.499-0.860) | (0.574-1.02) | (0.667-1.26) | (0.733-1.46) | (0.798-1.68) | (0.864-1.91) | (0.949-2.25) | (1.01-2.53) |
| 10-min | 0.705 | 0.835 | 1.05 | 1.22 | 1.47 | 1.66 | 1.86 | 2.05 | 2.31 | 2.50 |
| | (0.534-0.931) | (0.637-1.09) | (0.796-1.37) | (0.918-1.63) | (1.07-2.02) | (1.18-2.35) | (1.28-2.69) | (1.38-3.05) | (1.50-3.55) | (1.58-3.95) |
| 15-min | 0.902 | 1.06 | 1.32 | 1.53 | 1.83 | 2.06 | 2.29 | 2.54 | 2.88 | 3.15 |
| | (0.683-1.19) | (0.808-1.38) | (1.00-1.73) | (1.15-2.04) | (1.33-2.51) | (1.46-2.90) | (1.58-3.33) | (1.71-3.78) | (1.87-4.44) | (1.99-4.98) |
| 30-min | 1.27 | 1.49 | 1.84 | 2.14 | 2.54 | 2.85 | 3.17 | 3.53 | 4.03 | 4.43 |
| | (0.962-1.68) | (1.14-1.95) | (1.40-2.42) | (1.60-2.85) | (1.84-3.48) | (2.02-4.02) | (2.19-4.60) | (2.37-5.25) | (2.62-6.21) | (2.80-7.00) |
| 60-min | 1.64 | 1.93 | 2.42 | 2.82 | 3.39 | 3.81 | 4.27 | 4.78 | 5.53 | 6.14 |
| | (1.24-2.16) | (1.48-2.52) | (1.84-3.17) | (2.12-3.76) | (2.45-4.63) | (2.69-5.37) | (2.94-6.19) | (3.22-7.12) | (3.59-8.53) | (3.89-9.70) |
| 2-hr | 1.95 | 2.38 | 3.04 | 3.62 | 4.46 | 5.14 | 5.88 | 6.73 | 7.98 | 9.03 |
| | (1.48-2.56) | (1.81-3.05) | (2.32-3.95) | (2.73-4.80) | (3.26-6.09) | (3.65-7.21) | (4.07-8.48) | (4.54-9.96) | (5.20-12.3) | (5.74-14.2) |
| 3-hr | 2.11 | 2.64 | 3.42 | 4.13 | 5.18 | 6.05 | 7.02 | 8.14 | 9.80 | 11.2 |
| | (1.61-2.76) | (1.99-3.33) | (2.61-4.42) | (3.12-5.45) | (3.79-7.05) | (4.31-8.47) | (4.87-10.1) | (5.50-12.0) | (6.40-15.0) | (7.13-17.5) |
| 6-hr | 2.40 | 3.08 | 4.06 | 4.98 | 6.38 | 7.57 | 8.92 | 10.5 | 12.8 | 14.8 |
| | (1.84-3.12) | (2.32-3.83) | (3.11-5.21) | (3.79-6.54) | (4.70-8.65) | (5.43-10.6) | (6.22-12.8) | (7.12-15.4) | (8.42-19.6) | (9.49-23.1) |
| 12-hr | 2.71 (2.09-3.50) | 3.52 (2.65-4.32) | 4.67 (3.60-5.95) | 5.77 (4.41-7.53) | 7.46 (5.53-10.1) | 8.91 (6.43-12.4) | 10.6 (7.42-15.0) | 12.6 (8.55-18.3) | 15.6 (10.2-23.6) | 18.1 (11.6-28.1) |
| 24-hr | 3.05 | 3.99 | 5.31 | 6.60 | 8.56 | 10.3 | 12.2 | 14.6 | 18.2 | 21.2 |
| | (2.36-3.91) | (3.01-4.85) | (4.11-6.73) | (5.06-8.55) | (6.38-11.5) | (7.44-14.2) | (8.61-17.3) | (9.96-21.1) | (12.0-27.3) | (13.7-32.7) |
| 2-day | 3.46 | 4.54 | 6.07 | 7.54 | 9.78 | 11.7 | 14.0 | 16.6 | 20.7 | 24.1 |
| | (2.70-4.42) | (3.45-5.50) | (4.72-7.64) | (5.81-9.71) | (7.32-13.0) | (8.53-16.1) | (9.87-19.6) | (11.4-23.9) | (13.7-30.9) | (15.6-37.0) |
| 3-day | 3.77 | 4.93 | 6.58 | 8.15 | 10.5 | 12.6 | 15.0 | 17.7 | 21.9 | 25.5 |
| | (2.94-4.80) | (3.76-5.95) | (5.13-8.25) | (6.30-10.5) | (7.91-14.0) | (9.20-17.2) | (10.6-21.0) | (12.2-25.5) | (14.6-32.7) | (16.5-39.0) |
| 4-day | 4.02 | 5.22 | 6.96 | 8.60 | 11.1 | 13.2 | 15.6 | 18.5 | 22.7 | 26.3 |
| | (3.14-5.10) | (4.01-6.32) | (5.45-8.71) | (6.67-11.0) | (8.33-14.7) | (9.65-18.0) | (11.1-21.8) | (12.7-26.4) | (15.1-33.7) | (17.0-40.0) |
| 7-day | 4.60 | 5.90 | 7.80 | 9.56 | 12.2 | 14.4 | 16.9 | 19.7 | 23.9 | 27.5 |
| | (3.62-5.81) | (4.57-7.15) | (6.14-9.73) | (7.44-12.2) | (9.19-16.1) | (10.6-19.5) | (12.0-23.5) | (13.7-28.1) | (16.0-35.5) | (17.9-41.7) |
| 10-day | 5.09 | 6.45 | 8.48 | 10.3 | 13.1 | 15.3 | 17.9 | 20.7 | 24.9 | 28.4 |
| | (4.01-6.41) | (5.03-7.83) | (6.69-10.6) | (8.06-13.1) | (9.87-17.1) | (11.3-20.7) | (12.7-24.7) | (14.4-29.5) | (16.6-36.7) | (18.5-42.9) |
| 20-day | 6.56 | 8.08 | 10.5 | 12.5 | 15.5 | 17.8 | 20.4 | 23.1 | 27.1 | 30.4 |
| | (5.19-8.21) | (6.40-9.88) | (8.31-13.0) | (9.81-15.8) | (11.7-20.1) | (13.1-23.9) | (14.6-28.0) | (16.1-32.8) | (18.2-39.8) | (19.9-45.8) |
| 30-day | 7.76 | 9.40 | 12.0 | 14.3 | 17.4 | 19.8 | 22.4 | 25.1 | 29.0 | 32.1 |
| | (6.16-9.66) | (7.51-11.5) | (9.61-14.9) | (11.2-17.9) | (13.2-22.6) | (14.6-26.5) | (16.1-30.7) | (17.6-35.4) | (19.5-42.4) | (21.0-48.1) |
| 45-day | 9.40 (7.48-11.7) | 11.2 (9.04-13.8) | 14.2 (11.4-17.6) | 16.7 (13.2-20.9) | 20.1 (15.3-26.0) | 22.7 (16.8-30.2) | 25.4 (18.3-34.8) | 28.2 (19.8-39.7) | 32.1 (21.7-46.8) | 35.1 (23.1-52.5) |
| 60-day | 10.8 | 12.8 | 16.2 | 18.9 | 22.6 | 25.4 | 28.2 | 31.1 | 35.0 | 38.0 |
| | (8.65-13.4) | (10.4-15.8) | (13.0-19.9) | (14.9-23.6) | (17.2-29.1) | (18.8-33.6) | (20.3-38.4) | (21.8-43.6) | (23.7-50.8) | (25.0-56.7) |

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

Deals to Tea

PROPOSED CONDITIONS TIME OF CONCENTRATION TABLE C1-C-1

| Subbasin | | DA-P1 | DA-P2 | DA-P3 | DA-P4 | DA-P5 | DA-P6 | DA-P7 | DA-P8 | DA-P9 | DA-P10 | OS-1 | OS-2 |
|------------------|---------|---------|-----------|-----------|---------|----------|---------|---------|-----------|-----------|-----------|---------|----------|
| Area | saft | 325,402 | 2,889,729 | 1,462,482 | 485,705 | 903,182 | 754,710 | 292,836 | 1.005.166 | 1,565,743 | 1,553,862 | 976,804 | 338429 |
| | | | | , , | , | | , | | | , , | , , | , | |
| Area | ac. | 7.47 | 66.34 | 33.57 | 11.15 | 20.73 | 17.33 | 6.72 | 23.08 | 35.94 | 35.67 | 22.42 | 7.77 |
| Area | sqmi | 0.01167 | 0.10365 | 0.05246 | 0.01742 | 0.03240 | 0.02707 | 0.01050 | 0.03606 | 0.05616 | 0.05574 | 0.03504 | 0.01214 |
| Impervious | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 599276 | 386512 | 86500.00 |
| Impervious | | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 0% | 39% | 40% | 26% |
| Pervious | Cn | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 79 | 79 | 79 |
| Composite | Cn | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 86 | 87 | 84 |
| Sheet Flow | | | | | | | | | | | | | |
| Slope | in/in | 0.0400 | 0.0600 | 0.0600 | 0.0600 | 0.2000 | 0.2000 | 0.2000 | 0.2000 | 0.0100 | 0.0061 | 0.0100 | 0.0130 |
| Length | ft. | 100 | 300 | 300 | 100 | 100 | 100 | 50 | 100 | 100 | 300 | 300 | 300 |
| Roughness | n | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 | 0.15 |
| Time | hr. | 0.11 | 0.22 | 0.22 | 0.09 | 0.06 | 0.06 | 0.03 | 0.06 | 0.19 | 0.56 | 0.46 | 0.41 |
| Shallow Co | ncentra | ated | | | | | | | | | | | |
| Slope | in/in | 1.6349 | 0.1530 | 0.0957 | 0.2015 | 0.1666 | 0.2000 | 0.2000 | 0.2213 | 0.0258 | 0.0061 | 0.0100 | 0.0560 |
| Length | ft. | 18.35 | 248.30 | 125.37 | 138.98 | 72.03 | 29.60 | 30.00 | 45.19 | 387.44 | 1186.00 | 1116.00 | 320.00 |
| Paved? | p/u | u | u | u | u | u | u | u | u | u | u | u | u |
| Time | hr. | 0.00 | 0.01 | 0.01 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.04 | 0.26 | 0.19 | 0.02 |
| Shallow Co | ncentro | ated | | | | | | | | | | | |
| Slope | in/in | | | | | | | | | 0.0341 | | | |
| Length | ft. | | | | | | | | | 351.79 | | | |
| Paved? | p/u | | | | | | | | | u | u | u | u |
| Time | hr. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.03 | 0.00 | 0.00 | 0.00 |
| Channel Flo | w | | | | | | | | | | | | |
| Slope | in/in | 0.00 | 0.07 | 0.11 | 0.19 | 0.00 | 0.01 | 0.01 | 0.02 | 0.00 | 0 | 0 | 0 |
| Length | ft. | 0 | 2179.34 | 1474.72 | 653.53 | 1291.337 | 2315.48 | 722.98 | 3058.68 | 0 | 0 | 0 | 0 |
| Velocity | fps | 0 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 0 | 0 | 0 | 0 |
| Time | hr. | 0.00 | 0.12 | 0.08 | 0.04 | 0.07 | 0.13 | 0.04 | 0.17 | 0.00 | 0.00 | 0.00 | 0.00 |
| Summary | | | | | | | | | | | | | |
| , Travel Time | hr. | 0.11 | 0.36 | 0.31 | 0.13 | 0.13 | 0.19 | 0.07 | 0.23 | 0.23 | 0.82 | 0.65 | 0.44 |
| Tc | min. | 10.00 | 21.35 | 18.77 | 10.00 | 10.00 | 11.23 | 10.00 | 13.74 | 13.91 | 49.21 | 39.03 | 26.16 |
| Lag Time | min. | 6.00 | 12.81 | 11.26 | 6.00 | 6.00 | 6.74 | 6.00 | 8.24 | 8.35 | 29.52 | 23.42 | 15.70 |

POST-DEVELOPMENT SURFACE WATER IMPOUNDMENTS DESIGN PARAMETERS

South Pond - Proposed Condition

| Outfall Structures | | | | | | | | | | |
|--------------------|-----------------|----------------------------|------------------------|----------------------------|--------------------------------|--|--|--|--|--|
| Outfall Number | Outfall Type | Length or Diameter (ft) | Orifice Coefficient | Critical Elevation type | Critical Elevation (msl) | | | | | |
| 1 | Orifice | 1 | 0.66 | Flowline | 698.0 | | | | | |
| 2 | Orifice | 4 | 0.66 | Flowline | 703.0 | | | | | |

| | | Ι | Pond Geome | etry Summary | | | |
|----------------|----------------------|-------------------|----------------------------------|----------------------------------|---------------------------------|---------------------------------|--------------------------------|
| Stage (msl) | Pond Area (ac) | Pond Area (sf) | Sectional Volume (cu. Ft.) | Cumulative Volume (cu.ft.) | Outfall 1 Rating (cfs) | Outfall 2 Rating (cfs) | Cumulative Outflow (cfs) |
| 668 | 0.141 | 6,136 | - | - | | | |
| 670 | 0.203 | 8,824 | 17,648 | 17,648 | | | |
| 672 | 0.278 | 12,091 | 24,183 | 41,831 | | | |
| 674 | 0.370 | 16,103 | 32,206 | 74,036 | | | |
| 676 | 0.467 | 20,350 | 40,701 | 114,737 | | | |
| 678 | 0.554 | 24,144 | 48,287 | 163,024 | | | |
| 680 | 0.648 | 28,207 | 56,415 | 219,439 | | | |
| 682 | 0.752 | 32,768 | 65,537 | 284,976 | | | |
| 684 | 0.854 | 37,192 | 74,384 | 359,360 | | | |
| 686 | 1.869 | 81,409 | 162,819 | 522,178 | | | |
| 688 | 2.187 | 95,274 | 190,549 | 712,727 | | | |
| 690 | 2.403 | 104,670 | 209,341 | 922,068 | | | |
| 692 | 2.536 | 110,468 | 220,936 | 1,143,004 | | | |
| 694 | 2.670 | 116,318 | 232,637 | 1,375,640 | | | |
| 696 | 2.934 | 127,805 | 255,610 | 1,631,251 | | | |
| 698 | 3.230 | 140,677 | 281,354 | 1,912,605 | 0 | | 0.0 |
| 700 | 3.527 | 153,649 | 307,298 | 2,219,903 | 5.1 | | 5.1 |
| 702 | 3.737 | 162,784 | 325,567 | 2,545,470 | 7.8 | | 7.8 |
| 703 | 4.167 | 181,528 | 181,528 | 2,726,998 | 8.8 | | 8.8 |
| 704 | 4.363 | 190,065 | 190,065 | 2,917,063 | 9.8 | | 9.8 |
| 706 | 4.643 | 202,267 | 404,533 | 3,321,596 | 11.4 | 66.6 | 78.0 |
| 708 | 4.925 | 214,542 | 429,083 | 3,750,680 | 12.8 | 115.3 | 128.1 |
| 709 | 5.111 | 222,618 | 222,618 | 3,973,298 | 13.5 | 133.1 | 146.6 |

Civil & Environmental Consultants, Inc.

🛄 Summary Results for Reservoir "Pond"

Project: Beck with Southern Outfall Simulation Run: PR 025-YR

Reservoir: Pond

 Start of Run:
 01Jan2001, 00:01

 End of Run:
 02Jan2001, 00:02
 Compute Time:DATA CHANGED, RECOMPUTE Control Specifications: TypeIII-24Hr

Basin Model: Proposed Beck Meteorologic Model: 025-YR

Volume Units: O IN
 ACRE-FT

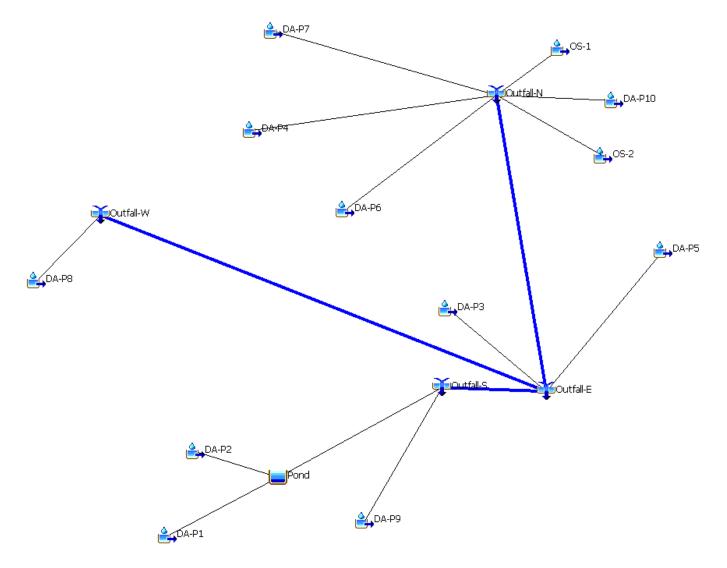
Computed Results

| Peak Inflow: | 302.3 (CFS) | |
|-----------------|------------------|-----|
| Peak Discharge: | 24.0 (CFS) | 1 |
| Inflow Volume: | 44.3 (ACRE-FT) | - a |
| Discharge Volum | e:17.8 (ACRE-FT) | 1 |

Date/Time of Peak Inflow: 01Jan2001, 10:05 Date/Time of Peak Discharge:01Jan2001, 13:43 Peak Storage: 67.6 (ACRE-FT) Peak Elevation: 705.0 (FT)

Summary Results for Reservoir "Pond" Project: Beck with Southern Outfall Simulation Run: PR 100-YR Reservoir: Pond Start of Run: 01Jan2001, 00:01 Basin Model: Proposed Beck Meteorologic Model: 100-YR End of Run: 02Jan2001, 00:02 Compute Time:DATA CHANGED, RECOMPUTE Control Specifications: TypeIII-24Hr Volume Units: O IN
 ACRE-FT Computed Results Peak Inflow: 445.8 (CFS) Date/Time of Peak Inflow: 01Jan2001, 10:05 Peak Discharge: 75.5 (CFS) Date/Time of Peak Discharge:01Jan2001, 10:58 Inflow Volume: 66.4 (ACRE-FT) Peak Storage: 71.6 (ACRE-FT) Discharge Volume:39.6 (ACRE-FT) Peak Elevation: 705.9 (FT)

PROPOSED CONDITION HEC-HMS SCHEMATIC



| Project Description | | |
|------------------------------------|--------------------------|--|
| Solve For | Discharge Coefficient | |
| Input Data | | |
| Discharge | 11.40 cfs | |
| Headwater Elevation | 705.90 ft | |
| Centroid Elevation | 698.50 ft | |
| Tailwater Elevation | 698.00 ft | |
| Diameter | 12.0 in | |
| Results | | |
| Discharge Coefficient | 0.665 | |
| Headwater Height Above Centroid | 7.40 ft | |
| Tailwater Height Above Centroid | -0.50 ft | |
| Flow Area | 0.8 ft ² | |
| Velocity | 14.51 ft/s | |

Peak Velocity Calculation for Pond Outlet 1

| Peak Velocity Calculation for Pond Outlet 2 | | | | | |
|---|--------------------------|--|--|--|--|
| Project Description | | | | | |
| Solve For | Discharge Coefficient | | | | |
| nput Data | | | | | |
| Discharge | 66.60 cfs | | | | |
| Headwater Elevation | 705.90 ft | | | | |
| Centroid Elevation | 705.00 ft | | | | |
| Tailwater Elevation | 703.00 ft | | | | |
| Diameter | 48.0 in | | | | |
| Results | | | | | |
| Discharge Coefficient | 0.696 | | | | |
| Headwater Height Above Centroid | 0.90 ft | | | | |
| Tailwater Height Above Centroid | -2.00 ft | | | | |
| Flow Area | 12.6 ft ² | | | | |
| Velocity | 5.30 ft/s | | | | |

HYDROLOGIC ANALYSIS

25-YEAR, 24-YEAR STORM EVENT 100-YEAR, 24-YEAR STORM EVENT

Type III, 24-hour Storm, 25 Year Event - Proposed Condition Project: Beck with Southern Outfall Simulation Run: PR 025-YR

| | Project: Beck V | vith Southern Outrali Simulation | RUN: PR 025-YR | |
|--|--|----------------------------------|--|--------------------------------|
| | Start of Run: 01Jan. End of Run: 02Jan. Compute Time:08Sep | 2001, 00:02 Meteorologic | Proposed Beck Model: 025-YR fications:TypeIII-24Hr | |
| Show Elements: All Elements $ \smallsetminus $ | | Volume Units: O IN () ACRE-FT | | Sorting: Watershed Explorer $$ |
| Hydrologic | Drainage Area | Peak Discharge | Time of Peak | Volume |
| Element | (MI2) | (CFS) | | (ACRE-FT) |
| DA-P10 | 0.1 | 93.1 | 1 January 2001, 10:23 | 21.2 |
| OS-1 | 0.0 | 67.5 | 1 January 2001, 10:16 | 13.5 |
| DA-P6 | 0.0 | 89.8 | 1 January 2001, 10:01 | 10.8 |
| DA-P4 | 0.0 | 59.1 | 1 January 2001, 10:00 | 6.7 |
| OS-2 | 0.0 | 27.8 | 1 January 2001, 10:09 | 4.5 |
| DA-P7 | 0.0 | 35.6 | 1 January 2001, 10:00 | 4.0 |
| Outfall-N | 0.2 | 291.2 | 1 January 2001, 10:02 | 60.7 |
| DA-P2 | 0.1 | 274.2 | 1 January 2001, 10:06 | 39.8 |
| DA-P1 | 0.0 | 39.6 | 1 January 2001, 10:00 | 4.5 |
| Pond | 0.1 | 24.0 | 1 January 2001, 13:43 | 17.8 |
| DA-P9 | 0.1 | 175.8 | 1 January 2001, 10:02 | 22.3 |
| Outfall-S | 0.2 | 183.0 | 1 January 2001, 10:02 | 40.1 |
| South to East | 0.2 | 183.0 | 1 January 2001, 10:08 | 40.0 |
| E to N Reach | 0.2 | 291.2 | 1 January 2001, 10:05 | 60.7 |
| DA-P3 | 0.1 | 146.6 | 1 January 2001, 10:05 | 20.2 |
| DA-P8 | 0.0 | 112.5 | 1 January 2001, 10:02 | 13.9 |
| Outfall-W | 0.0 112.5 | | 1 January 2001, 10:02 | 13.9 |
| W to E Reach | 0.0 | 112.5 | 1 January 2001, 10:20 | 13.8 |
| DA-P5 | 0.0 | 109.9 | 1 January 2001, 10:00 | 12.5 |
| Outfall-E | 0.5 | 729.5 | 1 January 2001, 10:05 | 147.1 |

Type III, 24-hour Storm, 100 Year Event - Proposed Condition Project: Beck with Southern Outfall Simulation Run: PR 100-YR

| | Start of Run: 01Jan: End of Run: 02Jan: Compute Time:08Sep | 2001, 00:02 Meteorologic M | Proposed Beck Model: 100-YR cations:TypeIII-24Hr | |
|--|--|------------------------------|--|--------------------------------|
| Show Elements: All Elements $ \smallsetminus $ | | Volume Units: O IN (ACRE-FT | | Sorting: Watershed Explorer $$ |
| Hydrologic Element | Drainage Area (MI2) | Peak Discharge (CFS) | Time of Peak | Volume (ACRE-FT) |
| DA-P10 | 0.1 | 138.7 | 1 January 2001, 10:23 | 31.7 |
| OS-1 | 0.0 | 100.1 | 1 January 2001, 10:16 | 20.2 |
| DA-P6 | 0.0 | 131.7 | 1 January 2001, 10:00 | 16.0 |
| DA-P4 | 0.0 | 87.0 | 1 January 2001, 10:00 | 10.0 |
| OS-2 | 0.0 | 41.7 | 1 January 2001, 10:09 | 6.8 |
| DA-P7 | 0.0 | 52.4 | 1 January 2001, 10:00 | 6.1 |
| Outfall-N | 0.2 | 431.4 | 1 January 2001, 10:02 | 90.7 |
| DA-P2 | 0.1 | 404.4 | 1 January 2001, 10:06 | 59.7 |
| DA-P1 | 0.0 | 58.3 | 1 January 2001, 10:00 | 6.7 |
| Pond | 0.1 | 75.5 | 1 January 2001, 10:58 | 39.6 |
| DA-P9 | 0.1 | 257.9 | 1 January 2001, 10:02 | 33.1 |
| Outfall-S | 0.2 | 267.1 | 1 January 2001, 10:02 | 72.7 |
| South to East | 0.2 | 267.1 | 1 January 2001, 10:08 | 72.6 |
| E to N Reach | 0.2 | 431.4 | 1 January 2001, 10:05 | 90.6 |
| DA-P3 | 0.1 | 216.0 | 1 January 2001, 10:05 | 30.2 |
| DA-P8 | 0.0 | 165.7 | 1 January 2001, 10:02 | 20.8 |
| Outfall-W | 0.0 | 165.7 | 1 January 2001, 10:02 | 20.8 |
| W to E Reach | 0.0 | 165.7 | 1 January 2001, 10:20 | 20.7 |
| DA-P5 | 0.0 | 161.8 | 1 January 2001, 10:00 | 18.7 |
| Outfall-E | 0.5 | 1075.8 | 1 January 2001, 10:05 | 232.8 |

BECK LANDFILL APPENDIX C1-D FACILITY SURFACE WATER DRAINAGE REPORT PERIMETER DRAINAGE BERM DESIGN

Includes pages C1-D-1 through C1-D-5

Revised January 2023



NARRATIVE

<u>30 TAC §330</u>.305

This appendix presents the design of Beck Landfill perimeter drainage channels and detention pond in accordance with §330.305(a)-(d).

PERIMETER DRAINAGE PLAN

Drawing C1-2 depicts the perimeter drainage system and detention pond location for Beck Landfill. The typical section for the perimeter drainage berms is shown on Figure C1-2A and the detention pond details are shown on Figure C3-1 and C3-2. The perimeter berm hydraulic analysis is included for the 25-year rainfall event. Profiles for the perimeter berms are shown on Figures C1-2A through C1-2F.

PERIMETER BERM DESIGN SUMMARY

The perimeter berms are designed for the peak discharge resulting from the 25-year storm event while maintaining velocities between 2 fps and 6 fps. The typical perimeter berm has 2:1 sideslopes, two feet top width, and is two feet high. The berm slope is 2%. The largest area contributing to a perimeter berm occurs for Berm 8 (See Figure C1-2) and is 6.5 acres. The Rational Method and methods and parameters included in the TxDOT Hydraulic *Design Manual*, September 2019 will be used to calculate the peak flow anticipated in this worst-case perimeter berm.

The rational formula estimates the peak rate of runoff at a specific location in a watershed as a function of the drainage area, runoff coefficient, and mean rainfall intensity for a duration equal to the time of concentration. The rational formula is:

Q=CIA Where:

Q = maximum rate of runoff (cfs)

C = runoff coefficient

I = average rainfall intensity (in./hr.)

A = drainage area (ac)

Runoff Coefficient (C)

The following table from the TxDOT manual lists appropriate run-off coefficients for various uses and surface conditions. Steep grassed slopes was chosen as the most appropriate for the landfill final cover, which corresponds to a coefficient of 0.70.

Chapter 4 — Hydrology

Section 12 - Rational Method

| Table 4-10: Runoff Coefficients for Urban Watersheds | | | | | |
|--|--------------------|--|--|--|--|
| Type of drainage area | Runoff coefficient | | | | |
| Business: | | | | | |
| Downtown areas | 0.70-0.95 | | | | |
| Neighborhood areas | 0.30-0.70 | | | | |
| Residential: | | | | | |
| Single-family areas | 0.30-0.50 | | | | |
| Multi-units, detached | 0.40-0.60 | | | | |
| Multi-units, attached | 0.60-0.75 | | | | |
| Suburban | 0.35-0.40 | | | | |
| Apartment dwelling areas | 0.30-0.70 | | | | |
| Industrial: | | | | | |
| Light areas | 0.30-0.80 | | | | |
| Heavy areas | 0.60-0.90 | | | | |
| Parks, cemeteries | 0.10-0.25 | | | | |
| Playgrounds | 0.30-0.40 | | | | |
| Railroad yards | 0.30-0.40 | | | | |
| Unimproved areas: | | | | | |
| Sand or sandy loam soil, 0-3% | 0.15-0.20 | | | | |
| Sand or sandy loam soil, 3-5% | 0.20-0.25 | | | | |
| Black or loessial soil, 0-3% | 0.18-0.25 | | | | |
| Black or loessial soil, 3-5% | 0.25-0.30 | | | | |
| Black or loessial soil, > 5% | 0.70-0.80 | | | | |
| Deep sand area | 0.05-0.15 | | | | |
| Steep grassed slopes | 0.70 | | | | |
| Lawns: | | | | | |
| Sandy soil, flat 2% | 0.05-0.10 | | | | |
| Sandy soil, average 2-7% | 0.10-0.15 | | | | |
| Sandy soil, steep 7% | 0.15-0.20 | | | | |
| Heavy soil, flat 2% | 0.13-0.17 | | | | |
| Heavy soil, average 2-7% | 0.18-0.22 | | | | |

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Rainfall Intensity (I)

The rainfall intensity (I) is the average rainfall rate in in./hr. for a specific rainfall duration and a selected frequency. The duration is assumed to be equal to the time of concentration. The intensity was taken from the following table from <u>2018 NOAA Atlas 14 Precipitation-Frequency Atlas of the United States, Volume 11, Version 2.0: Texas, assuming a time of concentration and storm duration of ten minutes. From the table the 25-year intensity is 8.8 in/hr and the 100-year intensity is 11.1 in/hr.</u>



NOAA Atlas 14, Volume 11, Version 2 Location name: Schertz, Texas, USA* Latitude: 29.5483°, Longitude: -98.2639° Elevation: 706.71 ft** * source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orian Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

| | | | | Avera | ge recurren | ce interval (y | years) | | | |
|----------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|--------------|
| Duration | 1 | 2 | 5 | 10 | 25 | 50 | 100 | 200 | 500 | 1000 |
| 5-min | 5.32 | 6.29 | 7.86 | 9.18 | 11.0 | 12.4 | 13.9 | 15.4 | 17.5 | 19.2 |
| | (4.03-7.02) | (4.80-8.21) | (5.99-10.3) | (6.89-12.2) | (8.00-15.1) | (8.80-17.5) | (9.58-20.1) | (10.4-22.9) | (11.4-27.0) | (12.1-30.3) |
| 10-min | 4.23 | 5.01 | 6.28 | 7.34 | 8.81 | 9.97 | 11.1 | 12.3 | 13.8 | 15.0 |
| | (3.20-5.59) | (3.82-6.54) | (4.78-8.24) | (5.51-9.77) | (6.42-12.1) | (7.07-14.1) | (7.68-16.1) | (8.27-18.3) | (8.99-21.3) | (9.50-23.7) |
| 15-min | 3.61 | 4.24 | 5.26 | 6.12 | 7.30 | 8.22 | 9.17 | 10.2 | 11.5 | 12.6 |
| | (2.73-4.77) | (3.23-5.53) | (4.00-6.90) | (4.59-8.15) | (5.31-10.0) | (5.82-11.6) | (6.32-13.3) | (6.84-15.1) | (7.49-17.8) | (7.98-19.9) |
| 30-min | 2.54 | 2.98 | 3.68 | 4.27 | 5.08 | 5.70 | 6.35 | 7.05 | 8.05 | 8.86 |
| | (1.92-3.36) | (2.27-3.89) | (2.80-4.84) | (3.21-5.69) | (3.69-6.96) | (4.03-8.04) | (4.38-9.20) | (4.74-10.5) | (5.23-12.4) | (5.61-14.0) |
| 60-min | 1.64 | 1.93 | 2.42 | 2.82 | 3.39 | 3.81 | 4.27 | 4.78 | 5.53 | 6.14 |
| | (1.24-2.16) | (1.48-2.52) | (1.84-3.17) | (2.12-3.76) | (2.45-4.63) | (2.69-5.37) | (2.94-6.19) | (3.22-7.12) | (3.59-8.53) | (3.89-9.70) |
| 2-hr | 0.974 | 1.19 | 1.52 | 1.81 | 2.23 | 2.57 | 2.94 | 3.37 | 3.99 | 4.52 |
| | (0.740-1.28) | (0.902-1.52) | (1.16-1.98) | (1.37-2.40) | (1.63-3.04) | (1.83-3.61) | (2.04-4.24) | (2.27-4.98) | (2.60-6.13) | (2.87-7.10) |
| 3-hr | 0.703 | 0.877 | 1.14 | 1.37 | 1.72 | 2.01 | 2.34 | 2.71 | 3.26 | 3.73 |
| | (0.536-0.920) | (0.663-1.11) | (0.869-1.47) | (1.04-1.81) | (1.26-2.35) | (1.44-2.82) | (1.62-3.36) | (1.83-4.00) | (2.13-4.99) | (2.37-5.84) |
| 6-hr | 0.401 | 0.514 | 0.678 | 0.832 | 1.07 | 1.26 | 1.49 | 1.75 | 2.15 | 2.48 |
| | (0.307-0.522) | (0.387-0.639) | (0.520-0.870) | (0.632-1.09) | (0.786-1.44) | (0.907-1.76) | (1.04-2.13) | (1.19-2.57) | (1.41-3.27) | (1.58-3.86) |
| 12-hr | 0.225 | 0.292 | 0.387 | 0.479 | 0.619 | 0.739 | 0.879 | 1.04 | 1.29 | 1.51 |
| | (0.173-0.290) | (0.220-0.358) | (0.299-0.494) | (0.366-0.625) | (0.459-0.835) | (0.533-1.03) | (0.616-1.25) | (0.710-1.52) | (0.849-1.96) | (0.965-2.33 |
| 24-hr | 0.127 | 0.166 | 0.221 | 0.275 | 0.357 | 0.428 | 0.510 | 0.608 | 0.757 | 0.885 |
| | (0.098-0.163) | (0.126-0.202) | (0.171-0.280) | (0.211-0.356) | (0.266-0.478) | (0.310-0.591) | (0.359-0.721) | (0.415-0.880) | (0.500-1.14) | (0.570-1.36 |
| 2-day | 0.072 | 0.095 | 0.126 | 0.157 | 0.204 | 0.244 | 0.291 | 0.346 | 0.430 | 0.502 |
| | (0.056-0.092) | (0.072-0.115) | (0.098-0.159) | (0.121-0.202) | (0.152-0.272) | (0.178-0.335) | (0.206-0.409) | (0.238-0.499) | (0.285-0.644) | (0.324-0.770 |
| 3-day | 0.052 | 0.068 | 0.091 | 0.113 | 0.146 | 0.175 | 0.208 | 0.246 | 0.305 | 0.354 |
| | (0.041-0.067) | (0.052-0.083) | (0.071-0.115) | (0.088-0.145) | (0.110-0.195) | (0.128-0.239) | (0.147-0.291) | (0.170-0.354) | (0.202-0.454) | (0.229-0.54 |
| 4-day | 0.042 | 0.054 | 0.073 | 0.090 | 0.115 | 0.138 | 0.163 | 0.192 | 0.236 | 0.274 |
| | (0.033-0.053) | (0.042-0.066) | (0.057-0.091) | (0.069-0.115) | (0.087-0.153) | (0.101-0.188) | (0.116-0.227) | (0.132-0.275) | (0.157-0.352) | (0.177-0.417 |
| 7-day | 0.027 | 0.035 | 0.046 | 0.057 | 0.073 | 0.086 | 0.101 | 0.117 | 0.143 | 0.164 |
| | (0.022-0.035) | (0.027-0.043) | (0.037-0.058) | (0.044-0.073) | (0.055-0.096) | (0.063-0.116) | (0.072-0.140) | (0.081-0.168) | (0.095-0.211) | (0.106-0.248 |
| 10-day | 0.021 | 0.027 | 0.035 | 0.043 | 0.054 | 0.064 | 0.074 | 0.086 | 0.104 | 0.118 |
| | (0.017-0.027) | (0.021-0.033) | (0.028-0.044) | (0.034-0.055) | (0.041-0.071) | (0.047-0.086) | (0.053-0.103) | (0.060-0.123) | (0.069-0.153) | (0.077-0.179 |
| 20-day | 0.014 | 0.017 | 0.022 | 0.026 | 0.032 | 0.037 | 0.042 | 0.048 | 0.057 | 0.063 |
| | (0.011-0.017) | (0.013-0.021) | (0.017-0.027) | (0.020-0.033) | (0.024-0.042) | (0.027-0.050) | (0.030-0.058) | (0.034-0.068) | (0.038-0.083) | (0.041-0.09 |
| 30-day | 0.011 | 0.013 | 0.017 | 0.020 | 0.024 | 0.028 | 0.031 | 0.035 | 0.040 | 0.045 |
| | (0.009-0.013) | (0.010-0.016) | (0.013-0.021) | (0.016-0.025) | (0.018-0.031) | (0.020-0.037) | (0.022-0.043) | (0.024-0.049) | (0.027-0.059) | (0.029-0.06 |
| 45-day | 0.009 (0.007-0.011) | 0.010 (0.008-0.013) | 0.013 (0.011-0.016) | 0.015 (0.012-0.019) | 0.019 (0.014-0.024) | 0.021 (0.016-0.028) | 0.024 (0.017-0.032) | 0.026 (0.018-0.037) | 0.030 (0.020-0.043) | 0.033 |
| 60-day | 0.008 | 0.009 | 0.011 | 0.013 | 0.016 (0.012-0.020) | 0.018 | 0.020 | 0.022 | 0.024 | 0.026 |

For the worst-case perimeter berm:

$$Q_{25} = CIA$$

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$$Q_{100} = CIA$$

= (0.7)(11.1 in/hr)(6.52 Acres)
= 50.7 cfs

The Flowmaster software package was utilized to determine flow depth for each of the perimeter berms and the table below lists each berm, the contributing area, and the calculated 25-year flow depth.

Beck Landfill Perimter Berm Design Calculations

| C= | 0.7 Steep grassed slopes |
|----|--------------------------|
|----|--------------------------|

i= 8.8 (in/hr) (25 yr return period)

| | | | РЕАК | Реак | FLOW |
|------|--------------|--------------|-------|----------|-------|
| | CONTRIBUTING | CONTRIBUTING | FLOW | Velocity | DEPTH |
| BERM | AREA (SF) | AREA (AC) | (CFS) | (FT/SEC) | (FT) |
| 1 | 137,456 | 3.16 | 19.44 | 5.41 | 1.1 |
| 2 | 129,787 | 2.98 | 18.35 | 5.33 | 1.1 |
| 3 | 99,459 | 2.28 | 14.06 | 4.99 | 1.0 |
| 4 | 206,752 | 4.75 | 29.24 | 5.99 | 1.3 |
| 5 | 102,102 | 2.34 | 14.44 | 5.02 | 1.0 |
| 6A | 94,439 | 2.17 | 13.36 | 4.93 | 1.0 |
| 6B | 110,462 | 2.54 | 15.62 | 5.12 | 1.0 |
| 7A | 39,377 | 0.90 | 5.57 | 3.96 | 0.7 |
| 7B | 51,131 | 1.17 | 7.23 | 4.22 | 0.8 |
| 7C | 27,391 | 0.63 | 3.87 | 3.62 | 0.6 |
| 8 | 283,991 | 6.52 | 40.16 | 6.49 | 1.4 |
| 9 | 38,656 | 0.89 | 5.47 | 3.94 | 0.7 |
| 10A | 122,091 | 2.80 | 17.27 | 5.25 | 1.0 |
| 10B | 93,610 | 2.15 | 13.24 | 4.92 | 0.9 |

Notes: 1) Flow depths and velocities calculated using FlowMaster Hydraulic Calculator

2) Peak flow calculated using Rational Method with factors shown in the table

| | Worst-Case | Perimeter Berm |
|-----------------------|---------------------|----------------|
| Project Description | | |
| Friction Method | Manning Formula | |
| Solve For | Normal Depth | |
| Input Data | | |
| Roughness Coefficient | 0.025 | |
| Channel Slope | 0.020 ft/ft | |
| Left Side Slope | 2.000 H:V | |
| Right Side Slope | 4.000 H:V | |
| Discharge | 40.16 cfs | |
| Results | | |
| Normal Depth | 1.4 ft | |
| Flow Area | 6.2 ft ² | |
| Wetted Perimeter | 9.1 ft | |
| Hydraulic Radius | 0.7 ft | |
| Top Width | 8.62 ft | |
| Critical Depth | 1.6 ft | |
| Critical Slope | 0.011 ft/ft | |
| Velocity | 6.49 ft/s | |
| Velocity Head | 0.65 ft | |
| Specific Energy | 2.09 ft | |
| Froude Number | 1.349 | |
| Flow Type | Supercritical | |
| GVF Input Data | | |
| Downstream Depth | 0.0 ft | |
| Length | 0.0 ft | |
| Number Of Steps | 0 | |
| GVF Output Data | | |
| Upstream Depth | 0.0 ft | |
| Profile Description | N/A | |
| Profile Headloss | 0.00 ft | |
| Downstream Velocity | Infinity ft/s | |
| Upstream Velocity | Infinity ft/s | |
| Normal Depth | 1.4 ft | |
| Critical Depth | 1.6 ft | |
| Channel Slope | 0.020 ft/ft | |
| Critical Slope | 0.011 ft/ft | |

Worst-Case Perimeter Berm

DETENTION POND ANALYSIS

The rainfall depth, duration, and frequency relationships for the storm event for the facility was taken from the <u>2018 NOAA Atlas 14 Precipitation-Frequency Atlas of the United States, Volume 11, Version 2.0: Texas</u>. Return periods of 25 and 100 years and a duration of 24 hours was used for the design storm. The synthetic rainfall distribution is the NRCS 24-hour Type III storm. The rainfall data for the facility located in Guadalupe County, Texas is shown on page C1-C-7. The details for the detention pond are shown on Figure C3-1 and the pond outlet design and elevation-stage-storage tables are shown on Page C1-C-9.

BECK LANDFILL

APPENDIX C1-E FACILITY SURFACE WATER DRAINAGE REPORT FINAL COVER DRAINAGE STRUCTURE DESIGN

Includes pages C1-E-1 through C1-E-11



NARRATIVE

30 TAC §§330.303 AND 330.305 This appendix presents the supporting documentation for evaluation of the final cover erosion layer and drainage structures.

FINAL COVER PLAN

The final cover plans depict the proposed final cover drainage system, which consists of a series of benches and downchutes designed to convey the flow of surface water produced during the 25-year storm event. The locations of the sideslope benches and downchutes are shown on Drawing C1-2. Final cover details are included in Attachment D3.

EROSION LAYER EVALUATION

The erosion layer evaluation is based on the Universal Soil Loss Equation (USLE) following Natural Resource Soil Conservation Service (NRCS) procedures. The evaluation is based on a 25-year storm event. The proposed 12-inch thick erosion layer is shown to provide sufficient erosion protection. Calculations are included beginning on page C1-E-2.

DRAINAGE BENCH DESIGN

The drainage bench design calculations are presented for the typical proposed bench flowline slope of 2 percent. The procedures in the TxDOT Hydraulic Design Manual, September 2019 were used to determine the flow depth, bench capacity, and contributing drainage area. The largest contributing area to any bench occurs in the western portion of DA-P02 and is 9.7 acres. Using the Rational Method procedures described in Attachment C1-D, the calculated peak flowrates for the worst-case bench for the 25-year and 100-year storms are 59.8 cfs and 75.4 cfs, respectively. The Flowmaster program was utilized to determine the full-flow capacity of the bench, which is 275.8 cfs. Therefore, the selected downchutes have abundant capacity to convey the 25-year and 100-year runoff flows. The output from the Flowmaster calculation is included below.

DOWNCHUTE DESIGN

The drainage downchute design calculations are presented for the typical proposed downchute flowline slope of 25 percent. The HEC-HMS model was used to calculate the 25-year flow for the worst-case downchute. The largest contributing area to a downchute is DA-P03 (66.3 acres). The 25-year flow from the HEC-HMS model for this downchute is 274.2 cfs and the 100-year flow is 404.4 cfs. The Flowmaster program was utilized to determine the full-flow capacity of the downchute, which is 802.2 cfs. Therefore, the selected downchutes have abundant capacity to convey the 25-year and 100-year runoff flows. The output from the Flowmaster calculation is included below. The downchutes were also evaluated using the Rational Method. The worst-case

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downchute has a drainage area of 66.3 acres and a time of concentration of 18 minutes. The 25year intensity is therefore 7.3 inches/hour. The worst-case Rational Method flow is determined by:

A Flowmaster calculation is provided below for this condition.

EROSION LAYER EVALUATION

This discussion presents the supporting documentation for evaluation of the thickness of the erosion layer for the final cover system at Beck Landfill. The evaluation is based on the premise of adding excess soil to increase the time required before maintenance is needed as recommended in the EPA Solid Waste Disposal Facility Criteria Technical Manual (EPA 530-R-93-017, November 1993).

The design procedure is as follows:

- The minimum thickness of the erosion layer is based on the depth of frost penetration, or six inches, whichever is greater. For Guadalupe County, the approximate depth of frost penetration is less than five inches.
- 2. Soil loss is calculated using the Universal Soil Loss Equation (USLE) by following NRCS procedures. The <u>TCEQ Surface Water Drainage and Erosional Stability</u> <u>Guidelines for a Municipal Solid Waste Landfills</u>, states that acceptable soil erosion for the final cover condition is 3 tons/acre/year. The calculated erosion rates for the top deck and sideslope areas are both less than 3 tons/acre/year. These results show that the thickness of the proposed 6-inch erosion layer is a sufficiently conservative design.
- 3. Vegetation for the site will be native and introduced grasses with root depths of 6 inches to 8 inches.
- 4. Native and introduced grasses will be hydroseeded with fertilizer on the disked (parallel to contours) erosion layer upon final grading. Temporary cold weather vegetation will be established if needed. Irrigation may be employed for 6 to 8 weeks or until vegetation is well established. Erosion control measures such as silt fences and straw bales will be used to minimize erosion until the vegetation is established. Areas that experience erosion or do not readily vegetate after hydroseeding will be reseeded until vegetation is established.
- 5. Slope stability information is included in Attachment D5 -Geotechnical Design.

MAXIMUM ALLOWABLE BENCH SPACING CALCULATION

Based on the discussion in the <u>TCEQ Surface Water Drainage and Erosional Stability Guidelines</u> for a Municipal Solid Waste Landfills, acceptable soil erosion for the final cover condition is 3 tons/acre/year. The USLE equation was utilized to calculate the bench spacing on the top deck and sideslope required to meet this value. Soil loss is calculated using the Universal Soil Loss Equation (USLE) by following NRCS procedures in Use *of the Universal Soil* Loss *Equation in Final Cover/Configuration Design Procedural Handbook* (October 1997). The soil loss is based on 90 percent vegetative cover. For the top deck, the bench seperation can be up to 1,000 feet, so no benches are required. For the sideslopes, a horizontal bench spacing of 120 feet provides a calculated erosion rate of 2.7 tons/acre/year. The 120 horizontal bench spacing has been used for the Beck landfill.

SIDESLOPE BENCH SEPARATION CALCULATION

| SOIL EROSION (RUSLE) | | | | | | |
|---|---------|--|--|--|--|--|
| $\mathbf{A} = \mathbf{R}^{*}\mathbf{K}^{*}\mathbf{L}^{*}\mathbf{S}^{*}$ | C*P | | | | | |
| R | 265 | | | | | |
| K | 0.32 | | | | | |
| LS | 5.3 | | | | | |
| C | 0.006 | | | | | |
| Р | 1 | | | | | |
| A (tons/acre/year) | 2.697 | | | | | |
| Bench Seperation | 120.000 | | | | | |

Figure 2-1 Isoerodent Map, USDA 1997

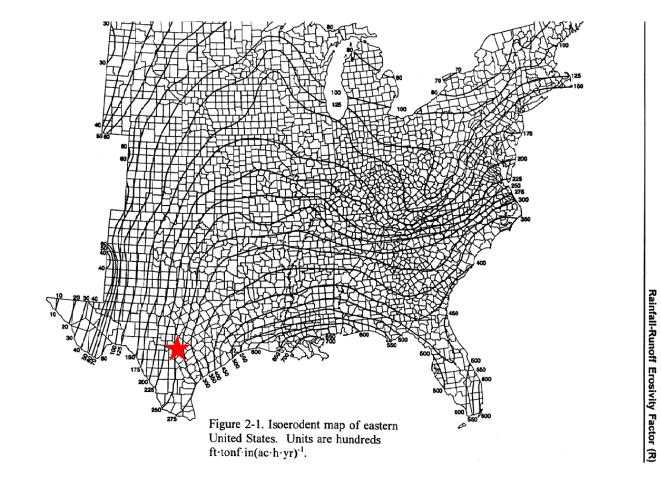
Monsic Clay Loam (more conservative than clay factor in Schertz Texas) Using the value of LS that you find go to table 4-3 and use the LS and slope to find bench distance. (should be different for Intermediate and Final Cover) (Type D, 90% grass - 0.006) Usually 1 for landfills (conservative case from the table provided in "P" Tab) 50 tons/ac/yr max for Intermediate Cover, 3 tons/ac/yr max for final cover Required Bench Horizontal Spacing

TOP DECK BENCH SEPARATION CALCULATION

| SOIL EROSION | | | | | |
|--|-------|--|--|--|--|
| (RUSLE) | | | | | |
| $\mathbf{A} = \mathbf{R}^* \mathbf{K}^* \mathbf{L}^* \mathbf{S}^*$ | *C*P | | | | |
| R | 265 | | | | |
| K | 0.32 | | | | |
| LS | 3.3 | | | | |
| C | 0.006 | | | | |
| Р | 1 | | | | |
| A (tons/acre/year) | 1.679 | | | | |
| Bench Seperation | 1000 | | | | |

Figure 2-1 Isoerodent Map, USDA 1997

Monsic Clay Loam (more conservative than clay factor in Schertz Texas) Using the value of LS that you find go to table 4-3 and use the LS and slope to find bench ((should be different for Intermediate and Final Cover) (Type D, 90% grass - 0.006) Usually 1 for landfills (conservative case from the table provided in "P" Tab) 50 tons/ac/yr max for Intermediate Cover, 3 tons/ac/yr max for final cover Required Bench Horizontal Spacing



| research stations | idle land ¹ | | | | | | | | | | |
|--|------------------------|--|----------------------|-------------------|------------|--------------------------------------|-------|----------|--------|-------|--|
| Soil Source of data | Computed K | Vegetative conc | Vegetative canopy Co | | | Cover that contacts the soil surface | | | | | |
| Dunkirk silt loamGeneva, N.Y. | '0.69 | .,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | Percent | | | Pe | rcent | ground | cover | | |
| Keene silt loamZanesville, Ohio | .48 | height ² | cover ³ | Type ⁴ | 0 | 20 | 40 | 60 | 80 | \$ | |
| Shelby loamBethany, Mo. | ,41 | No appreciable | | G | 0.45 | 0.20 | 0.10 | 0.042 | 0.013 | 0 | |
| Lodi loamBlacksburg, Va. | .39 | canopy | | w | .45 | .24 | .15 | .091 | .043 | | |
| Fayette silt loamLaCrosse, Wis. | 1.38 | | | | | | | | | | |
| Cecil sandy clay loam | .36 .33 | Tall weeds or | 25 | G | .36 | .17 | .09 | .038 | .013 | | |
| Ida silt Ioam | .33 | short brush | | w | .36 | .20 | .13 | .083 | .041 | | |
| Mansic clay loam | .32 | with average | | | | | | | | | |
| Hagerstown silty clay loamState College, Pa. | .31 | drop fall heigh | t 50 | G | .26 | .13 | .07 | .035 | .012 | | |
| Austin clay | .29 | of 20 in | | w | .26 | .16 | .11 | .076 | .039 | | |
| Mexico silt loam | .28 | | | | | | | | | | |
| Honeoye silt loam | 3.28 | | 75 | G | .17 | .10 | .06 | .032 | .011 | | |
| Cecil sandy loamClemson, S.C. | 1.28 | | | w | | .12 | .09 | .068 | .038 | | |
| Ontario Ioam | 1.27 | | | | | | | | | | |
| Cecil clay loam | .26 | Appreciable brush | 25 | G | .40 | .18 | .09 | .040 | .013 | | |
| Boswell find sandy loamTyler, Tex. | .25 | or bushes, with | | w | .40 | .22 | .14 | .087 | .042 | | |
| Cecil sandy loamWatkinsville, Ga. | .23 | average drop fo | all . | | | | | | | | |
| Zaneis fine sandy loamGuthrie, Okla. | .22 | height of 6½ f | t 50 | G | .34 | .16 | .08 | .038 | .012 | | |
| Tifton loamy sandTifton, Ga. | .10 | | | w | .34 | .19 | .13 | .082 | .041 | | |
| Freehold loamy sand | .08 | | | | | | | | | | |
| Bath floggy silt loam with surface Arnot, N.Y. | 3.05 | 1 | 75 | G | .28 | .14 | .08 | .036 | .012 | ł. | |
| stones > 2 inches removed | | | | w | .28 | .17 | .12 | .078 | .040 | ł | |
| Albia gravelly loam Beemerville, N.J. | .03 | | | | | | | | | | |
| ¹ Evaluated from continuous fallow. All others were | computed | Trees, but no | 25 | G | .42 | .19 | .10 | .041 | .013 | | |
| from rowcrop data. | | appreciable low | | w | .42 | .23 | .14 | .089 | .042 | 1 | |
| | | brush. Average | | | | | | | | | |
| | | drop fall heigh | t 50 | G | .39 | .18 | .09 | .040 | .013 |) = - | |
| | | of 13 ft | | w | .39 | .21 | .14 | .087 | .042 | l | |
| | | | 75 | ~ | 24 | | ~ | .039 | .012 | | |
| | | | /5 | G W | .36 .36 | | | | .041 | | |
| | | | | | | | | | | - | |
| | | 'The listed C randomly distribu | | | | | - | tion an | d mul | ch | |
| | | ¹ Canopy heigh | | | | | | all heir | aht of | | |
| | | drops falling from | | | | | - | | - | | |
| | | versely proportion | | | | - | | | | | |
| | | height exceeds 33 | | | | | | | | | |
| | | ^a Portion of tote | | surface | that | would | be h | idden f | rom v | de. | |
| | | canopy in a vert | | | | | | | | | |
| | | *G: cover at | | | | | | | caying | 3 | |
| | | pacted du | | | | | | | | - | |
| | | | | | | | | | s pla | nte | |
| | | W: cover at surface is mostly broadleaf herbaceous | | | | | | | | | |

| Table 4-3. | |
|--|--|
| Values for topographic factor, LS, for high ratio of rill to interrill erosion. ¹ | |

| | an a station of the second | | | | | | er faltereit mericau al fiele | H | orizontal sl | ope length | (ft) | | | | | | |
|--------------|----------------------------|------|------|------|------|------|-------------------------------|------|--------------|------------|-------|-------|-------|-------|-------|-------|-------|
| Slope (%) | <3 | 6 | 9 | 12 | 15 | 25 | 50 | 75 | 100 | 150 | 200 | 250 | 300 | 400 | 600 | 800 | 1000 |
| 0.2 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 0.5 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | 0.08 | 80.0 | 0.09 | 0.09 | 0.10 | 0.10 | 0.10 | 0.11 | 0.12 | 0.12 | 0.13 |
| 1.0 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 | 0.10 | 0.13 | 0.14 | 0.15 | 0.17 | 0.18 | 0.19 | 0.20 | 0.22 | 0.24 | 0.26 | 0.27 |
| 2.0 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 | 0.16 | 0.21 | 0.25 | 0.28 | 0.33 | 0.37 | 0.40 | 0.43 | 0.48 | 0.56 | 0.63 | 0.69 |
| 3.0 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.21 | 0.30 | 0.36 | 0.41 | 0.50 | 0.57 | 0.64 | 0.69 | 0.80 | 0.96 | 1.10 | 1.23 |
| 4.0 | 0.20 | 0.20 | 0.20 | 0.20 | 0.20 | 0.26 | 0.38 | 0.47 | 0.55 | 0.68 | 0.79 | 0.89 | 0.98 | 1.14 | 1.42 | 1.65 | 1.86 |
| 5.0 | 0.23 | 0.23 | 0.23 | 0.23 | 0.23 | 0.31 | 0.46 | 0.58 | 0.68 | 0.86 | 1.02 | 1.16 | 1.28 | 1.51 | 1.91 | 2.25 | 2.55 |
| 6.0 | 0.26 | 0.26 | 0.26 | 0.26 | 0.26 | 0.36 | 0.54 | 0.69 | 0.82 | 1.05 | 1.25 | 1.43 | 1.60 | 1.90 | 2.43 | 2.89 | 3.30 |
| 8.0 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.45 | 0.70 | 0.91 | 1.10 | 1.43 | 1.72 | 1.99 | 2.24 | 2.70 | 3.52 | 4.24 | 4.91 |
| 10.0 | 0.35 | 0.37 | 0.38 | 0.39 | 0.40 | 0.57 | 0.91 | 1.20 | 1.46 | 1.92 | 2.34 | 2.72 | 3.09 | 3.75 | 4.95 | 6.03 | 7.02 |
| 12.0 | 0.36 | 0.41 | 0.45 | 0.47 | 0.49 | 0.71 | 1.15 | 1.54 | 1.88 | 2.51 | 3.07 | 3.60 | 4.09 | 5.01 | 6.67 | 8.17 | 9.57 |
| 14.0 | 0.38 | 0.45 | 0.51 | 0.55 | 0.58 | 0.85 | 1.40 | 1.87 | 2.31 | 3.09 | 3.81 | 4.48 | 5.11 | 6.30 | 8.45 | 10.40 | 12.23 |
| 16.0 | 0.39 | 0.49 | 0.56 | 0.62 | 0.67 | 0.98 | 1.64 | 2.21 | 2.73 | 3.68 | 4.56 | 5.37 | 6.15 | 7.60 | 10.26 | 12.69 | 14.96 |
| 20.0 | 0.41 | 0.56 | 0.67 | 0.76 | 0.84 | 1.24 | 2.10 | 2.86 | 3.57 | 4.85 | 6.04 | 7.16 | 8.23 | 10.24 | 13.94 | 17.35 | 20.57 |
| 25.0 | 0.45 | 0.64 | 0.80 | 0.93 | 1.04 | 1.56 | 2.67 | 3.67 | 4.59 | 5.3 6.30 | 7.88 | 9.38 | 10.81 | 13.53 | 18.57 | 23.24 | 27.66 |
| 30.0 | 0.48 | 0.72 | 0.91 | 1.08 | 1.24 | 1.86 | 3.22 | 4.44 | 5.58 | 7.70 | 9.67 | 11.55 | 13.35 | 16.77 | 23.14 | 29.07 | 34.71 |
| 40.0 | 0.53 | 0.85 | 1.13 | 1.37 | 1.59 | 2.41 | 4.24 | 5.89 | 7.44 | 10.35 | 13.07 | 15.67 | 18.17 | 22.95 | 31.89 | 40.29 | 48.29 |
| 50.0 | 0.58 | 0.97 | 1.31 | 1.62 | 1.91 | 2.91 | 5.16 | 7.20 | 9.13 | 12.75 | 16.16 | 19.42 | 22.57 | 28.60 | 39.95 | 50.63 | 60.84 |
| 60.0 | 0.63 | 1.07 | 1.47 | 1.84 | 2.19 | 3.36 | 5.97 | 8.37 | 10.63 | 14.89 | 18.92 | 22.78 | 26.51 | 33.67 | 47.18 | 59.93 | 72.15 |

¹Such as for freshly prepared construction and other highly disturbed soil conditions with little or no cover (not applicable to thawing soil)

Between the proposed benches, the run-off condition will be sheet flow and Figure 5-4 from the TxDOT 2004 Hydraulic Manual below demonstrates that sheet flow from the 6% top deck and 25% sideslopes will travel at a velocity less than six feet per second, which will prevent significant erosion from occurring. For areas with final cover, it is assumed that the soil layer will have vegetation equivalent to "short grass pasture and lawns" and the calculated sheet flow velocity for the top deck is 1.9 ft/sec while the calculated sheet flow velocity for the sideslopes is 3.1 ft/sec.

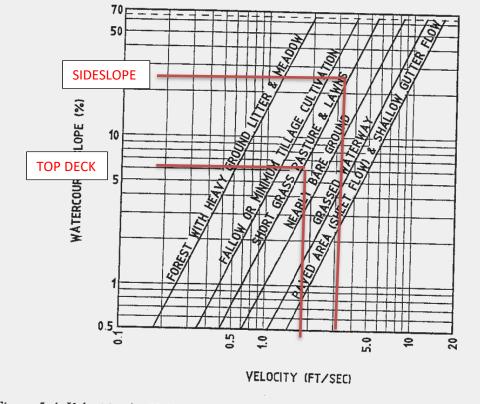


Figure 5-4. Velocities for Upland Method of Estimating Time of Concentration--English (Adapted from the National Engineering Handbook Volume 4)

FINAL COVER BENCH FULL-FLOW CALCULATION

| | Fu | II-Flow Bench | | | |
|---------------------------------------|--|--|-----------------------|---------------------------|--|
| Project Description | | | | _ | |
| Friction Method | Manning Formula | | | _ | |
| Solve For | Discharge | | | _ | |
| Input Data | | | | _ | |
| Channel Slope | 0.020 ft/ft | | | | |
| Normal Depth | 2.6 ft | | | - | |
| | Se | ction Definitions | | | |
| Stati (ft) | | | Elevation (ft) | | |
| | | 0+00 | | 10.00 | |
| | | 0+04 | | 8.00 | |
| | | 0+08 | | 7.43 | |
| | | 0+20 | | 10.40 | |
| | Roughne | ss Segment Definitions | | | |
| Start Station | | Ending Station | Roughness Coefficient | | |
| (0+00, 10.00) | | (0+20, 10.40) | | 0.025 | |
| Options | | | | - | |
| Current Roughness Weighted | Pavlovskii's | | | _ | |
| Method | Method | | | | |
| Open Channel Weighting Method | Pavlovskii's Method | | | | |
| Closed Channel Weighting | Pavlovskii's | | | | |
| Method | Method | | | _ | |
| Results | | | | - | |
| Discharge | 275.75 cfs | | | _ | |
| Roughness Coefficient | 0.025 | | | | |
| Elevation Range | 7.4 to 10.4 ft | | | | |
| Flow Area | 26.5 ft ² | | | | |
| Wetted Perimeter | 19.2 ft | | | | |
| Hydraulic Radius | 1.4 ft | | | | |
| Top Width | 18.38 ft | | | | |
| Normal Depth | 2.6 ft 3.1 ft | | | | |
| Critical Depth Critical Slope | 0.008 ft/ft | | | | |
| Velocity | 10.41 ft/s | | | | |
| Velocity Velocity Head | 1.68 ft | | | | |
| Specific Energy | 4.25 ft | | | | |
| Froude Number | 1.529 | | | | |
| Flow Type | Supercritical | | | _ | |
| GVF Input Data | | | | - | |
| Downstream Depth | 0.0 ft | | | _ | |
| | Bentley Systems, Inc. Haestad Methods Solution | | | | |
| Beck Hydraulic Calcs.fm8 8/28/2022 | | Center on Company Drive Suite 200 W | l | [10.03.00.03 Page 1 of | |
| | | CT 06795 ÚSA +1-203-755-1666 | | | |

FINAL COVER DOWNCHUTE FULL-FLOW CALCULATION

| ~~~ | Sist-Case Downc | nute Full Flow Capacity |
|-----------------------------------|----------------------|-------------------------|
| Project Description | | |
| Friction Method | Manning | |
| Solve For | Formula Discharge | |
| | Discharge | |
| put Data | | |
| Roughness Coefficient | 0.069 | |
| Channel Slope | 0.250 ft/ft | |
| Normal Depth | 2.0 ft | |
| eft Side Slope | 4.000 H:V | |
| Right Side Slope | 4.000 H:V | |
| Bottom Width | 20.00 ft | |
| esults | | |
| Discharge | 802.22 cfs | |
| Flow Area | 56.0 ft ² | |
| Wetted Perimeter | 36.5 ft | |
| Hydraulic Radius | 1.5 ft | |
| Top Width | 36.00 ft | |
| Critical Depth | 3.0 ft | |
| Critical Slope | 0.055 ft/ft | |
| Velocity | 14.33 ft/s | |
| elocity Head | 3.19 ft | |
| Specific Energy | 5.19 ft | |
| Froude Number | 2.025 | |
| ow Type | Supercritical | |
| /F Input Data | | |
| ownstream Depth | 0.0 ft | |
| .ength | 0.0 ft | |
| umber Of Steps | 0 | |
| /F Output Data | | |
| lpstream Depth | 0.0 ft | |
| Profile Description | N/A | |
| Profile Headloss | 0.00 ft | |
| Downstream Velocity Infinity ft/s | | |
| Ipstream Velocity | Infinity ft/s | |
| Iormal Depth | 2.0 ft | |
| ritical Depth | 3.0 ft | |
| Channel Slope | 0.250 ft/ft | |
| Critical Slope | 0.055 ft/ft | |

Worst-Case Downchute Full Flow Capacity

FINAL COVER DOWNCHUTE RATIONAL METHOD WORST-CASE CALCULATION

| Project Description | | |
|-----------------------|----------------------|--|
| | Manning | |
| Friction Method | Formula | |
| Solve For | Normal Depth | |
| Input Data | | |
| Roughness Coefficient | 0.069 | |
| Channel Slope | 0.250 ft/ft | |
| Left Side Slope | 4.000 H:V | |
| Right Side Slope | 4.000 H:V | |
| Bottom Width | 20.00 ft | |
| Discharge | 339.00 cfs | |
| Results | | |
| Normal Depth | 1.2 ft | |
| Flow Area | 31.0 ft ² | |
| Wetted Perimeter | 30.2 ft | |
| Hydraulic Radius | 1.0 ft | |
| Top Width | 29.93 ft | |
| Critical Depth | 1.8 ft | |
| Critical Slope | 0.063 ft/ft | |
| Velocity | 10.94 ft/s | |
| Velocity Head | 1.86 ft | |
| Specific Energy | 3.10 ft | |
| Froude Number | 1.896 | |
| Flow Type | Supercritical | |
| GVF Input Data | | |
| Downstream Depth | 0.0 ft | |
| Length | 0.0 ft | |
| Number Of Steps | 0 | |
| GVF Output Data | | |
| Upstream Depth | 0.0 ft | |
| Profile Description | N/A | |
| Profile Headloss | 0.00 ft | |
| Downstream Velocity | Infinity ft/s | |
| Upstream Velocity | Infinity ft/s | |
| Normal Depth | 1.2 ft | |
| Critical Depth | 1.8 ft | |
| Channel Slope | 0.250 ft/ft | |
| Critical Slope | 0.063 ft/ft | |

Permissible Velocities

Table 8-6

Table 8-6 below from the USDA Part 654 Stream Restoration Design National Engineering Handbook provides maximum allowable velocities for grass-lined channels to maintain non-erosive conditions. The clay soils at the site would be considered erosion resistant in this table. For Bermudagrass lined earthen channels with slopes of 0-5%, the maximum non-erosive velocity is 8 feet per second. The highest calculated velocity for any of the final cover control structures is for Perimeter Berm 8 and it is 6.49 ft/sec. The benches and other berms all have lower calculated peak velocities. The velocities in the downchutes are higher than 8 ft/sec, which is why they are proposed to be armored with gabion mattresses.

| 0 | 61 | Allowable velocity (ft/s) | | | | |
|---|---|-------------------------------|---------------------|--|--|--|
| Cover | Slope range percent | Erosion-resistant soils | Easily eroded soils | | | |
| Bermudagrass | 0-5 | 8 | 6 | | | |
| | 5-10 | 7 | 5 | | | |
| | >10 | 6 | 4 | | | |
| Buffalograss, Kentucky bluegrass, | 0-5 | 7 | 5 | | | |
| smooth brome, blue grama | 5-10 | 6 | 4 | | | |
| | >10 | 5 | 3 | | | |
| Grass mixture | 0-5 | 5 | 4 | | | |
| | 5-10 | 4 | 3 | | | |
| | Not recommended on slopes greater than 10% | | | | | |
| Lespedeza sericea, weeping lovegrass, | 0-5 | 3.5 | 2.5 | | | |
| ischaemum (yellow bluestem), kudzu, alfalfa, crabgrass | Not recommended on slopes greater than 5%, except for side slopes in a compound channel | | | | | |
| Annuals—used on mild slopes or as | 0-5 | 3.5 | 2.5 | | | |
| temporary protection until permanent covers are established, common lespedeza, Sudangrass | Not recomm | ended for slopes greater that | an 5% | | | |

Allowable velocities for channels lined with grass

(210-VI-NEH, August 2007)

8-27

BECK LANDFILL

APPENDIX C1-F FACILITY SURFACE WATER DRAINAGE REPORT INTERMEDIATE COVER EROSION AND SEDIMENTATION CONTROL PLAN

Includes pages C1-F-1 through C1-F-8



CONTENTS

| Narrative | .1 |
|--|----|
| Erosion And Sediment Control Landfill Cover Phases | .2 |
| Best Management Practices | .4 |
| Soil Stabilization and Vegetation Schedule | .6 |
| Stormwater System Maintenance Plan | .7 |



NARRATIVE

This appendix presents temporary erosion and sediment control structures for the intermediate cover phase of landfill development. "Temporary", for the purposes of this narrative, is defined as the time between the construction of intermediate cover and the construction of final cover or the placement of additional waste, as the case may be. Intermediate top slope surfaces and external sideslopes, for the purposes of compliance with 30 TAC §330.305(d), are those above-grade slopes that:

- a) Drain directly to the site perimeter stormwater management system (i.e., areas where the stormwater directly flows to a perimeter channel or detention pond),
- b) Have received intermediate or final cover, and
- c) Have either reached their permitted elevation, or will subsequently remain inactive for longer than 180 days.

Slopes that drain to ongoing waste placement, pre-excavated areas, areas that have received only operational cover, or areas under construction that have not received waste are not covered under this appendix and do not contribute to offsite runoff.

EROSION AND SEDIMENT CONTROL LANDFILL COVER PHASES

The purpose of this section is to define the landfill cover phases and where they are addressed throughout the Beck Landfill Site Development Plan:

<u>Operational Cover</u>- Operational cover is defined in §330.165(a), except that for Type IV landfills it is required weekly. Operational cover consists of 6 inches of well-compacted earthen material not previously mixed with garbage, rubbish, or other solid waste applied as required in the Site Operating Plan. The placement and erosion control practices for operational cover areas are defined in Part IV- Site Operating Plan and in the Best Management Practices Section of this appendix.

<u>Intermediate Cover</u> - Intermediate cover is defined in §330.165(c). Intermediate cover consists of at least 12 inches of suitable earthen material and is graded and maintained to prevent erosion and ponding of water. The placement requirements and erosion control practices for intermediate cover areas are defined in this appendix.

<u>Final Cover</u> - Final cover is defined in Subchapter K. The placement and erosion control practices for final cover areas are defined in Attachment C1, Appendix C1-E. Final cover at Beck Landfill will be managed as provided for in the closure and post-closure plan required by 30 TAC 330 Subchapter K, Closure and Post-Closure.

During all phases of operation, the goal is keep all run-off from the sideslopes and top dome areas as sheet flow to reduce the formation of erosion rills. Based on the TxDOT (2004 Hydraulic Design Manual) Figure 5-4 below, sheet flow from the 6% top deck and 25% sideslopes will travel at a velocity less than six feet per second, which will prevent significant erosion from occurring. For areas with operational and intermediate cover, it is conservatively assumed that the soil layer will be "nearly bare ground" and the calculated sheet flow velocity for the top deck is 2.5 ft/sec while the calculated sheet flow velocity for the sideslopes is 5.0 ft/sec. In order to maintain sheet flow conditions, temporary structural controls should be placed at 300 to 400 feet maximum spacings. Based on the USLE calculations provided in Appendix C1-G, no temporary structural controls are required on the top deck to maintain allowable erosion levels, and temporary structural controls are required at a maximum spacing of 400 feet for the sideslopes.

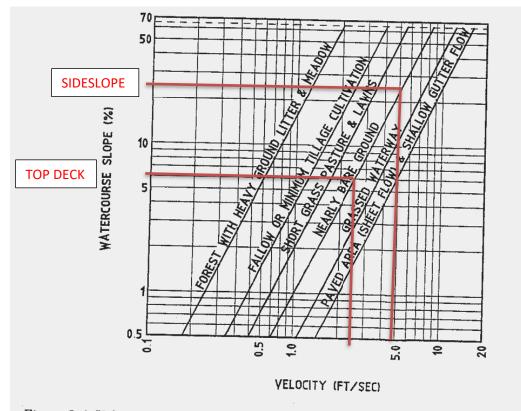


Figure 5-4. Velocities for Upland Method of Estimating Time of Concentration--English (Adapted from the National Engineering Handbook Volume 4)

BEST MANAGEMENT PRACTICES

Vegetation and temporary erosion control structures provide the most effective means of reducing the amount of soil loss during operation of the landfill. Best management practices utilized for erosion and sediment control may be broadly categorized as nonstructural and structural controls. Nonstructural controls addressing erosion include the following:

- Minimization of the disruption of the natural features, drainage, topography, or vegetative cover features
- Phased development to minimize the area of bare soil exposed at any given time
- Disturbing only the smallest area necessary to perform current activities
- Confining sediment to the construction area during the construction phase
- Scheduling of construction activities during the time of year with the least erosion potential, when applicable
- Stabilization of exposed surfaces in a timely manner
- Structural controls are preventative and also mitigative since they control erosion and sediment movement. In the event that additional soil stabilization or erosion control measures are deemed necessary, one or more of the following measures will be implemented:
- Vegetative and Non-Vegetative Stabilization. A soil stabilization and vegetation schedule is provided in this appendix.
- Check Dams. Check dams shall be constructed using gravel, rock, gabions, compost socks, or sand bags to reduce flow velocity and therefore erosion in a perimeter channel or detention pond.
- Filter Berms. Filter berms shall be constructed of mulch, woodchips, brush, compost, shredded wood waste, or synthetic filter materials. Mesh socks shall be filled with compost, mulch, woodchips, brush, or shredded wood waste. Filter berms or filled mesh socks shall be installed at the bottom of slopes, throughout the perimeter drainage system, and on sideslopes. The maximum drainage area to the filter berm or filled mesh sock will not exceed two acres. Specifications for the filter berms are provided on Drawing C3-3.
- Baled Hay, Hay bales, straw bales, or baled hay shall be approximately 30 inches in length and be composed entirely of vegetable matter. Hay bales shall be embedded in the soil a minimum of four inches.

- Sediment Traps. Sediment traps are small, excavated areas that function as sediment basins. Sediment traps allow for the settling of suspended sediment in stormwater runoff. Sediment traps shall be constructed in perimeter channels, temporary internal channels, and at entrances to detention ponds. The maximum drainage area contributing to a sediment trap will not exceed 10 acres.
- Temporary Sediment Control Fence or Silt Fence. Silt fences or fabric filter fences shall be used where there is sheet flow and sediment transport. The maximum drainage area to the silt fence will not exceed the manufacturer's specification, but will in no case be greater than 0.5 acre per 100 feet of fence. To ensure sheet flow, a gravel collar or level spreader may be used upslope of the silt fence.
- Berms. These structures will be constructed of earthen material with the top six inches capable of sustaining native plant growth. Rolled erosion control mats or blankets made from natural materials or synthetic fiber, grass, or compost/mulch/straw may be used as erosion protection along the flowline. These structures direct the flow to the drainage system. These structures decrease downslope velocities of runoff that could cause erosion on the intermediate cover slopes.
- Benches. These structures will be constructed out of the waste material and covered with intermediate cover. Rolled erosion control mats or blankets made from natural materials or synthetic fiber, grass, or compost/mulch/straw may be used as erosion protection along the flowline. These structures direct the flow to the drainage system. These structures decrease downslope velocities of runoff that could cause erosion on the intermediate cover slopes.
- Downchutes. downchutes are bermed conveyance structures constructed on the intermediate cover slopes. Flow will be directed to the downchutes via swales, then conveyed to the perimeter drainage system. The downchutes will be lined with an FML geomembrane, turf reinforcement mats, Maccaferri gabion mattresses, concrete, gabions, crushed concrete, or stone.

SOIL STABILIZATION AND VEGETATION SCHEDULE

The soil stabilization and vegetation schedule is as follows:

- Areas that will remain inactive for greater than 180 days will receive intermediate cover.
- Intermediate cover on slopes will be stabilized by tracking into the slope. Soil stabilization can be enhanced by mulching, the addition of soil tackifiers, or a combination of these measures. The intermediate cover will be graded to provide positive drainage.
- Temporary erosion control structures will be installed within 180 days from when intermediate cover is constructed.
- The intermediate cover area will be seeded or sodded as soon as practical, following placement of intermediate cover and will be documented in the site operating record. All intermediate cover areas will be managed to control erosion and achieve a predicted soil loss of less than 50 tons per acre per year. A 60 percent vegetative cover will be established over the intermediate cover areas within 180 days from intermediate cover construction unless prevented by climatic events (e.g., drought, rainfall, etc.). Additional temporary erosion control measures will be implemented during these events to promote establishment of vegetative cover.
- Mulch, woodchips, or compost may be used as a layer placed over the intermediate cover to protect the exposed soil surface from erosive forces and conserve soil moisture until vegetation can be established. The mulch, woodchips, or compost will be used to stabilize recently graded or seeded areas. The mulch, woodchips, or compost will be spread evenly over a recently seeded area and tracked into the surface to protect the soil from erosion and moisture loss, if required to promote the establishment of vegetation. These materials are not required for the establishment of vegetation on the intermediate cover; however, they may be used if Beck Landfill determines they are needed to promote vegetative growth or to provide additional erosional stability to the intermediate cover surface. These materials will vary in thickness but will not be placed to a thickness to inhibit vegetative growth.
- The intermediate cover and temporary erosion control structures will be maintained as detailed in the Stormwater System Maintenance Plan.
- Final cover will be constructed as the site develops. Temporary erosion control features will be removed as permanent erosion control structures are constructed.

STORMWATER SYSTEM MAINTENANCE PLAN

Beck Landfill will restore and repair temporary stormwater systems such as channels, benches, drainage swales, chutes, and flood control structures in the event of washout or failure. In addition, the BMPs discussed in this appendix will also be replaced or repaired in the event of failure. Excessive sediment will be removed, as needed, so that the drainage structures function as designed. Site inspections by facility personnel will be performed weekly or within 48 hours of a rainfall event of 0.5 inches or more. The final cover system and the erosion sediment control structures will be maintained throughout the site life and post-closure period.

The following items will be evaluated during the inspections:

- Erosion of intermediate cover areas, perimeter ditches, temporary chutes, swales, detention ponds, berms, and other drainage features
- Settlement of intermediate cover areas, final cover areas, perimeter ditches, chutes, swales, and other drainage features
- Silt and sediment build-up in perimeter ditches, chutes, swales, and detention ponds
- Presence of ponded water on intermediate cover or behind temporary erosion control structures
- Obstructions in drainage features
- Presence of erosion or sediment discharge at offsite stormwater discharge locations
- Temporary erosion and sediment control features

Maintenance activities will be performed to correct damaged or deficient items noted during the site inspections. These activities will be performed as soon as possible after the inspection. The time frame for correction of damaged or deficient items will vary based on weather, ground conditions, and other site-specific conditions.

Maintenance activities will consist of the following, as needed:

- Placement of additional temporary or permanent vegetation
- Placement, grading, and stabilization of additional soils in eroded areas or in areas which have settled
- Replacement of gabion mattresses or other structural lining
- Removal of obstructions from drainage features
- Removal of silt and sediment build-up from the temporary erosion control structures. Removed sediment will be re-used as daily or intermediate cover.

- Removal of ponded water on the intermediate cover or behind temporary erosion control structures. If removed water has not contacted waste, it may be discharged in accordance with the site's stormwater permit. If the water has potentially contacted waste, it will be managed as contaminated stormwater,
- Repairs to erosion and sedimentation controls
- Installation of additional erosion and sedimentation controls
- Documentation and training requirements are discussed below:
- Site inspections by facility personnel will be performed weekly or within 48 hours of a rainfall event of 1.5 inches or more.
- Documentation of the inspection will be included in the site operating record.
- Documentation of maintenance activities that were performed to correct damaged or deficient items noted during the site inspections will be included in the site operating record.
- Facility personnel will be trained to perform inspections, and to install and maintain temporary erosion control structures.

BECK LANDFILL

APPENDIX C1-G FACILITY SURFACE WATER DRAINAGE REPORT INTERMEDIATE COVER EROSION CONTROL STRUCTURE DESIGN

Includes pages C1-G-1 through C1-G-6



Civil & Environmental Consultants, Inc.

Beck Landfill Revised (9/23) Part III, Attachment C1-G

CONTENTS

| Narrative | 1 |
|-----------------------------------|---|
| Intermediate Cover Evaluation | 2 |
| Temporary Drainage Berm Design | 3 |
| Temporary Drainage Letdown Design | 4 |
| Design Summary | |



NARRATIVE

This appendix presents the supporting documentation to evaluate and design temporary erosion and sediment control structures for the intermediate cover phase of landfill development.

INTERMEDIATE COVER PLAN

As intermediate cover is constructed, benches, temporary chutes and berms will be constructed to prevent erosion and sedimentation. Erosion control features (i.e., filter berms, rock check dams, hay bales, or equivalent) may be constructed at the toe of filled areas to minimize erosion and prevent disturbance of the existing grassed slopes. Otherwise, temporary erosion and sediment control features will be installed within 180 days from when the intermediate cover is constructed. An existing conditions summary and Best Management Practices are included in Appendix C1-F. Example intermediate cover drainage calculations are included in this appendix for use in site operations.

INTERMEDIATE COVER EVALUATION

The intermediate cover evaluation is based on the Universal Soil Loss Equation (USLE) following Natural Resource Conservation Service (NRCS) procedures. The evaluation is based on a 12-inch thick intermediate cover layer with 60 percent vegetated cover. Calculations for the soil loss for intermediate cover on external 6 percent and 25 percent slopes have been provided below.

TEMPORARY DRAINAGE BERM DESIGN

The temporary drainage berms are designed for typical drainage areas and flowline slopes. The procedures in the TxDOT Hydraulic Design Manual, September 2019, were used to determine peak flow, flow depth, flow velocity, and capacity. The Rational Method and the Manning's Equation were used to calculate the design parameters.

TEMPORARY DIVERSION CHANNEL DESIGN

The temporary diversion channels are designed for typical drainage areas and flowline slopes. The procedures in the TxDOT Hydraulic Design Manual, September 2019, were used to determine peak flow, flow depth, flow velocity, and diversion channel capacity. The Rational Method and the Manning's Equation were used to calculate the design parameters.

TEMPORARY DRAINAGE DOWNCHUTE DESIGN

The temporary drainage downchutes are designed for typical drainage areas on a 25 percent external side slope. The procedures in the TxDOT Hydraulic Design Manual, September 2019, were used to determine peak flow, flow depth, flow velocity, and downchute capacity. The Rational Method and the Manning's Equation were used to calculate the design parameters.

Civil & Environmental Consultants, Inc.

INTERMEDIATE COVER EVALUATION

SOIL LOSS

This section presents the supporting documentation for evaluation of the potential for intermediate cover soil erosion loss at Beck Landfill. The evaluation is based on the premise of adding excess soil to increase the time required before maintenance is needed as recommended in the EPA Solid Waste Disposal Facility Criteria Technical Manual (EPA 530-R-93-017, November 1993).

The design procedure is as follows:

- 1. Minimum thickness of the intermediate cover is evaluated based on the maximum soil loss of 50 tons per acre per year.
- 2. Soil loss is calculated using the Universal Soil Loss Equation (USLE) by following NRCS procedures. The soil loss is based on 60 percent vegetative cover as recommended in the TCEQ, Use of the Universal Soil Loss Equation in Final Cover/Configuration Design Procedural Handbook (October 1997). The pages from the NRCS manual are included in Appendix C1-E. These results of the calculations show that erosion controls must be placed on maximum 400 feet spacing on the sideslopes.

| SOIL EROSION | | | | | |
|---|--------|--|--|--|--|
| (RUSLE) | | | | | |
| $\mathbf{A} = \mathbf{R}^{*}\mathbf{K}^{*}\mathbf{L}^{*}\mathbf{S}^{*}\mathbf{C}^{*}\mathbf{P}$ | | | | | |
| R | 265 | | | | |
| K | 0.32 | | | | |
| LS | 13.53 | | | | |
| С | 0.042 | | | | |
| Р | 1 | | | | |
| A (tons/acre/year) | 48.188 | | | | |
| Control Seperation | 400 | | | | |

Figure 2-1 Isoerodent Map, USDA 1997 Monsic Clay Loam (more conservative than clay factor in Schertz Texas) Using the value of LS that you find go to table 4-3 and use the LS and slope to find bench distance. (should be different for Intermediate and Final Cover) (Type G, 60% grass - 0.042) Usually 1 for landfills (conservative case from the table provided in "P" Tab) 50 tons/ac/yr max for Intermediate Cover, 3 tons/ac/yr max for final cover Required Berm, Bench, or Other Control Horizontal Spacing

3. Temporary vegetation for the intermediate cover areas will be native and introduced grasses with root depths of six inches to eight inches.

Native and introduced grasses will be hydroseeded, drill seeded, or broadcast seeded with fertilizer on the disked (parallel to contours) intermediate cover layer as soon as practical following placement of intermediate cover and will be documented in the site operating record. All intermediate cover areas will be managed to control erosion and achieve a predicted soil loss of less than 50 tons per acre per year. Temporary erosion and sediment control features (including at least 60 percent vegetative cover) will be installed within 180 days from when the intermediate cover is constructed. Areas that experience erosion or do not readily vegetate will be reseeded and additional temporary erosion control measures will be implemented until vegetation is established or the soil will be replaced with soil that will support the grasses.

The facility will utilize a combination of vegetation and interim and permanent structural controls to control sediment creation. Soil loss calculations above demonstrate that the expected worst-case conditions for the interim phases of the landfill produce less sediment than the maximum recommended values provided in Section 2.5 of TCEQ guidance document RG-417. The site operations are regulated through the Texas Pollutant Discharge Elimination System program for stormwater discharges and interim controls will be continuously evaluated to ensure that the minimum amount of sediment possible will be discharged from the site.

| Table 4-3. | | |
|--------------------------------|---|----|
| Values for topographic factor, | LS, for high ratio of rill to interrill erosion | .1 |

| | Horizontal slope length (ft) | | | | | | | | | | | | | | | | |
|--------------|------------------------------|------|------|------|------|------|------|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Slope (%) | <3 | 6 | 9 | 12 | 15 | 25 | 50 | 75 | 100 | 150 | 200 | 250 | 300 | 400 | 600 | 800 | 1000 |
| 0.2 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 | 0.06 |
| 0.5 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | 0.08 | 0.08 | 0.09 | 0.09 | 0.10 | 0.10 | 0.10 | 0.11 | 0.12 | 0.12 | 0.13 |
| 1.0 | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 | 0.10 | 0.13 | 0.14 | 0.15 | 0.17 | 0.18 | 0.19 | 0.20 | 0.22 | 0.24 | 0.26 | 0.27 |
| 2.0 | 0.13 | 0.13 | 0.13 | 0.13 | 0.13 | 0.16 | 0.21 | 0.25 | 0.28 | 0.33 | 0.37 | 0.40 | 0.43 | 0.48 | 0.56 | 0.63 | 0.69 |
| 3.0 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.21 | 0.30 | 0.36 | 0.41 | 0.50 | 0.57 | 0.64 | 0.69 | 0.80 | 0.96 | 1.10 | 1.23 |
| 4.0 | 0.20 | 0.20 | 0.20 | 0.20 | 0.20 | 0.26 | 0.38 | 0.47 | 0.55 | 0.68 | 0.79 | 0.89 | 0.98 | 1.14 | 1.42 | 1.65 | 1.86 |
| 5.0 | 0.23 | 0.23 | 0.23 | 0.23 | 0.23 | 0.31 | 0.46 | 0.58 | 0.68 | 0.86 | 1.02 | 1.16 | 1.28 | 1.51 | 1.91 | 2.25 | 2.55 |
| 6.0 | 0.26 | 0.26 | 0.26 | 0.26 | 0.26 | 0.36 | 0.54 | 0.69 | 0.82 | 1.05 | 1.25 | 1.43 | 1.60 | 1.90 | 2.43 | 2.89 | 3.30 |
| 8.0 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.45 | 0.70 | 0.91 | 1.10 | 1.43 | 1.72 | 1.99 | 2.24 | 2.70 | 3.52 | 4.24 | 4.91 |
| 0.0 | 0.35 | 0.37 | 0.38 | 0.39 | 0.40 | 0.57 | 0.91 | 1.20 | 1.46 | 1.92 | 2.34 | 2.72 | 3.09 | 3.75 | 4.95 | 6.03 | 7.02 |
| 2.0 | 0.36 | 0.41 | 0.45 | 0.47 | 0.49 | 0.71 | 1.15 | 1.54 | 1.88 | 2.51 | 3.07 | 3.60 | 4.09 | 5.01 | 6.67 | 8.17 | 9.57 |
| 4.0 | 0.38 | 0.45 | 0.51 | 0.55 | 0.58 | 0.85 | 1.40 | 1.87 | 2.31 | 3.09 | 3.81 | 4.48 | 5.11 | 6.30 | 8.45 | 10.40 | 12.23 |
| 6.0 | 0.39 | 0.49 | 0.56 | 0.62 | 0.67 | 0.98 | 1.64 | 2.21 | 2.73 | 3.68 | 4.56 | 5.37 | 6.15 | 7.60 | 10.26 | 12.69 | 14.96 |
| 20.0 | 0.41 | 0.56 | 0.67 | 0.76 | 0.84 | 1.24 | 2.10 | 2.86 | 3.57 | 4.85 | 6.04 | 7.16 | 8.23 | 10.24 | 13.94 | 17.35 | 20.57 |
| 25.0 | 0.45 | 0.64 | 0.80 | 0.93 | 1.04 | 1.56 | 2.67 | 3.67 | 4.59 | 6.30 | 7.88 | 9.38 | 10.81 | 13.53 | 18.57 | 23.24 | 27.66 |
| 80.0 | 0.48 | 0.72 | 0.91 | 1.08 | 1.24 | 1.86 | 3.22 | 4.44 | 5.58 | 7.70 | 9.67 | 11.55 | 13.35 | 16.77 | 23.14 | 29.07 | 34.71 |
| 0.0 | 0.53 | 0.85 | 1.13 | 1.37 | 1.59 | 2.41 | 4.24 | 5.89 | 7.44 | 10.35 | 13.07 | 15.67 | 18.17 | 22.95 | 31.89 | 40.29 | 48.29 |
| 50.0 | 0.58 | 0.97 | 1.31 | 1.62 | 1.91 | 2.91 | 5.16 | 7.20 | 9.13 | 12.75 | 16.16 | 19.42 | 22.57 | 28.60 | 39.95 | 50.63 | 60.84 |
| 0.0 | 0.63 | 1.07 | 1.47 | 1.84 | 2.19 | 3.36 | 5.97 | 8.37 | 10.63 | 14.89 | 18.92 | 22.78 | 26.51 | 33.67 | 47.18 | 59.93 | 72.15 |

¹Such as for freshly prepared construction and other highly disturbed soil conditions with little or no cover (not applicable to thawing soil)

TEMPORARY DRAINAGE BERM DESIGN

The temporary drainage berm design for intermediate cover areas is presented for the typical berm flowline of 2 percent. The procedures in the TxDOT Hydraulic Design Manual were used to determine peak flow, flow depth, flow velocity, and berm capacity. The temporary berms will be located on the intermediate cover to prevent erosion as follows:

All temporary berms shall be designed to minimize erosion and provide a maximum flow depth of two feet. The total height of the berms at the flowline is a minimum of three feet. A detail for the temporary drainage berm is provided on Figure C3-4, in Appendix C-3. As noted in the calculations, the velocities in the berms are less than permissible non-erodible velocities. If sustained erosion is observed, facility management will evaluate and construct additional temporary drainage berms. Example drainage berm calculations for a grassed intermediate cover are provided below.

| Berms | | | | | |
|-----------------------------|------|--|--|--|--|
| Bottom width | 0 ft | | | | |
| Side slope 1 (horiz./vert.) | 4/1 | | | | |
| Side slope 2 (horiz./vert.) | 3/1 | | | | |
| Manning roughness, n | 0.03 | | | | |
| Channel slope | 2% | | | | |
| Flow depth | 2 ft | | | | |

| Results | | | | | | |
|-------------------|-------|--------|--|--|--|--|
| Flow area | 14 | ft^2 | | | | |
| Wetted perimeter | 14.57 | ft | | | | |
| Hydraulic radius | 0.96 | ft | | | | |
| Velocity, v | 6.82 | ft/sec | | | | |
| Flow, Q | 95.49 | cfs | | | | |
| Velocity head, hv | 0.72 | ft | | | | |
| Top width, T | 14 | ft | | | | |

The cross-sections for the temporary berms is three feet height, two feet top width, 3:1 uphill sideslopes and 2:1 downhill sideslopes. A detail for the temporary drainage berm is provided on Figure C3-4, in Appendix C-3. Based on the Rational Method parameters developed in Appendix C1-D, the maximum drainage area allowable for a temporary berm is 15 acres.

Q₂₅ = CIA 95 cfs= (0.7)(8.8 in/hr)(A) A= 15 acres

TEMPORARY DRAINAGE DOWNCHUTE DESIGN

The temporary downchute design is applicable for external side slopes of the landfill with intermediate cover. Temporary downchutes will typically consist of channels lined with erosion control material. The flow capacity of the downchute structures was determined based on the Manning's Equation. The maximum flow calculated from the Manning's Equation is used to determine the maximum drainage area based on the NRCS Method. The design calculations presented below represent typical calculations for temporary downchutes on a 25 percent slope. If sustained erosion is observed, facility management will evaluate the use and construction of temporary letdowns.

| Chute Design | | | | | |
|---------------|---|------|--|--|--|
| Bottom | ft | 20 | | | |
| Depth | ft | 2 | | | |
| Side slope | % | 25 | | | |
| Channel slope | % | 25 | | | |
| Roughness | Natural channel, very poor condition | 0.06 | | | |

| Capacity (max) | | | | | |
|----------------|-----|--------|--|--|--|
| Q | cfs | 922.54 | | | |
| V | fps | 16.47 | | | |
| D | ft | 2 | | | |

| Parameters | | | | | | | |
|-------------------|--------|--------|--|--|--|--|--|
| Flow area | 56.00 | ft^2 | | | | | |
| Wetted perimeter | 36.49 | ft | | | | | |
| Hydraulic radius | 1.53 | ft | | | | | |
| Velocity, v | 16.47 | ft/sec | | | | | |
| Flow, Q | 922.54 | cfs | | | | | |
| Velocity head, hv | 4.22 | ft | | | | | |
| Top width, T | 36.00 | ft | | | | | |

The cross-sections for the temporary downchutes is shown above. A detail for the temporary drainage berm is provided on Figure C3-4, in Appendix C-3. Based on the Rational Method parameters developed in Appendix C1-D, the maximum drainage area allowable for a temporary downchute is 149 acres.

Q₂₅ = CIA 922.5 cfs= (0.7)(8.8 in/hr)(A) A= 149 acres

Civil & Environmental Consultants, Inc.

DESIGN SUMMARY

Beck Landfill will implement the erosion and sediment control features on the intermediate cover as the landfill develops. The following items will be implemented, as filling operations are ongoing:

- Intermediate cover will be established on all areas that have received waste but will remain inactive for periods greater than 180 days.
- Sufficient permanent and temporary erosion and sediment control features shall be constructed to redirect surface water and prevent erosion.
- Temporary erosion and sediment control features shall be constructed within 180 days of placement of intermediate cover.
- Temporary erosion control structures (e.g., rock check dams, filter berms) may be established along the toe of existing vegetated intermediate cover areas with approximately 70-90 percent coverage.
- Final cover may be constructed as the site develops. Temporary erosion control features will be removed as permanent erosion controls are constructed.

The facility will utilize a combination of vegetation and interim and permanent structural controls to control sediment creation. Soil loss calculations previously provided demonstrate that the expected worst-case conditions for the interim and final phases of the landfill produce less sediment than the maximum recommended values provided in Section 2.5 of TCEQ guidance document RG-417. The site operations are regulated through the Texas Pollutant Discharge Elimination System program for stormwater discharges and interim controls will be continuously evaluated to ensure that the minimum amount of sediment possible will be discharged from the site.

MUNICIPAL SOLID WASTE PERMIT MAJOR AMENDMENT

PART III-ATTACHMENT C2 - FLOOD CONTROL ANALYSIS



NAME OF PROJECT: Beck Landfill MSW PERMIT APPLICATION NO.: 1848A OWNER: Nido, LTD (CN603075011) OPERATOR: Beck Landfill (RN102310968) CITY, COUNTY: Schertz, Guadalupe County

Major Amendment: Revised August 2024

Prepared by:



Civil & Environmental Consultants, Inc.

Texas Registration Number F-38 1221 S MoPac Expressway Suite 350, Austin, Texas 78746 (512) 329-0006



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APPENDIX C2-A

LOMR Application and Approval Letter

APPENDIX C2-B

No-Rise Certification for Proposed Stormwater Pond

APPENDIX C2-C

FEMA Correspondence



Discussion of 100 Year Floodplain

The current FEMA map panels for the area around the landfill property are numbers 48187C0210F & 48029C0295F, which were revised in 2007 and 2010, respectively. At the time the model for these panels was created, the Beck Landfill was permitted to be filled to its final grades, but not yet constructed to an extent where the entire footprint was above the calculated 100-year water surface. FEMA modeled this permitted future condition by placing blocked obstructions on the cross-sections that traverse the landfill footprint, so that the model accounted for the authorized final condition of the landfill. FEMA then extended the floodplain across the portions of the landfill that had not yet been constructed above the 100-year water surface elevations.

To prevent the wash-out of waste by a flood event, the entire landfill footprint is encompassed by a compacted clay berm, which extends above the current 100-year flood elevation. As part of the amendment application, Beck Landfill is proposing to extend the berm 10 feet vertically to provide additional freeboard above the 100-year event. The entire footprint of the landfill and perimeter berm is currently constructed above the 100-year water surface and Beck Landfill submitted a LOMR application to the City of Schertz and FEMA to revise the affected panels to accurately reflect the lateral extents of the floodplain. The LOMR application has updated cross-sections affected by the landfill with current topography and re-delineated the extents of the floodplain. The floodway shown on these panels was also revised to reflect the updated topography. The LOMR application maintains the hydrologic flow values included in the effective FEMA model.

The City of Schertz has approved the LOMR application and a copy of their concurrence is included in this section. The LOMR has also been approved by FEMA under Case No. 22-06-2567P. A complete copy of the LOMR application and approval letter are included in Appendix C2-A.

In compliance with 30 TAC 330.63(c)(2)(C), the following table has been prepared to show the projected 100 year flood elevation, top of the existing perimeter berm, and top of the proposed perimeter berm at each cross-section used in the HEC-RAS hydraulic model that was approved by FEMA as part of the LOMR application. The locations of each of these cross-sections are shown on Figure C2-2.

| Cross- Section Label | LOMR 100 Year Water Surface Elevation | Perimeter Dil (ft M | | Proposed Freeboard Above 100 Year Flood |
|----------------------------|---|------------------------|----------|--|
| | (ft MSL) | Existing | Proposed | (ft) |
| | | | | |
| 444777 | 714.34 | 716 | 726 | 11.7 |
| 442240 | 712.59 | 716 | 726 | 13.4 |
| 443555 | 712.24 | 715 | 725 | 12.8 |
| 442891 | 711.58 | 714 | 724 | 12.4 |
| 442214 | 709.72 | 714 | 724 | 14.3 |
| 441476 | 708.12 | 712 | 722 | 13.9 |
| 440762 | 705.81 | 709 | 719 | 13.2 |
| 439971 | 705.51 | 709 | 719 | 13.5 |
| 438740 | 705.3 | 709 | 719 | 13.7 |
| 437996 | 705.21 | 709 | 719 | 13.8 |
| 437265 | 705.03 | 709 | 719 | 14.0 |
| 436536 | 704.27 | 708 | 718 | 13.7 |
| 435810 | 703.05 | 706 | 716 | 13.0 |
| 435043 | 702.4 | 704 | 714 | 11.6 |
| 434953 | 701.08 | 702 | 712 | 10.9 |
| 433730 | 700.47 | 701 | 711 | 10.5 |
| 433539 | 700.39 | 701 | 711 | 10.6 |
| | | | | |

Table C2-1 Comparison of Projected Flooding Levels and Perimeter Berm

Stormwater Detention and Sedimentation Pond

The proposed stormwater pond for the landfill is within the 100-year floodplain. The pond will be excavated below grade and include above grade compacted soil berms to provide additional volume. The purpose of the pond is to provide detention and sedimentation capacity for the landfill. The pond will be constructed at the same location as the existing stormwater pond and the proposed soil berms will be tied into the existing landfill perimeter berm to minimize the encroachment on the floodplain. In order to offset the loss of flow area in the floodplain from the pond berm, the area south of the new pond is proposed to be excavated to enhance flow through Cibolo Creek. A no-rise certification for the proposed pond was submitted to the City of Schertz for review and a copy of the submittal is included in Appendix C2-B. Based on the modeling in the no-rise certification, there is no increase in the calculated water surface elevation of the floodplain from the pond construction, since the areas along the creek will be excavated to completely offset any effects of the new pond.

The City of Schertz approved the no-rise certification for the pond construction on October 20, 2022.

Since the pond will be located within the floodplain and floodway of Cibolo Creek, the proposed location was evaluated by Power Engineers, Inc. to determine if any Waters of the U.S. (WOTUS) would be impacted by the construction. Attachment K in Part II of this amendment application includes the wetlands report and WOTUS evaluation. As shown on Figure 3 in Attachment K, no WOTUS features are present in the location of the existing sedimentation pond/proposed detention pond. Therefore, a U.S. Army Corps of Engineers permit is not required under Section 404 of the Clean Water Act.

Compliance with Chapter 301

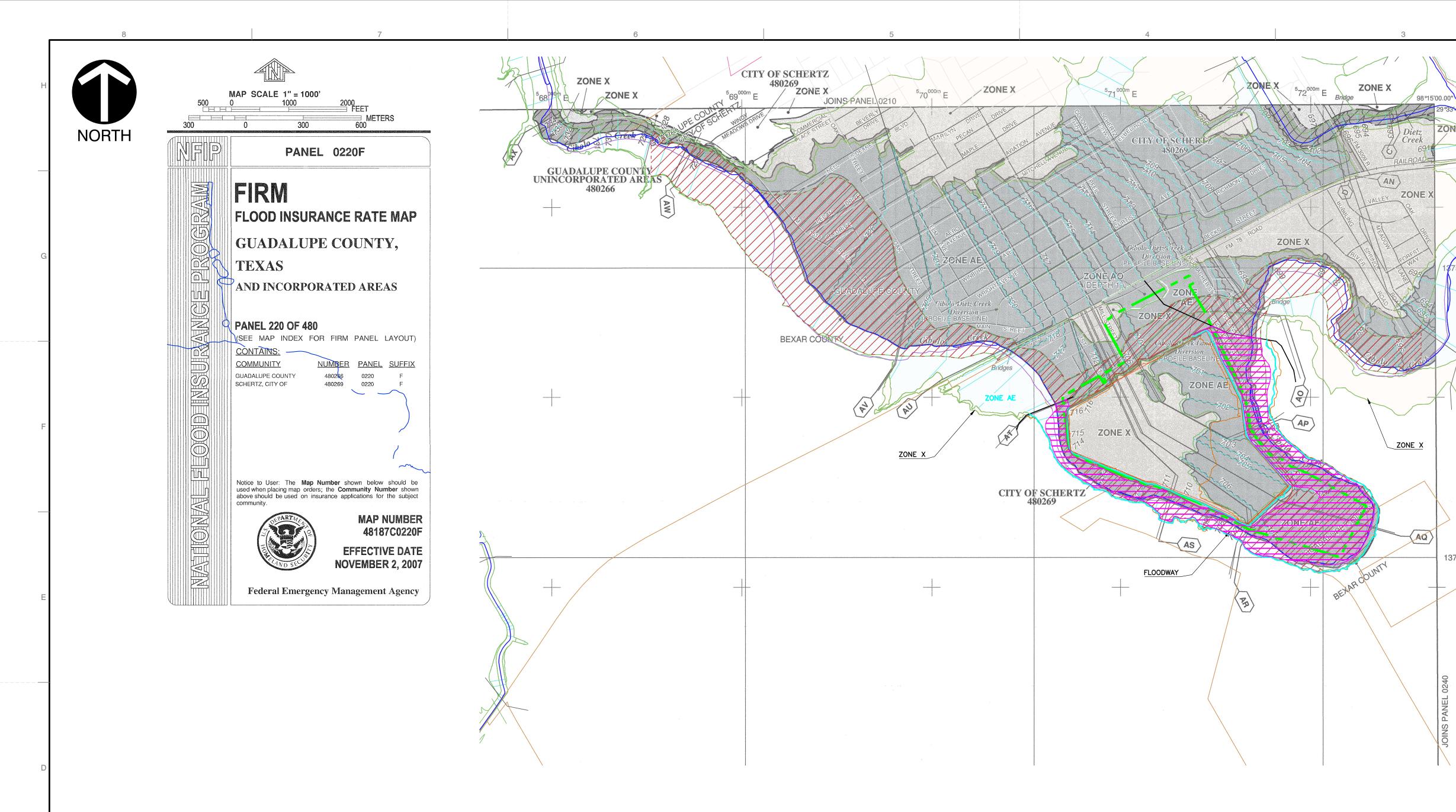
The existing levee and the proposed pond construction have been reviewed and approved by the City of Schertz and are exempt from the requirements of 30TAC pursuant to §301.2(3)(A) and Texas Water Code Section 16.236(h)(3) which states:

(h) Subsection (a) of this section does not apply to:...

(3) a levee or other improvement within the corporate limits of a city or town provided:

(a) plans for the construction or maintenance or both must be approved by the city or town as a condition precedent to starting the project and

(b) the city or town requires that such plans be in substantial compliance with rules and standards adopted by the commission;

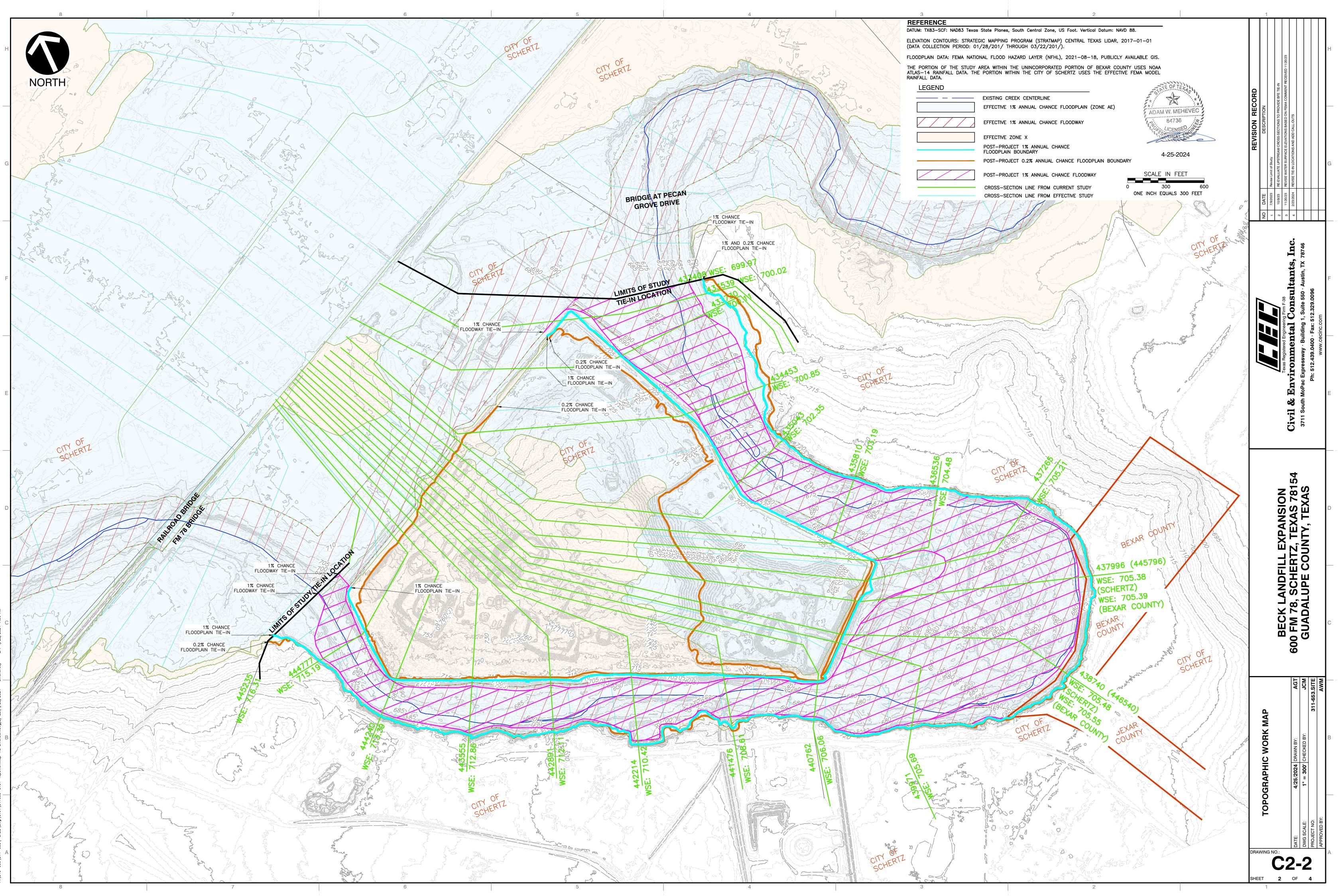


REFERENCE

AERIAL IMAGERY PROVIDER: GOOGLE EARTH; DATE OF PHOTOGRAPHY: 11/22/2019.

ELEVATION CONTOURS: STRATEGIC MAPPING PROGRAM (STRATMAP) CENTRAL TEXAS LIDAR, 2017–01–01 (DATA COLLECTION PERIOD: 01/28/201/ THROUGH 03/22/201/).

| | 2 | 1 | <u> </u> |
|--------------------|---|---|--|
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| 745000 FT | ZONE X Areas of 0.2% annual chance flood; areas of 1% annual chance flood annual chance flood. Image: Constraint and areas protected by levees from 1% annual chance flood. Image: Constraint and areas protected by levees from 1% annual chance flood. Image: Constraint and areas protected by levees from 1% annual chance flood. Image: Constraint and areas protected by levees from 1% annual chance flood. Image: Constraint and areas protected by levees from 1% annual chance flood. Image: Constraint and areas protected by levees from 1% annual chance flood. Image: Constraint and areas protected by levees from 1% annual chance flood. Image: Constraint and areas protected by levees from 1% annual chance flood. Image: Constraint and areas protected by levees from 1% annual chance flood. Image: Constraint and areas in which flood hazards are undetermined, but possible. Image: Constraint and areas in which flood hazards are undetermined. Image: Constraint and only flood f | | Civil & Environmental Consultants, Inc 3711 South MoPac Expressway · Building 1, Suite 550 · Austin, TX 78746 Ph: 512.439.0400 · Fax: 512.329.0096 www.cecinc.com |
| | 97:07:30*, 32:22:30* Geographic coordinates referenced to the North American Datum of 1983 (NAD 83) 4275:000mN 1000-meter Universal Transverse Mercator grid ticks, zone 14 6000000 FT 5000-foot grid values: Texas State Plane coordinate system, south central zone (FIPSZONE 4204), Lambert Conformal Conic DX55:10 Bench mark (see explanation in Notes to Users section of this FIRM panel) M1.5 River Mile MAP REPOSITORIES Refer to Map Repositories list on Map Index EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP November 2, 2007 EFFECTIVE DATE (S) OF REVISION(S) TO THIS PANEL EEGEEND LANDFILL PERMIT BOUNDARY LANDFILL FOOTPRINT BOUNDARY | BECK LANDFILL EXPANSION | 600 FM 78, SCHERTZ, TEXAS 78154 GUADALUPE COUNTY, TEXAS |
| | | RATE MAP (FIRM) 0220F | DRAWN BY: AGT CHECKED BY: JCM 311-653.SITE AWM |
| | ADAM W. MEHEVEC | FLOOD INSURANCE RATE 48187C0220F | 12/21/2022 SCALE: 1" = 1000' ECT NO: OVED BY: |
| | | I | DATE: DWG PROJI |



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FOR PERMIT PURPOSES ONLY

Part III – Attachment C2 – Flood Control Analysis Beck Landfill, Permit No. MSW-1848A

BECK LANDFILL APPENDIX C2-A LOMR Application and Approval Letter



Federal Emergency Management Agency

Washington, D.C. 20472 June 18, 2024

CERTIFIED MAIL RETURN RECEIPT REQUESTED

The Honorable Peter Sakai Bexar County Judge 101 West Nueva Street, 10th Floor San Antonio, TX 78205 IN REPLY REFER TO:

Case No.:2Community Name:ECommunity No.:4Effective Date ofThis Revision:N

22-06-2567P Bexar County, TX 480035 November 4, 2024

Dear Judge Sakai:

The Flood Insurance Study (FIS) report and Flood Insurance Rate Map (FIRM) for your community have been revised by this Letter of Map Revision (LOMR). Please use the enclosed annotated map panels revised by this LOMR for floodplain management purposes and for all flood insurance policies and renewals issued in your community.

Additional documents are enclosed that provide information regarding this LOMR. Please see the List of Enclosures below to determine which documents are included. Other enclosures specific to this request may be included as referenced in the Determination Document. If you have any questions regarding floodplain management regulations for your community or the National Flood Insurance Program (NFIP) in general, please contact the Consultation Coordination Officer for your community. If you have any technical questions regarding this LOMR, please contact the Director, Mitigation Division of the Department of Homeland Security's Federal Emergency Management Agency (FEMA) in Denton, Texas, at (940) 898-5127, or the FEMA Mapping and Insurance eXchange toll free at 1-877-336-2627 (1-877-FEMA MAP). Additional information about the NFIP is available on our website at https://www.fema.gov/flood-insurance.

Sincerely,

Allt

Patrick "Rick" F. Sacbibit, P.E., Branch Chief Engineering Services Branch Federal Insurance and Mitigation Administration

List of Enclosures:

Letter of Map Revision Determination Document Annotated Flood Insurance Rate Map Annotated Flood Insurance Study Report

cc: The Honorable Ralph Gutierrez Mayor, City of Schertz

> Doug Letbetter, CFM Floodplain Administrator City of Schertz

> Robert Brach, P.E., CFM Floodplain Administrator Bexar County

Adam Mehevec, P.E. Vice President Civil and Environmental Consultants, Inc.



Federal Emergency Management Agency

Washington, D.C. 20472

June 18, 2024

CERTIFIED MAIL RETURN RECEIPT REQUESTED

The Honorable Ralph Gutierrez Mayor, City of Schertz 1400 Schertz Parkway Schertz, TX 78154 IN REPLY REFER TO:

Case No.: Community Name: Community No.: Effective Date of This Revision:

22-06-2567P City of Schertz, TX 480269 November 4, 2024

Dear Mayor Gutierrez:

The Flood Insurance Study (FIS) report and Flood Insurance Rate Map (FIRM) for your community have been revised by this Letter of Map Revision (LOMR). Please use the enclosed annotated map panels revised by this LOMR for floodplain management purposes and for all flood insurance policies and renewals issued in your community.

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Sincerely,

Allt

Patrick "Rick" F. Sacbibit, P.E., Branch Chief Engineering Services Branch Federal Insurance and Mitigation Administration

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cc: The Honorable Peter Sakai Bexar County Judge

> Robert Brach, P.E., CFM Floodplain Administrator Bexar County

> Doug Letbetter, CFM Floodplain Administrator City of Schertz

Adam Mehevec, P.E. Vice President Civil and Environmental Consultants, Inc.



Federal Emergency Management Agency Washington, D.C. 20472

Washington, D.C. 20472

LETTER OF MAP REVISION DETERMINATION DOCUMENT

| | COMMUNITY AND REVISION INFORMATION | PROJECT DESCRIPTION | BASIS OF REQUEST |
|---|--|---|--|
| COMMUNITY | City of Schertz Bexar and Guadalupe Counties Texas COMMUNITY NO.: 480269 | FILL | 1D HYDRAULIC ANALYSIS FLOODWAY UPDATED TOPOGRAPHIC DATA |
| IDENTIFIER | Beck Landfill | APPROXIMATE LATITUDE AND LONG SOURCE: Other DATUM: NAD | |
| | ANNOTATED MAPPING ENCLOSURES | a contract of the second | JDY ENCLOSURES |
| TYPE: FIRM* TYPE: FIRM* | NO.: 48029C0295F DATE: September 29, 2010 NO.: 48187C0220F DATE: November 2, 2007 | DATE OF EFFECTIVE FLOOD INSURA PROFILES: 40P, 41P | pe County |
| Enclosures reflect * FIRM - Flood Ins | changes to flooding sources affected by this revision. urance Rate Map | · | |
| | FLOODING SOURCE | AND REVISED REACH | |
| | n approximately 280 feet upstream of Nu Pecan Grove to approx | | |
| | | DF REVISIONS Deding Revised Flooding | Increases Decreases |
| Flooding Source Cibolo Creek | Effective Floo BFEs* Floodway Zone X (shade Zone AE | BFEs Floodway | YES YES YES YES YES YES YES YES |
| * BFEs - Base Floo | od Elevations | | |
| | DETERM | MINATION | |
| regarding a requ a revision to the warranted. Thi | provides the determination from the Department of Home uest for a Letter of Map Revision (LOMR) for the area des flood hazards depicted in the Flood Insurance Study (FIS is document revises the effective NFIP map, as indicated by this LOMR for floodplain management purposes and for | scribed above. Using the information S) report and/or National Flood Insura in the attached documentation. Plea | submitted, we have determined that nce Program (NFIP) map is se use the enclosed annotated map |
| questions about thi Clearinghouse, 360 | is based on the flood data presently available. The enclosed docum is document, please contact the FEMA Mapping and Insurance eXcha 01 Eisenhower Avenue, Suite 500, Alexandria, VA 22304-6426. Ad <u>iovflood-insurance</u> . | ange toll free at 1-877-336-2627 (1-877-FEMA | MAP) or by letter addressed to the LOMC |
| | al. | let | |
| | Patrick "Rick" F. Sac Engineering Service | bibit, P.E., Branch Chief s Branch | |

Federal Insurance and Mitigation Administration

22-06-2567P

102-I-A-C

| Page 2 of 5 | Issue Date: June 18, 2024 |
|-------------|---------------------------|
|-------------|---------------------------|

Effective Date: November 4, 2024



Federal Emergency Management Agency Washington, D.C. 20472

LETTER OF MAP REVISION DETERMINATION DOCUMENT (CONTINUED)

OTHER COMMUNITIES AFFECTED BY THIS REVISION

CID Number: 480035

Name: Bexar County, Texas

| AFFECTED | MAP PANELS | AFFECTED PORTIONS OF THE FLOOD INSURANCE STUDY REPORT |
|----------------------------|-----------------------------|--|
| TYPE: FIRM* NO.: 48029C029 | 5F DATE: September 29, 2010 | DATE OF EFFECTIVE FLOOD INSURANCE STUDY: July 19, 2023 PROFILES: 40P, 41P |

This determination is based on the flood data presently available. The enclosed documents provide additional information regarding this determination. If you have any questions about this document, please contact the FEMA Mapping and Insurance eXchange toll free at 1-877-336-2627 (1-877-FEMA MAP) or by letter addressed to the LOMC Clearinghouse, 3601 Eisenhower Avenue, Suite 500, Alexandria, VA 22304-6426. Additional Information about the NFIP is available on our website at https://www.fema.govflood-insurance.

Patrick "Rick" F. Sacbibit, P.E., Branch Chief Engineering Services Branch Federal Insurance and Mitigation Administration

22-06-2567P

102-I-A-C

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Federal Emergency Management Agency

Washington, D.C. 20472

LETTER OF MAP REVISION DETERMINATION DOCUMENT (CONTINUED)

COMMUNITY INFORMATION

APPLICABLE NFIP REGULATIONS/COMMUNITY OBLIGATION

We have made this determination pursuant to Section 206 of the Flood Disaster Protection Act of 1973 (P.L. 93-234) and in accordance with the National Flood Insurance Act of 1968, as amended (Title XIII of the Housing and Urban Development Act of 1968, P.L. 90-448), 42 U.S.C. 4001-4128, and 44 CFR Part 65. Pursuant to Section 1361 of the National Flood Insurance Act of 1968, as amended, communities participating in the NFIP are required to adopt and enforce floodplain management regulations that meet or exceed NFIP criteria. These criteria, including adoption of the FIS report and FIRM, and the modifications made by this LOMR, are the minimum requirements for continued NFIP participation and do not supersede more stringent State/Commonwealth or local requirements to which the regulations apply.

We provide the floodway designation to your community as a tool to regulate floodplain development. Therefore, the floodway revision we have described in this letter, while acceptable to us, must also be acceptable to your community and adopted by appropriate community action, as specified in Paragraph 60.3(d) of the NFIP regulations.

COMMUNITY REMINDERS

We based this determination on the base (1-percent-annual-chance) flood discharges computed in the FIS for your community without considering subsequent changes in watershed characteristics that could increase flood discharges. Future development of projects upstream could cause increased flood discharges, which could cause increased flood hazards. A comprehensive restudy of your community's flood hazards would consider the cumulative effects of development on flood discharges subsequent to the publication of the FIS report for your community and could, therefore, establish greater flood hazards in this area.

Your community must regulate all proposed floodplain development and ensure that permits required by Federal and/or State/Commonwealth law have been obtained. State/Commonwealth or community officials, based on knowledge of local conditions and in the interest of safety, may set higher standards for construction or may limit development in floodplain areas. If your State/Commonwealth or community has adopted more restrictive or comprehensive floodplain management criteria, those criteria take precedence over the minimum NFIP requirements.

We will not print and distribute this LOMR to primary users, such as local insurance agents or mortgage lenders; instead, the community will serve as a repository for the new data. We encourage you to disseminate the information in this LOMR by preparing a news release for publication in your community's newspaper that describes the revision and explains how your community will provide the data and help interpret the NFIP maps. In that way, interested persons, such as property owners, insurance agents, and mortgage lenders, can benefit from the information.

This revision has met our criteria for removing an area from the base floodplain to reflect the placement of fill. However, we encourage you to require that the lowest adjacent grade and lowest floor (including basement) of any structure placed within the subject area be elevated to or above the Base (1-percent-annual-chance) Flood Elevation.

This determination is based on the flood data presently available. The enclosed documents provide additional information regarding this determination. If you have any questions about this document, please contact the FEMA Mapping and Insurance eXchange toll free at 1-877-336-2627 (1-877-FEMA MAP) or by letter addressed to the LOMC Clearinghouse, 3601 Eisenhower Avenue, Suite 500, Alexandria, VA 22304-6426. Additional Information about the NFIP is available on our website at https://www.fema.govflood-insurance.

Patrick "Rick" F. Sacbibit, P.E., Branch Chief Engineering Services Branch Federal Insurance and Mitigation Administration

22-06-2567P



Federal Emergency Management Agency

Washington, D.C. 20472

LETTER OF MAP REVISION DETERMINATION DOCUMENT (CONTINUED)

We have designated a Consultation Coordination Officer (CCO) to assist your community. The CCO will be the primary liaison between your community and FEMA. For information regarding your CCO, please contact:

Roosevelt Grant Director, Mitigation Division Federal Emergency Management Agency, Region VI 800 North Loop 288 Denton, TX 76209 (940) 898-5127

STATUS OF THE COMMUNITY NFIP MAPS

We will not physically revise and republish the FIRM and FIS report for your community to reflect the modifications made by this LOMR at this time. When changes to the previously cited FIRM panel and FIS report warrant physical revision and republication in the future, we will incorporate the modifications made by this LOMR at that time.

This determination is based on the flood data presently available. The enclosed documents provide additional information regarding this determination. If you have any questions about this document, please contact the FEMA Mapping and Insurance eXchange toll free at 1-877-336-2627 (1-877-FEMA MAP) or by letter addressed to the LOMC Clearinghouse, 3601 Eisenhower Avenue, Suite 500, Alexandria, VA 22304-6426. Additional Information about the NFIP is available on our website at https://www.fema.govflood-insurance.

Patrick "Rick" F. Sacbibit, P.E., Branch Chief Engineering Services Branch Federal Insurance and Mitigation Administration

22-06-2567P

102-I-A-C

| | Page 5 of 5 | Issue Date: June 18, 2024 |
|--|-------------|---------------------------|
|--|-------------|---------------------------|

Effective Date: November 4, 2024



Federal Emergency Management Agency

Washington, D.C. 20472

LETTER OF MAP REVISION DETERMINATION DOCUMENT (CONTINUED)

PUBLIC NOTIFICATION OF REVISION

A notice of changes will be published in the *Federal Register*. This information also will be published in your local newspaper on or about the dates listed below, and through FEMA's Flood Hazard Mapping website at https://www.floodmaps.fema.gov/fhm/bfe_status/bfe_main.asp

LOCAL NEWSPAPER

Name: *San Antonio Business Journal* Dates: June 28, 2024 and July 5, 2024

Within 90 days of the second publication in the local newspaper, any interested party may request that we reconsider this determination. Any request for reconsideration must be based on scientific or technical data. Therefore, this letter will be effective only after the 90-day appeal period has elapsed and we have resolved any appeals that we receive during this appeal period. Until this LOMR is effective, the revised flood hazard determination presented in this LOMR may be changed.

This determination is based on the flood data presently available. The enclosed documents provide additional information regarding this determination. If you have any questions about this document, please contact the FEMA Mapping and Insurance eXchange toll free at 1-877-336-2627 (1-877-FEMA MAP) or by letter addressed to the LOMC Clearinghouse, 3601 Eisenhower Avenue, Suite 500, Alexandria, VA 22304-6426. Additional Information about the NFIP is available on our website at https://www.fema.gov/flood-insurance.

Patrick "Rick" F. Sacbibit, P.E., Branch Chief Engineering Services Branch Federal Insurance and Mitigation Administration

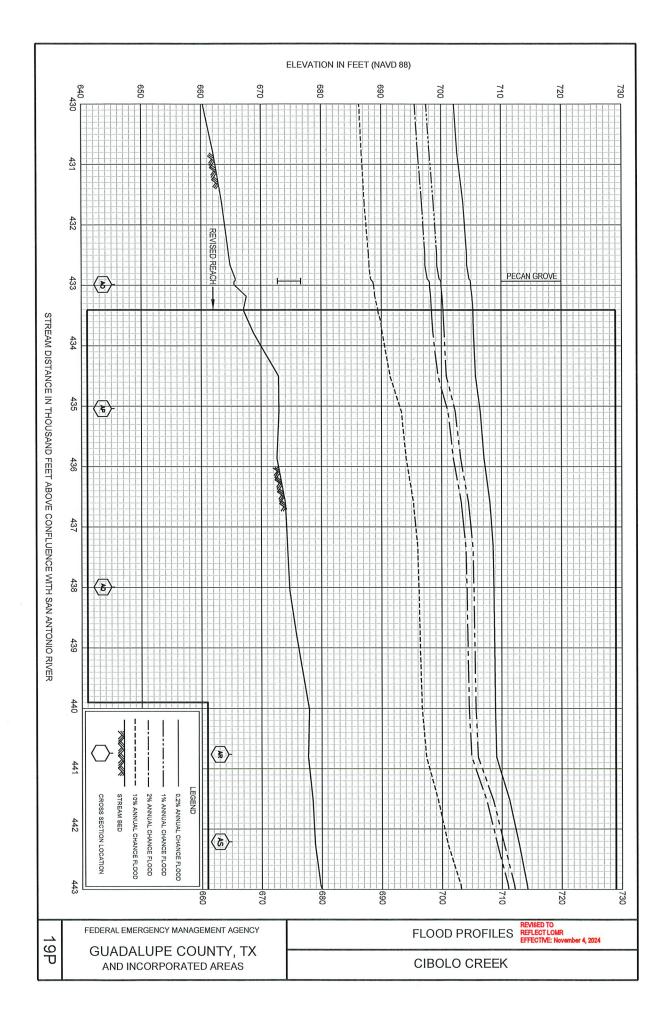
22-06-2567P

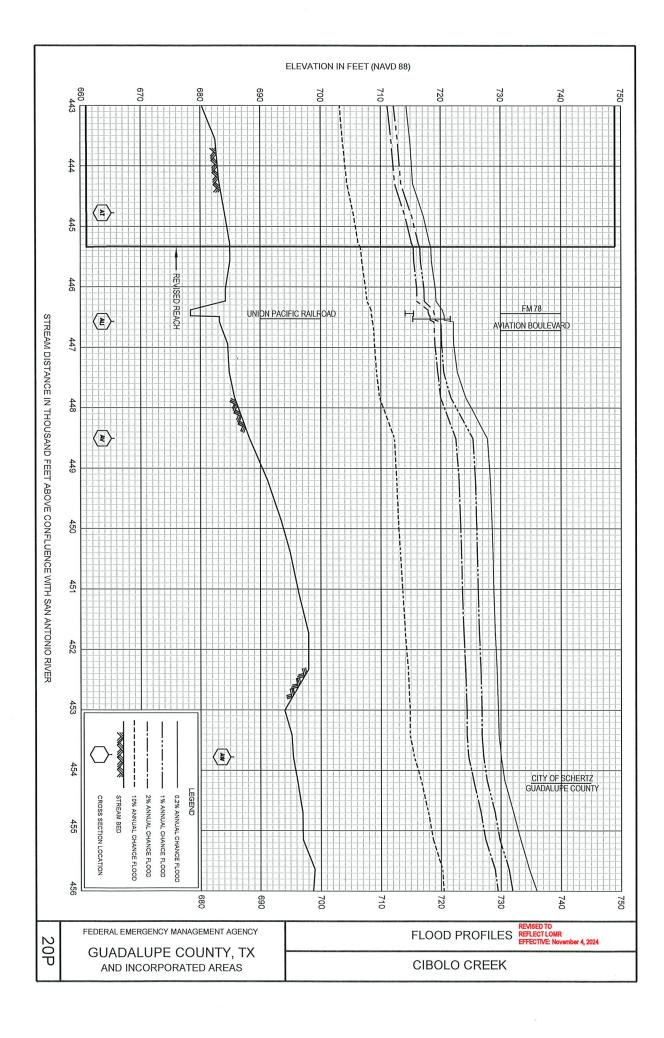
102-I-A-C

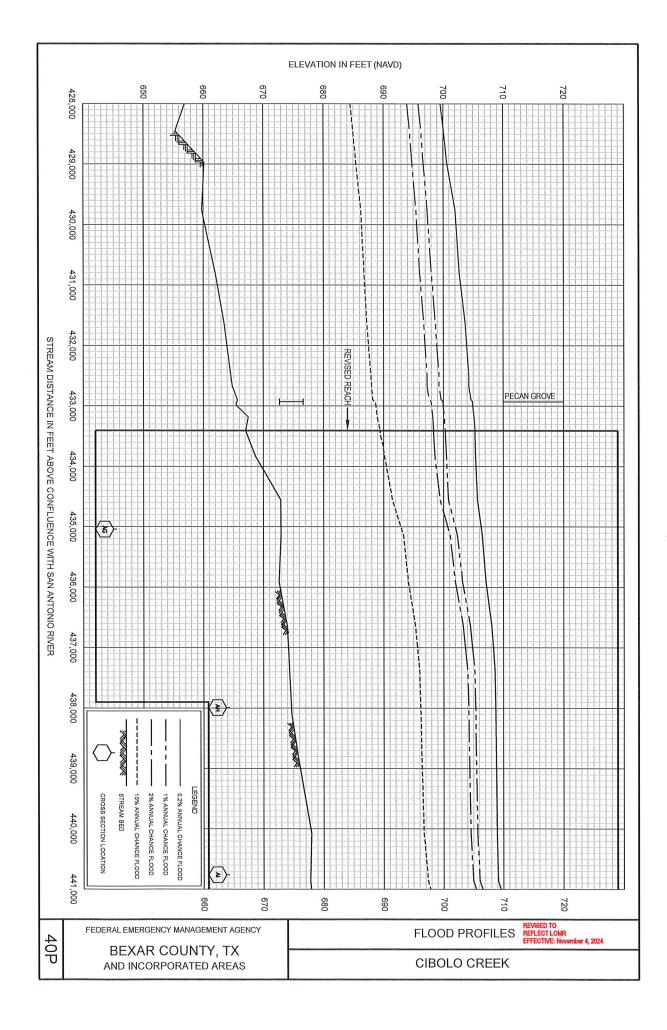
Table 23: Floodway Data, (continued)

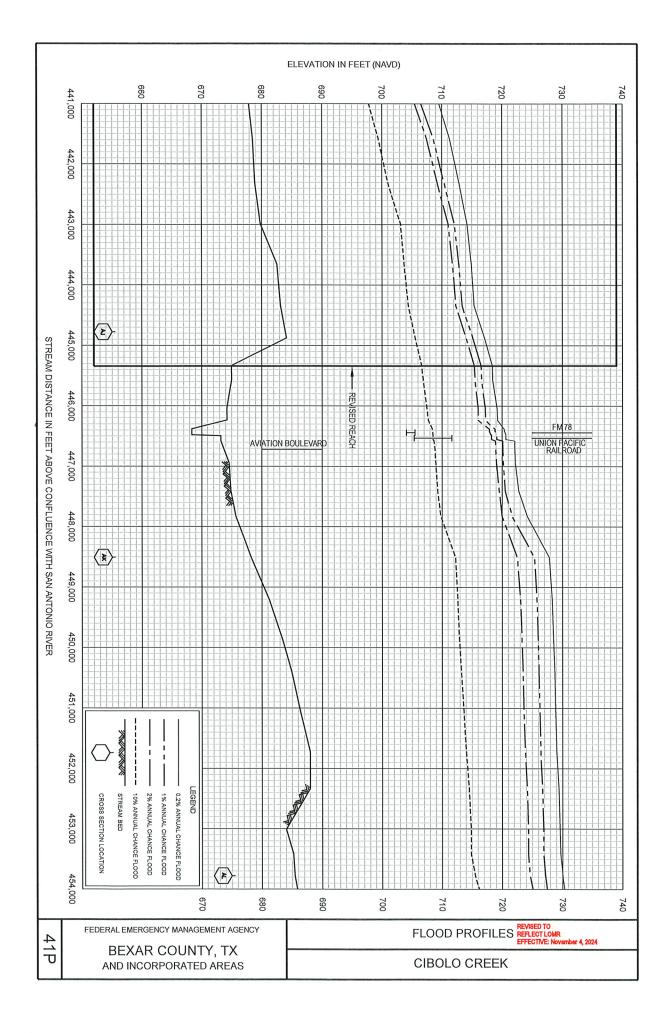
| IRFACE | INCREASE | 0.7 | 0.5 | 0.9 | 1.0 | 0.8 | 0.3 | 0.6 | 0.6 | 0.7 | 0.6 | 0.2 | 0.0 | 0.1 | 0.5 | 0.4 | 0.3 | 0.3 | 0.8 | 0.8 | | | REFLECT LOMR EFFECTIVE: November 4, 2024 | | | × |
|---|--------------------------------|-----------|-----------|---------|---------|---------|-----------|------------|-----------|-----------|-----------|---------|-----------|---------|---------|---------|---------|---------|---------|-----------|--|--------------|---|---------------------------------|------------------------|-------------------------------|
| DOD WATER SL ET NAVD88) | WITH FLOODWAY | 673.6 | 677.8 | 687.0 | 696.1 | 700.7 | 702.6 | 706.0 | 706.7 | 711.1 | 715.8 | 720.3 | 725.4 | 727.3 | 734.9 | 736.6 | 741.4 | 743.7 | 756.4 | 763.8 | | REVISED TO | REFLECT LOMR EFFECTIVE: Nov | ATA | | BOLO CREEI |
| 1% ANNUAL CHANCE FLOOD WATER SURFACE ELEVATION (FEET NAVD88) | WITHOUT FLOODWAY | 672.9 | 677.3 | 686.1 | 695.1 | 699.9 | 702.3 | 705.4 | 706.1 | 710.4 | 715.2 | 720.1 | 725.4 | 727.2 | 734.4 | 736.2 | 741.1 | 743.4 | 755.6 | 763.0 | | | | FLOODWAY DATA | | FLOODING SOURCE: CIBOLO CREEK |
| 1% ANNUA | REGULATORY | 672.9 | 677.3 | 686.1 | 695.1 | 699.9 | 702.3 | 705.4 | 706.1 | 710.4 | 715.2 | Λ 720.1 | 725.4 | 727.2 | 734.4 | 736.2 | 741.1 | 743.4 | 755.6 | 763.0 | | REVISED DATA | | | | FLOODING |
| | MEAN VELOCITY (FEET/SEC) | 5.1 | 6.0 | 8.6 | 6.2 | 5.5 | 7.0 | 2.6 | 11.4 | 8.4 | 8.1 | 7.5 | 4.3 | 9.2 | 8.9 | 10.4 | 8.3 | 8.5 | 8.7 | 3.4 | er | REVISE | | | ۰, | |
| FLOODWAY | SECTION AREA (SQ. FEET) | 19,543 | 16,568 | 11,662 | 14,018 | 15.893 | 10,722 | 29,239 | 6,535 | 8,907 | 9,205 | 11,130 | 23,287 | 10,812 | 11,277 | 9,648 | 12,019 | 11,748 | 11,482 | 29,405 | ian Antonio Rivei | | | GENCY | AS AS | |
| | WIDTH ² (FEET) | 1,906/190 | 2,490/113 | 693/52 | 592/521 | 800/631 | 423 / 236 | 1,476 / 23 | 260 / 100 | 498 / 142 | 351 / 128 | 435/199 | 1,025/862 | 661/169 | 446/310 | 412/113 | 457/268 | 499/223 | 408/139 | 1,496/824 | nfluence with S | | | NAGEMENT A | JNTY. TEX | TED AREAS |
| ION | DISTANCE ¹ | 418,516 | 419,470 | 423,625 | 427,183 | 432.987 | 435,041 | 437.996 | 440.762 | 442.214 | 444.777 | 446,577 | 448,507 | 453,783 | 456,713 | 457,901 | 459,264 | 460,345 | 466,729 | 471,196 | n feet above co in Countv | | | FEDERAL EMERGENCY MANAGEMENT AG | GUADALUPE COUNTY. TEXA | AND INCORPORATED AREAS |
| LOCATION | CROSS SECTION | AK | AL | AM | AN | AO | AP | AQ | AR | AS | AT | AU | AV | AW | AX | AY | AZ | BA | BB | BC | ¹ Stream distance in feet above confluence with San ² Width/Width Within County | | | FEDERAL EM | GUADA | AND |
| | | L | | | | | | | | | | | | | | | | | | | 1 | | | ТА | BLE | E 23 |

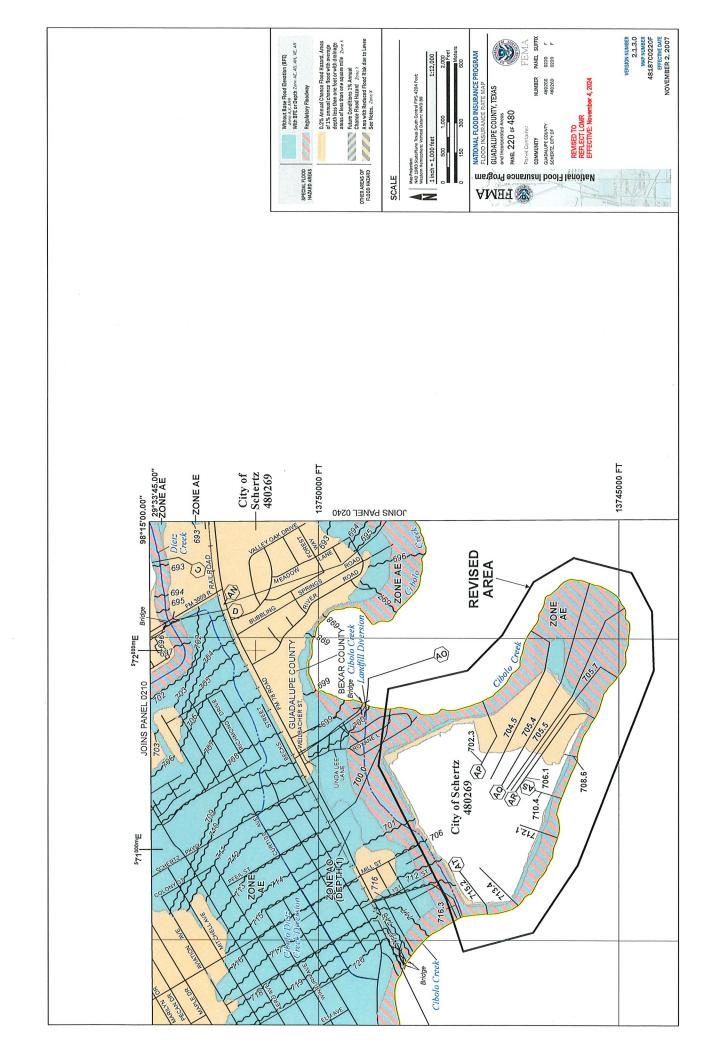
64

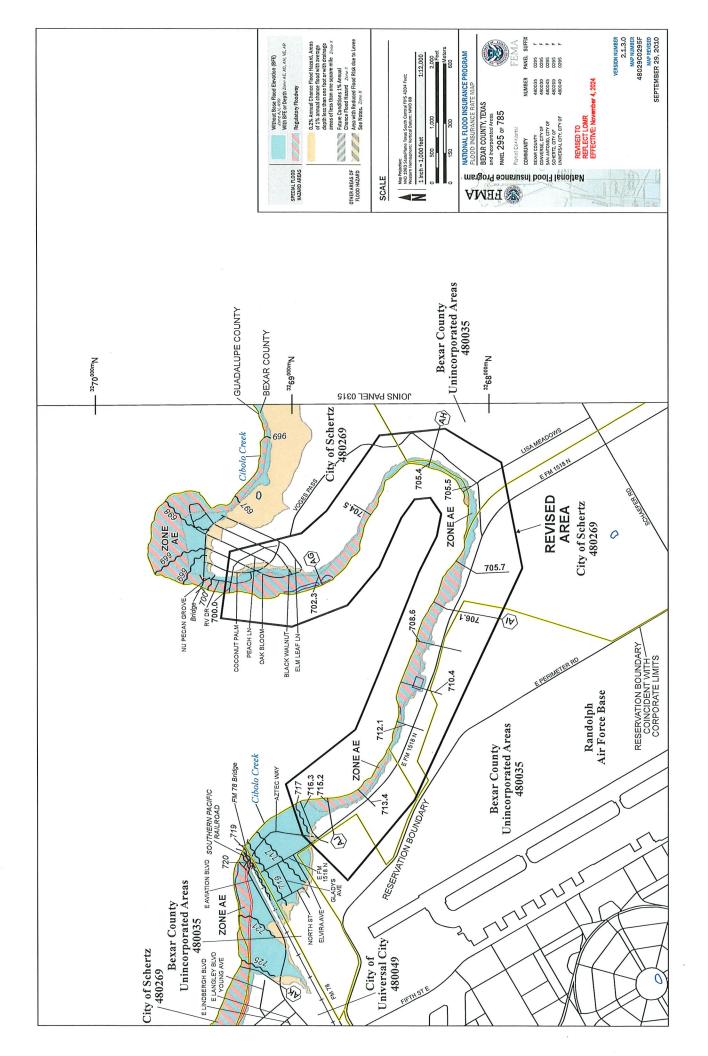












| From: | Tariq Makhdoom |
|----------|--|
| To: | Mehevec, Adam |
| Cc: | <u>dletbetter@schertz.com; Lokulutu, Bosulu</u> |
| Subject: | Revision Request Received – LOMR Case Number (22-06-2567P) – Guadalupe County, Texas and Incorporated Areas– Response Requested |
| Date: | Monday, August 15, 2022 12:17:21 PM |

Dear Adam Mehevec:

We have received your request that the Department of Homeland Security's Federal Emergency Management Agency (FEMA) issue a revision to the flood hazard information on the applicable National Flood Insurance Program (NFIP) map for Guadalupe County, Texas and Unincorporated Areas. This e-mail is being sent to officially acknowledge the receipt of your request and replaces the paper copy acknowledgement letters previously issued by FEMA. <u>We ask that you please</u> respond directly to this e-mail to verify that it has been received.

The case number assigned to your request is 22-06-2567P, and the project identifier is Beck Landfill.

We are reviewing your submitted data and will contact you if additional information is required to process your request.

If additional information is not required, we will issue a final letter of determination within 90 days of receiving your request. Please be aware that this LOMR will become effective approximately 4.5 months after the final letter of determination is issued.

If you have general questions about your request, FEMA policy, or the NFIP, please contact the FEMA Mapping and Insurance eXchange (FMIX), toll free, at 1-877-FEMA MAP (1-877-336-2627). If you have specific questions concerning your request, the case reviewer's contact information is listed below, or please contact the Revisions Coordinator for your State, Mr. Bosulu Lokulutu, E.I.T., CFM, by e-mail at <u>bosulu.lokulutu@aecom.com</u> or by telephone at (972) 735-7093.

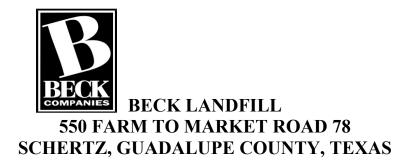
Please be assured we will do our best to respond to all inquiries in a timely manner.

Thank you,

M. Tariq Makhdoom, Ph.D., CFM

Taylor Engineering, Inc., a member of **Compass PTS JV** 10199 Southside Blvd., Suite 310, Jacksonville, FL 32256 Main: 904-731-7040 | Direct: 904 -553 - 5760 <u>TMakhdoom@Taylorengineering.Com</u>

LETTER OF MAP REVISION REQUEST FOR FIRM PANELS 48029C0295F AND 48187C0210F



Prepared By:

CIVIL & ENVIRONMENTAL CONSULTANTS, INC. AUSTIN, TEXAS (TEXAS P.E. FIRM F-38)

CEC Project 311-653

JUNE 2022



Civil & Environmental Consultants, Inc.



June 15, 2022

Attention: Kathryn Woodlee, PE, CFM

Subject: LOMR Application Case Number: Unassigned Floodplain Panels: 48187C0210F & 48029C0295F in Guadalupe County, TX NIDO. Ltd. CEC Project 311-653

Dear Kathryn,

This letter outlines the methodology used for the preparing the attached Letter of Map Revision (LOMR) request for the area immediately adjacent to the Beck Landfill located at 550 Farm-To-Market Road 78, Schertz, Texas.

The current FEMA map panels for the area around the landfill property are numbers 48187C0210F & 48029C0295F, which were revised in 2007 and 2010, respectively. At the time the model for these panels was created, the Beck Landfill was permitted to be filled to its final grades, but not yet constructed to an extent where the entire footprint was above the calculated 100-year water surface. FEMA modeled this permitted future condition by placing blocked obstructions on the cross-sections that traverse the landfill footprint, so that the model accounted for the authorized final condition of the landfill. FEMA then extended the floodplain across the portions of the landfill, that had not yet been constructed above the 100-year water surface elevations.

The entire footprint of the landfill has now been constructed above the 100-year water surface and Beck Landfill is submitting this LOMR application to revise the affected panels to accurately reflect the lateral extents of the floodplain. We have updated the cross-sections affected by the landfill with current topography and re-delineated the extents of the floodplain. The floodway shown on these panels has not been revised since the new topography did not affect the areas shown as floodway. We have also maintained the flow values included in the effective FEMA model.



Please feel free to contact me at (512) 329-0006 or <u>amehevec@cecinc.com</u> if you have any questions related to this LOMR application.

Sincerely,

CIVIL & ENVIRONMENTAL CONSULTANTS, INC. Texas Registered Engineering Firm F-38

4

Adam W. Mehevec, P.E. Principal



DEPARTMENT OF HOMELAND SECURITY Federal Emergency Management Agency **OVERVIEW & CONCURRENCE FORM**

OMB Control Number: 1660-0016 Expiration: 1/31/2024

| PAPERWORK BURDEN DISCLOSURE NOTICE | | | | | | | | | |
|---|---|--------|---------|-----------|----------------|--|--|--|--|
| Public reporting burden for this form is estimated to average 1 hours per response. The burden estimate includes the time for reviewing nstructions, searching existing data sources, gathering and maintaining the needed data, and completing, reviewing, and submitting the form. You are not required to respond to this collection of information unless it displays a valid OMB control number. Send comments regarding the accuracy of the burden estimate and any suggestions for reducing this burden to: Information Collections Management, Department of Homeland Security, Federal Emergency Management Agency, 500 C Street, SW, Washington, DC 20472, Paperwork Reduction Project (1660-0016). Submission of the form is required to obtain or retain benefits under the National Flood Insurance Program. Please do not send your completed survey to the above address . | | | | | | | | | |
| | PRIVACY ACT STATEMENT | | | | | | | | |
| Law 93-234. PRINCIPAL PURPOSI National Flood insuran ROUTINE USE(S): The as amended. This incl National Flood Insuran DISCLOSURE: The dis | AUTHORITY: The National Flood Insurance Act of 1968, Public Law 90-448, as amended by the Flood Disaster Protection Act of 1973, Public Law 93-234. PRINCIPAL PURPOSE(S): This information is being collected for the purpose of determining an applicant's eligibility to request changes to National Flood Insurance Program (NFIP) Flood Insurance Rate Maps (FIRM). ROUTINE USE(S): The information on this form may be disclosed as generally permitted under 5 U.S.C § 552a(b) of the Privacy Act of 1974, as amended. This includes using this information as necessary and authorized by the routine uses published in DHS/FEMA/NFIP/LOMA-1 National Flood Insurance Program (NFIP); Letter of Map Amendment (LOMA) February 15, 2006, 71 FR 7990. DISCLOSURE: The disclosure of information on this form is voluntary; however, failure to provide the information requested may delay or prevent FEMA from processing a determination regarding a requested change to a (NFIP) Flood Insurance Rate Maps (FIRM). | | | | | | | | |
| | A. REQUESTED RESPONSE FROM DH | S-FEMA | | | | | | | |
| CLOMR: revision or proposed hydrolog Endangered Speci | revision or proposed hydrology changes (See 44 CFR Ch. 1, Parts 60, 65 & 72). All CLOMRs require documentation of compliance with the Endangered Species Act. Refer to the Instructions for details. | | | | | | | | |
| | ··· B. OVERVIEW | | | | | | | | |
| 1. The NFIP map pa | anel(s) affected for all impacted communities is (are): | | 1 | | | | | | |
| Community No. | Community Name | State | Map No. | Panel No. | Effective Date | | | | |
| 480269 | City of Schertz; Guadalupe County | тх | 48187C | 0220F | 11/2/07 | | | | |
| 10 | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |

| 2. | a. Flooding Source: Cibe | olo Creek |
|----|--------------------------|---|
| | b. Types of Flooding: | Riverine Coastal Shallow Flooding (e.g., Zones AO and AH) |
| | | Alluvial Fan Lakes Other (Attach Description) |
| 3. | Project Name/Identifier: | Beck Landfill |
| 4. | FEMA zone designations | (choices: A, AH, AO, A1-A30, A99, AE, AR, V, V1-V30, VE, B, C, D, X) |
| | a. Effective: AE | |
| | b. Revised: AE | |

| 5. Basis for Request and Type of Revision: | | |
|---|---|---|
| a. The basis for this revision request is (check all that apply) | | |
| Physical Change Improved Methodology/Data | Regulatory Floodway Revision Ba | ase Map Changes |
| Coastal Analysis Hydraulic Analysis | Hydrologic Analysis | orrections |
| Weir-Dam Changes | 🔲 Alluvial Fan Analysis 📃 Na | atural Changes |
| New Topographic Data Other (Attach Description) | | |
| Note: A photograph and narrative description of the area of conce | rn is not required, but is very helpful during revie | ew. |
| b. The area of revision encompasses the following structures (che | eck all that apply) | |
| Structures: Channelization Levee/Floodwall | Bridge/Culvert | |
| Dam Fill | Other (Attach Description) | |
| 6. Documentation of ESA compliance is submitted (required to information. | initiate CLOMR review). Please refer to the instr | ructions for more |
| C. REVIE | W FEE | |
| Has the review fee for the appropriate request category been included? | X Yes Fee amount: \$ 8,000 | |
| | No, Attach Explanation | |
| - Please see the DHS-FEMA Web site at http://www.fema.go | | /flood- |
| map-related-fees for Fee Amounts and Exemption | S | |
| D. SIGNA | TURES | |
| 1. REQUESTOR'S SIGNATURE | | |
| All documents submitted in support of this request are correct to the to punishable by fine or imprisonment under Title 18 of the United States C | best of my knowledge. I understand that any fa Code, Section 1001. | alse statement may be |
| Name: Adam Mehevec | Company: Civil and Environmental Consultants | s, Inc. |
| Mailing Address: | Daytime Telephone: 512-225-8103 Fax N | No.: 512-329-0096 |
| 3711 S. Mopac Expressway, Bldg 1, Suite 550 | E-mail Address: amehevec@cecinc.com | |
| Austin, TX 78745 | Date: July 30, 2022 | |
| Signature of Requestor (required): | | |
| 2. COMMUNITY CONCURRENCE | | |
| As the community official responsible for floodplain management, I hereby a (LOMR) or conditional LOMR request. Based upon the community's review, we community floodplain management requirements, including the requirements for State, and local permits have been, or in the case of a conditional LOMR, will Endangered Species Act (ESA) compliance to FEMA prior to FEMA's review compliance with Sections 9 and 10 of the ESA has been achieved independent Federal or State agencies, documentation from the agency showing its completermined that the land and any existing or proposed structures to be remo 44CFR 65.2(c), and that we have available upon request by FEMA, all analyses | a find the completed or proposed project meets or is of or when fill is placed in the regulatory floodway, and the lobe obtained. For Conditional LOMR requests, the a of the Conditional LOMR application. For LOMR request, thy of FEMA's process. For actions authorized, funded iance with Section 7(a)(2) of the ESA will be submitting wed from the SFHA are or will be reasonably safe for | Jesigned to meet all of the hat all necessary Federal, applicant has documented juests, I acknowledge that ed, or being carried out by ted. In addition, we have |
| Community Official's Name and Title: Doug Letbetter, CFM | | |
| Mailing Address: | Community Name: City of Schertz | |
| 10 Commercial Place, Building 2 Schertz, TX 78154 6 AAAAA | | No.: 210-619-1849 |
| Dee Att | E-mail Address: dletbetter@schertz.com | |
| Community Official's Signature (required): | Date: 0 8-01- | -2022 |
| | | |

FEMA FORM FF-206-FY-21-100 (formerly 086-0-27) (01/21)

3. CERTIFICATION BY REGISTERED PROFESSIONAL ENGINEER AND/OR LAND SURVEYOR

This certification is to be signed and sealed by a licensed land surveyor, registered professional engineer, or architect authorized by law to certify elevation information data, hydrologic and hydraulic analysis, and any other supporting information as per NFIP regulations paragraph 65.2(b) and as described in the MT-2 Forms Instructions. All documents submitted in support of this request are correct to the best of my knowledge. I understand that any false statement may be punishable by fine or imprisonment under Title 18 of the United States Code, Section 1001.

| Certifier's Name: Adam W. Mehevec, PE | | License No.: 84736 | Expiration Date: 12/31/2022 |
|---|---------------------------|--|-----------------------------|
| Company Name: Civil and Environmental Consultants, In | IC. | Mailing Address: 3711 S. Mopac Expressway, | |
| Telephone No.: 512-225-8103 Fax No.: 512-329-0096 | | | |
| E-mail Address: amehevec@cecinc.com | | | |
| Signature: | | | Date: 7-30-2022 |
| Ensure the forms that are appropriate to your revisio | on request ar | e Included in your submittal. | |
| Form Name and (Number) | Required i | i <u>f</u> | TE OF TELLS |
| X Riverine Hydrology and Hydraulics Form (Form 2) | New or rev surface ele | vised discharges or water- evations | |
| Riverine Structures Form (Form 3) | bridge/culv | modified, addition/revision of verts, addition/revision of lwall, addition/revision of dam | ADAM W. MEHEVEC |
| Coastal Analysis Form (Form 4) | New or rev | vised coastal elevations | |
| Coastal Structures Form (Form 5) | Addition/re | evision of coastal structure | 7-31-22 |
| Alluvial Fan Flooding Form (Form 6) | Flood cont | trol measures on alluvial fans | Seal (Optional) |

DEPARTMENT OF HOMELAND SECURITY

Federal Emergency Management Agency

RIVERINE HYDROLOGY & HYDRAULICS FORM (FORM 2)

PAPERWORK BURDEN DISCLOSURE NOTICE

| instr You accu Hom (166 | lic reporting burden for this form is estimated to average 3.5 hours per response. The burden estimate includes the time for reviewing uctions, searching existing data sources, gathering and maintaining the needed data, and completing, reviewing, and submitting the form. are not required to respond to this collection of information unless it displays a valid OMB control number. Send comments regarding the iracy of the burden estimate and any suggestions for reducing this burden to: Information Collections Management, Department of heland Security, Federal Emergency Management Agency, 500 C Street, SW, Washington, DC 20472, Paperwork Reduction Project 60-0016). Submission of the form is required to obtain or retain benefits under the National Flood Insurance Program. Please do not send r completed survey to the above address. |
|--|---|
| | PRIVACY ACT STATEMENT |
| Law PRI Nati ROU as a Nati DIS | THORITY: The National Flood Insurance Act of 1968, Public Law 90-448, as amended by the Flood Disaster Protection Act of 1973, Public 93-234. NCIPAL PURPOSE(S): This information is being collected for the purpose of determining an applicant's eligibility to request changes to onal Flood Insurance Program (NFIP) Flood Insurance Rate Maps (FIRM). JTINE USE(S): The information on this form may be disclosed as generally permitted under 5 U.S.C § 552a(b) of the Privacy Act of 1974, amended. This includes using this information as necessary and authorized by the routine uses published in DHS/FEMA/NFIP/LOMA-1 onal Flood Insurance Program (NFIP); Letter of Map Amendment (LOMA) February 15, 2006, 71 FR 7990. CLOSURE: The disclosure of information on this form is voluntary; however, failure to provide the information requested may delay or rent FEMA from processing a determination regarding a requested change to a (NFIP) Flood Insurance Rate Maps (FIRM). |
| Floo | ding Source: Cibolo Creek |
| Note | e: Fill out one form for each flooding source studied |
| | A. HYDROLOGY |
| 1. | Reason for New Hydrologic Analysis (check all that apply): |
| | ➢ Not revised (skip to section B) |
| | Alternative methodology Proposed Conditions (CLOMR) Changed physical condition of watershed |
| 2. | Comparison of Representative 1%-Annual-Chance Discharges |
| | LocationDrainage Area (Sq. Mi.)Effective/FIS (cfs)Revised (cfs) |
| 3. | Methodology for New Hydrologic Analysis (check all that apply) |
| | Precipitation/Runoff Model → Specify Model: <u>Beck</u> Duration: <u>24-hr</u> Rainfall Amount: <u>13.2 (100vr)</u> |
| | Statistical Analysis of Gage Records |
| | Regional Regression Equations Other (please attach description) |
| | ase enclose all relevant models in digital format, maps, computations (including computation of parameters), and documentation to port the new analysis. |
| 4. | Review/Approval of Analysis |
| | If your community requires a regional, state, or federal agency to review the hydrologic analysis, please attach evidence of approval/review. 4. HEC-RAS File Description**: |
| 5. | Impacts of Sediment Transport on Hydrology |
| | Is the hydrology for the revised flooding source(s) affected by sediment transport? \Box Yes $	imes$ No |
| | If yes, then fill out Section F (Sediment Transport) of Form 3. If No, then attach your explanation. |

| B. HYDRAULICS | | | | | | | | | |
|---|---|---|--|--|--|--|--|--|--|
| 1. <u>F</u> | Reach to be Revised | | | | | | | | |
| | | Description | Cross S | Section | Water-Surface | Elevation (ft.) | | | |
| | | | | | Effective | Proposed/Revised | | | |
| C | Downstream Limit* | Watershed Stu | dy 4329 | 987 | 704.84 | 699.92 | | | |
| ι | Jpstream Limit* | Watershed Stu | dy 4463 | 383 | 719.48 | 717.88 | | | |
| *Proposed/Revised elevations must tie-into the Effective elevations within 0.5 foot at the downstream and upstream limits of revision. 2. <u>Hydraulic Method/Model Used:</u> <u>HFC-RAS</u> | | | | | | | | | |
| | X Steady State | Unsteady State | One-Dime | nsional | Two-Dimentional | | | | |
| 3. <u>F</u> | Pre-Submittal Review of H | <u>Hydraulic Models*</u> | | L | | | | | |
| mode | ls, respectively. We reco | ommend that you revie | | | n the review of HEC-2 and els with CHECK-2 and CHE | | | | |
| 4. ⊢ | IEC-RAS File Descriptior | י*: | | | | | | | |
| | Models Submitted | Natura | al Run | | Floodway Run | Datum | | | |
| Du | plicate Effective Model* | File Name: | Plan Name: | File Name | e: Plan Name: | | | | |
| | | | | | | | | | |
| Co | rrected Effective Model* | File Name: | Plan Name: | File Nam | e: Plan Name: | | | | |
| | isting or Pre-Project nditions Model | File Name: | Plan Name: | File Name | e: Plan Name: | | | | |
| | | CiboloCkR1LOMR | Cibolo Creek Update | | | | | | |
| | vised or Post-Project nditions Model | File Name: | Plan Name: | File Name | e: Plan Name: | | | | |
| | | Ele Niewer | Dian Naman | Eile Mana | | | | | |
| Otr | ner - (attach description) | File Name: | Plan Name: | File Nam | e: Plan Name: | | | | |
| * For | dataila, rafar ta tha aarra | anonding agotion of th | o instructions | | | | | | |
| **See | details, refer to the correst instructions for informati | on about modeling ot | her then HEC-RAS. | ⊠ Digital M | odels Submitted? (Require | d) | | | |
| | | | C. MAPPING REQ | UIREMENTS | | | | | |
| existin annua with st bound descrij | A certified topographic work map must be submitted showing the following information (where applicable): the boundaries of the effective, existing, and proposed conditions 1%-annual-chance floodplain (for approximate Zone A revisions) or the boundaries of the 1%- and 0.2%-annual-chance floodplains and regulatory floodway (for detailed Zone AE, AO, and AH revisions); location and alignment of all cross sections with stationing control indicated; stream, road, and other alignments (e.g., dams, levees, etc.); current community easements and boundaries; boundaries of the requester's property; certification of a registered professional engineer registered in the subject State; location and description of reference marks; and the referenced vertical datum (NGVD, NAVD, etc.). | | | | | | | | |
| - | graphic Information: | | | , | | | | | |
| Sourc | e: Strategic Mapping Pr | ogram Center Texas | LIDAR | | Date: 1/28/2021 through | n 3/22/2021 | | | |
| Vertica | al Datum: NAVD88 | | S | patial Projectio | n: | | | | |
| FBFM at the floodwa | hat the boundaries of the must tie-in with the effec same scale as the origin | tive floodplain and reg nal, annotated to sho undaries of the effect n revision. | gulatory floodway bou w the boundaries of | Indaries. Pleas the revised 19 nual-chance flo | e attach a copy of the eff %-and 0.2%-annual-chance bodplain and regulatory flo | on the revised FIRM and/or Fective FIRM and/or FBFM , e floodplains and regulatory odway at the upstream and | | | |

| | D. COMMON REGULATORY REQUIREMENTS* |
|----|---|
| 1. | For LOMR/CLOMR requests, do Base Flood Elevations (BFEs) or Special Flood Hazard Areas (SFHAs) increase compared to the effective BFEs? |
| | If Yes, please attach proof of property owner notification . Examples of property owner notifications can be found in the MT-2 Form 2 Instructions. |
| 2. | For CLOMR requests, if either of the following is true, please submit evidence of compliance with Section 65.12 of the NFIP regulations: |
| | The proposed project encroaches upon a regulatory floodway and would result in increases above 0.00 foot compared to pre-project conditions. |
| | The proposed project encroaches upon a SFHA with or without BFEs established and would result in increases above 1.00 foot compared to pre-project conditions. |
| 3. | Does the request involve the placement or proposed placement of fill? |
| | If Yes, the community must be able to certify that the area to be removed from the special flood hazard area, to include any structures or proposed structures, meets all of the standards of the local floodplain ordinances, and is reasonably safe from flooding in accordance with the NFIP regulations set forth at 44 CFR 60.3(A)(3), 65.5(a)(4), and 65.6(a)(14). Please see the MT-2 instructions for more information. |
| 4. | Does the request involve the placement or proposed placement of fill? |
| | If Yes, attach evidence of regulatory floodway revision notification . As per Paragraph 65.7(b)(1) of the NFIP Regulations, notification is required for requests involving revisions to the regulatory floodway Elements and examples of regulatory floodway revision notification can be found in the MT-2 Form 2 Instructions. |
| 5. | For CLOMR requests, please submit documentation to FEMA and the community to show that you have complied with Sections 9 and 10 of the Endangered Species Act (ESA). For actions authorized, funded, or being carried out by Federal or State agencies, please submit documentation from the agency showing its compliance with Section 7(a)(2) of the ESA. Please see the MT-2 instructions for more detail. |
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ENGINEERING & DRAINAGE REPORT

600 FM 78 SCHERTZ, GUADALUPE COUNTY TEXAS

Prepared For: NIDO, LTD.

Prepared By:

CIVIL & ENVIRONMENTAL CONSULTANTS, INC. AUSTIN, TEXAS

CEC Project 311-653

JUNE 2022





Civil & Environmental Consultants, Inc.

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APPENDICES

A. LOCATION MAP B. SOIL MAP – USDA NRCS C. EXISTING FEMA FIRM MAPS D. HEC-RAS HYDRAULIC RESULTS

1.0 GENERAL

1.1 PROJECT INTRODUCTION

The proposed project is to continue using the site for existing landfill purposes on the property located in Guadalupe County, Texas, consisting of approximately 154.6 acres within the Full Purpose Jurisdiction of the City of Schertz. The site lies within the Cibolo Creek Watershed and is not located within any zones of the Edwards Aquifer. This report accompanies a Letter of Map Revision (LOMR) submittal to revise the relevant floodplain maps to reflect the current topography of the site.

The current FEMA map panels for the area around the landfill property are numbers 48187C0210F & 48029C0295F, which were revised in 2007 and 2010, respectively. At the time the model for these panels was created, the Beck Landfill was permitted to be filled to its final grades, but not yet constructed to an extent where the entire footprint was above the calculated 100-year water surface. FEMA modeled this permitted future condition by placing blocked obstructions on the cross-sections that traverse the landfill footprint, so that the model accounted for the authorized final condition of the landfill. FEMA then extended the floodplain across the portions of the landfill, that had not yet been constructed above the 100-year water surface elevations.

The entire footprint of the landfill has now been constructed above the 100-year water surface and Beck Landfill is submitting this LOMR application to revise the affected panels to accurately reflect the lateral extents of the floodplain. The cross-sections affected by the landfill construction have been updated with current topography and we have re-delineated the extents of the floodplain. The floodway shown on these panels has not been revised since the new topography did not affect the areas shown as floodway. We have also maintained the flow values included in the effective FEMA model.

2.0 EXISTING CONDITIONS

2.1 ZONING

The site is currently zoned M-2 (Heavy Manufacturing), which allows for landfilling with the approval of a specific use permit. The landfill pre-dates the establishment of zoning in this area and therefore the current use is allowed to continue as long as there is no lateral expansion of the landfill.

2.2 TOPOGRAPHY AND STORMWATER CONVEYANCE PATTERNS

Cibolo Creek loops around three sides of the site, west, south, and east. The subject tract sheet flows into Cibolo Creek along three sides and into a constructed drainage channel on the north side. The site contains an operating landfill and the current topography of the landfill area has a high point elevation of approximately ± 785 feet Mean Sea Level (MSL) located near the northwest corner of the landfill. The low point elevation on the site is in Cibolo Creek near the northeast corner of the tract and is approximately ± 668 feet MSL. The site consists of varying slopes, with slopes along the creek from 1%-5%, while slopes in the landfill area are as steep as 33%. The native soils are mostly Sunev Loam with some areas of Barbarosa Silty Clay and Bosque and Seguin Soils. See the appendices of this report for a soil map.

2.3 FLOODPLAIN

According to FEMA Panel Numbers 48187C0220F and 48029C9295F effective November 2, 2007 and September 29, 2010 respectively, the majority of the site lies within the 100-year floodplain. The FIRMs are included in the appendices of this report.

2.4 UPSTREAM DRAINAGE AREAS

There is existing City of Schertz maintained storm water conveyance infrastructure south of the right-of-way (ROW) of John E. Peterson Blvd. The site is surrounded by Cibolo Creek and City

of Schertz public stormwater structures that divert stormwater around the site. Therefore there is no off-site drainage flowing onto the subject property other than the flow in Cibolo Creek. The hydrology data for the offsite flow in Cibolo Creek was taken from the effective FEMA model. Maps showing the general location and nature of the stormwater structures from the City of Schertz GIS are included in the appendices of this report. No offsite stormwater enters the landfill footprint.

3.0 PROPOSED CONDITIONS

3.1 DETENTION AND WATER QUALITY

There is no change in the stormwater flow rates associated with this LOMR submittal. The hydrology included in the effective FEMA model was maintained in the proposed condition. No detention or water quality ponds are proposed in conjunction with this LOMR submittal.

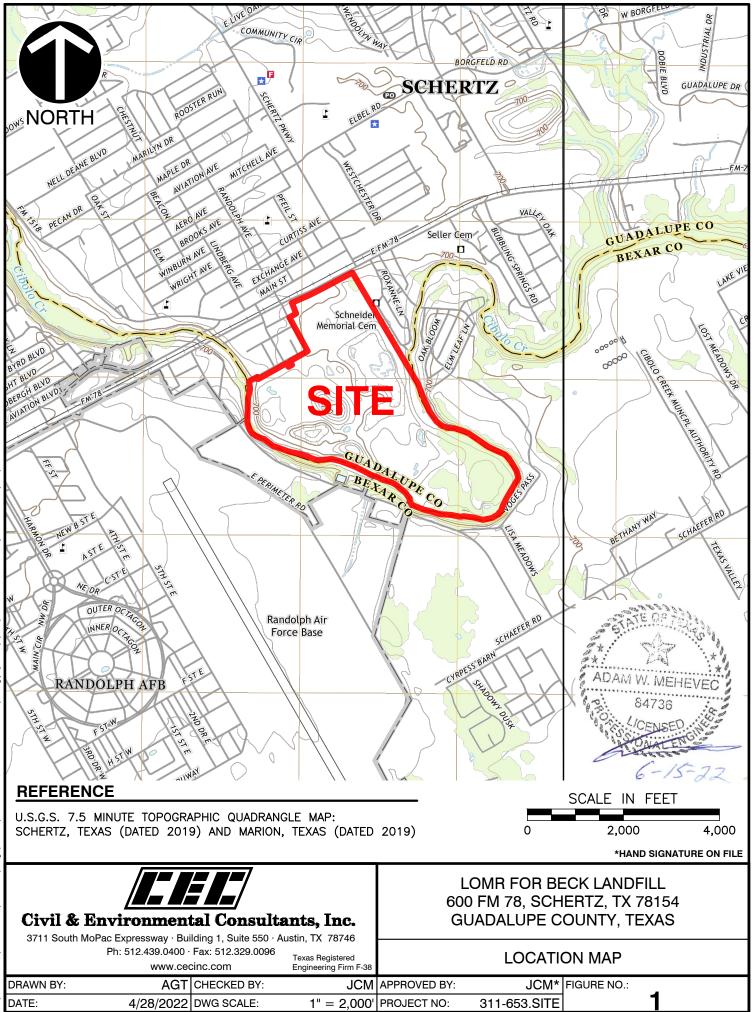
3.2 VARIANCES AND WAIVERS

No new variances or waivers are requested or planned for this development.

3.3 SOIL DISPOSAL

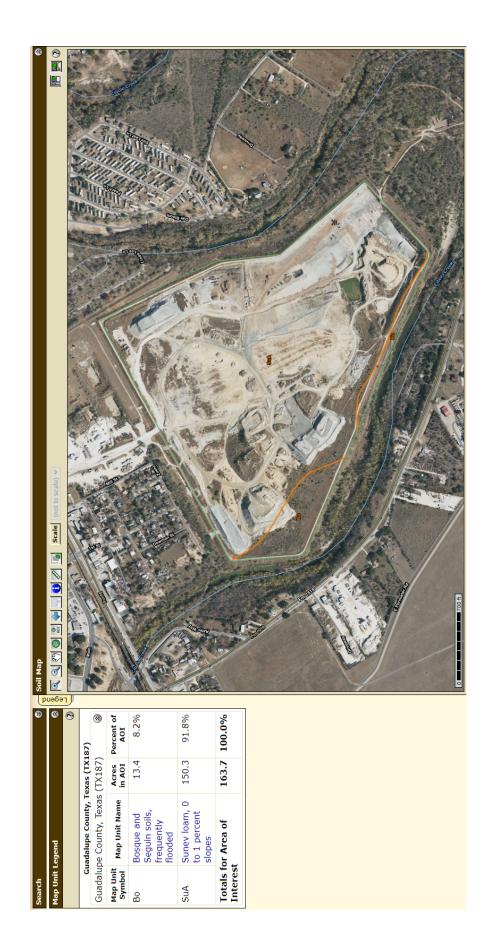
No improvements are proposes as part of this submittal, so there will not be any spoils generated.

LOCATION MAP

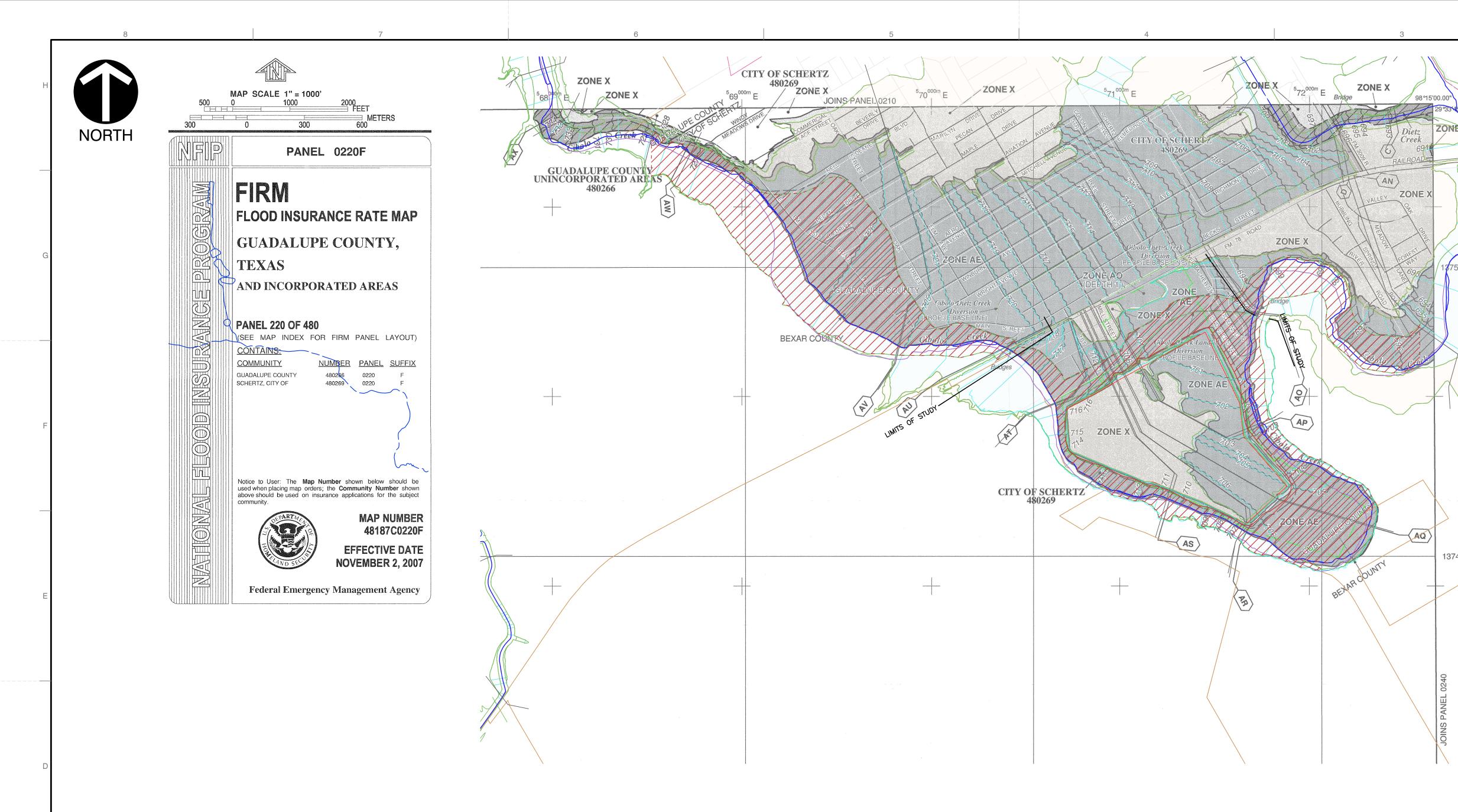


PM

SOIL MAP



FIRM MAPS



10-000\311-653\-CADD\Dwg\CV01\311653-CV01-AnnotatedFiRMmap.dwg{3} LS:(5/2/2022 - mvories) + LP: 5/16/2022 12:42 PW

REFERENCE

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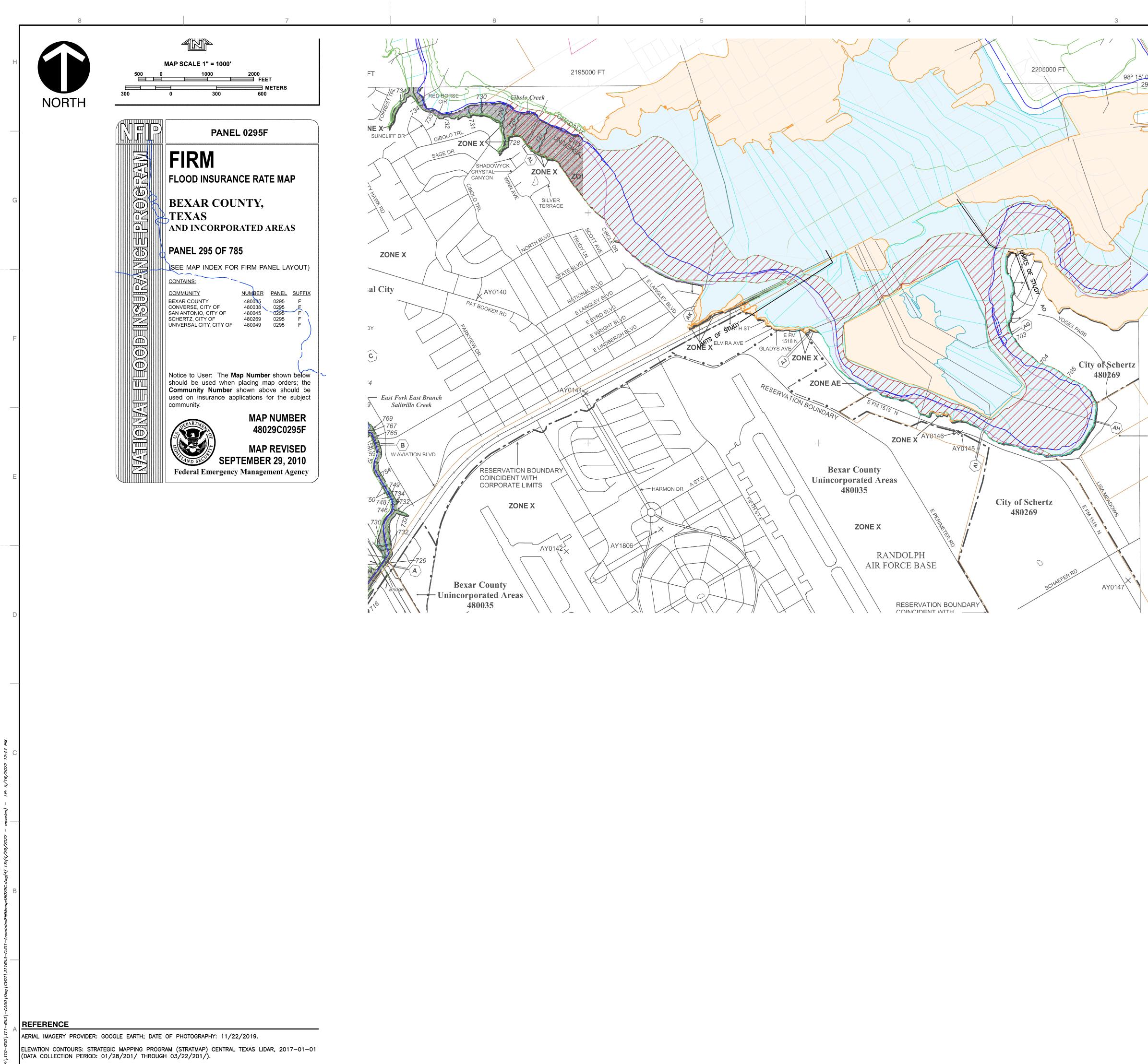
AERIAL IMAGERY PROVIDER: GOOGLE EARTH; DATE OF PHOTOGRAPHY: 11/22/2019. ELEVATION CONTOURS: STRATEGIC MAPPING PROGRAM (STRATMAP) CENTRAL TEXAS LIDAR, 2017-01-01 (DATA COLLECTION PERIOD: 01/28/201/ THROUGH 03/22/201/).

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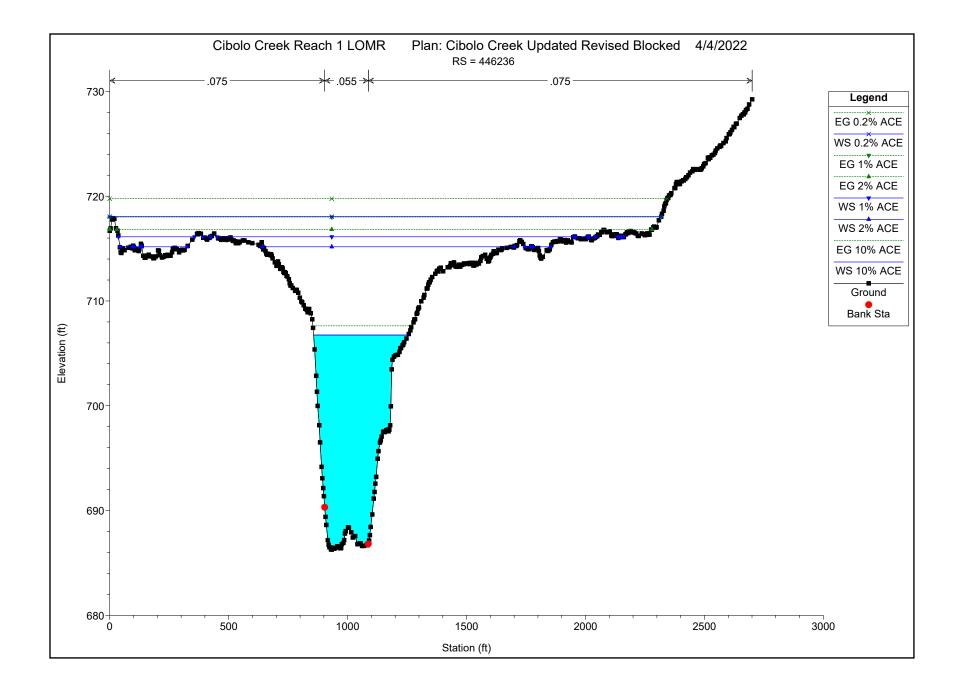
| ZONE X 98 '95 '00.00' 29 '33 '5.00' Dietz Creek G9t AN XONE AE Creek G9t TONE AE Creek G9t TONE AE Creek G9t TONE AE TONE | <text><text><text><text><text><text><text><text><text><text><text><text><text><text></text></text></text></text></text></text></text></text></text></text></text></text></text></text> | | |
|--|---|---|--|
| ACCENTINE ACCENTINA ACCENTINA ACCENTINA ACCENTINA ACCENTINA ACCENTINA ACCENT | ZONE VE Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined. Image: Coastal Problem in the stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights. Image: Coastal Problem in the stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights. Image: Coastal Problem in the stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights. Image: Coastal Problem in the stream plus any adjacent floodplain. ZONE X Areas determined to be outside the 0.2% annual chance floodplain. ZONE D Areas in which flood hazards are undetermined, but possible. Image: Coastal Barrier RESOURCES SYSTEM (CBRS) AREAS Image: Coastal Barrier RESOURCES SYSTEM (CBRS) AREAS Image: Coastal Barrier RESOURCES SYSTEM (CBRS) AREAS Image: Coastal Barrier RESOURCES System flood Hazard Areas. Image: Floodplain boundary Image: Coastal Boundary Image: Coastal Boundary Image: Coastal Barrier Resource flood Hazard Areas of different Base Flood Elevation line and value; elevation in feet* (EL 987) Base Flood Elevation value where uniform within zone; elevation in feet* | Image: Additional and the second structure Molecan base Molecan base Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the second structure Image: Additional and the sec | Ph: 512.439.0400 · Fax: 512.329.0096 www.cecinc.com |
| JOINS PANEL 0240 | 97'0730', 32*22'30'' Geographic coordinates referenced to the North American Datum of 1983 (NAD 83) 4275'000mN 1000-meter Universal Transverse Mercator grid ticks, zone 14 6000000 FT 5000-foot grid values: Texas State Plane coordinate system, south central zone (FIPSZONE 4204), Lambert Conformal Conic DX5510 Bench mark (see explanation in Notes to Users section of this FIRM panel) MAP REPOSITORIES M1.5 River Mile MAP REPOSITORIES Refer to Map Repositories list on Map Index EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP November 2, 2007 EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL | BECK LANDFILL EXPANSION 600 FM 78, SCHERTZ, TEXAS 78154 GUADALUPE COUNTY, TEXAS | |
| | | | 311-653.SITE AWM |
| | | FLOOD INSURANC FIRM) 48187C0220F 5/2/2022 DRAWN BY: 1" = 1000' | |
| 3 | SCALE IN FEET 0 1000 2000 2 | DRAWING NO.: BHEET 3 OF 4 | PROJECT NO: APPROVED BY: |

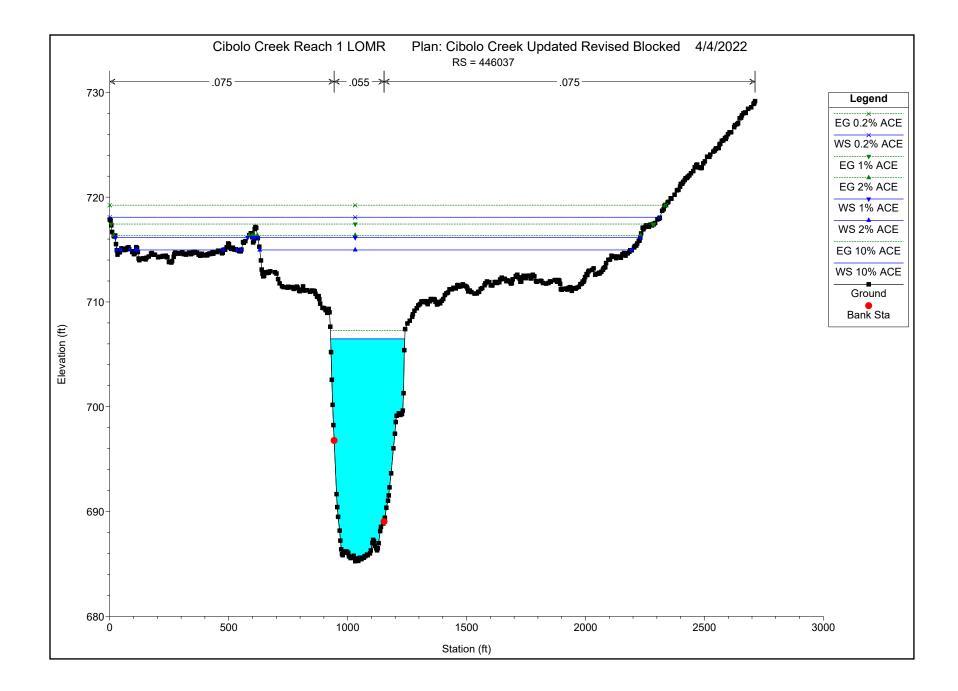


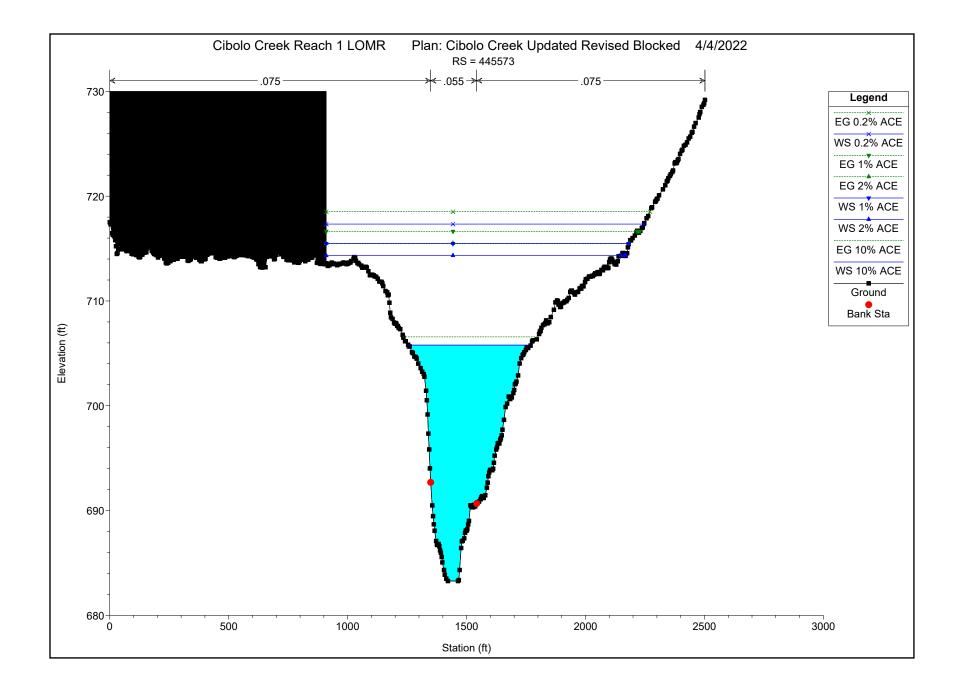
| | <text><image/><image/><section-header> For the set of the set of</section-header></text> | REVISION RECORD | DATE DESCRIPTION | | | | | |
|--|---|-----------------|--|--|---------------------------------|-------------------------------|--------------------------------------|------------------|
| Bexar County Unincorporated Art 480035 | encroachment so that the 1% annual chance flood can be carried without substantial increases in flood heights. Image: Constraint of the stress of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage preas less than 1 square mile; and areas protected by levees from 1% annual chance flood. ZONE X Areas of 0.2% annual chance flood based on future conditions hydrology. No (Future Base Flood) Base Flood Elevations determined. Image: Constraint of the stress of 1% annual chance flood plain. OTHER AREAS ZONE X Areas determined to be outside the 0.2% annual chance floodplain. ZONE D Areas determined to be outside the 0.2% annual chance floodplain. ZONE D Areas determined to be outside the 0.2% annual chance floodplain. ZONE D Areas in which flood hazards are undetermined, but possible. Image: Constraint Barrier RESOURCES SYSTEM (CBRS) AREAS COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS Image: Constraint Barrier RESOURCES SYSTEM (CBRS) AREAS Floodplain Boundary Image: Constraint Barrier RESOURCES SYSTEM (CBRS) AREAS Floodplain Boundary Image: Constraint Barrier RESOURCES System (CBRS) areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas. Floodplain Boundary Image: Constraint Barrier RESOURCES System Resource RESOURCES. Special Flood Elevation in feet* Image: Cond Elevation Special Flood Hazard Areas of | | | Texas Registered Engineering Firm F-38 | iror | pressway · Building 1, S | Ph: 512.439.0400 · Fax: 512.329.0096 | www.cecilic.coll |
| | **99000n N 1000-meter Universal Transverse Mercator grid values, Zone 14 DX5510 X Bench mark (see explanation in Notes to Users section of this FIRM pane) * M1.5 River Mie MAP REPOSITORIES ON MAP INDEX CFECTIVE DATE OF COUNTYWIDE TOOD INSURANCE RATE MAP DEDUCTIVE DATE OF COUNTYWIDE TOOD INSURANCE RATE MAP FEBRUARY 18, 1996 EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL September 29, 2010- to change the Base Flood Elevations, Special Flood Hazard Areas, roads and road names; to reflect updated topographic information; to incorporate previously issued Letters of Map Revision and to update corporate limits. | | | BECK LANDFILL EXPANSION | 600 FM 78, SCHERTZ, TEXAS 78154 | GUADALUPE COUNTY, TEXAS | | |
| | | L | | <u> </u> | АGТ | JCM | 311-653.SITE | AWM |
| | | | ANNULATED FLOUD INSURANU MAP (FIRM) 48029C0295F | | 4/29/2022 DRAWN BY: | 1" = 1000' CHECKED BY: | | |
| | SCALE IN FEET 0 1000 2000 2 | | WING | NO.: 4 | DATE: | DWG SCALE: | | |

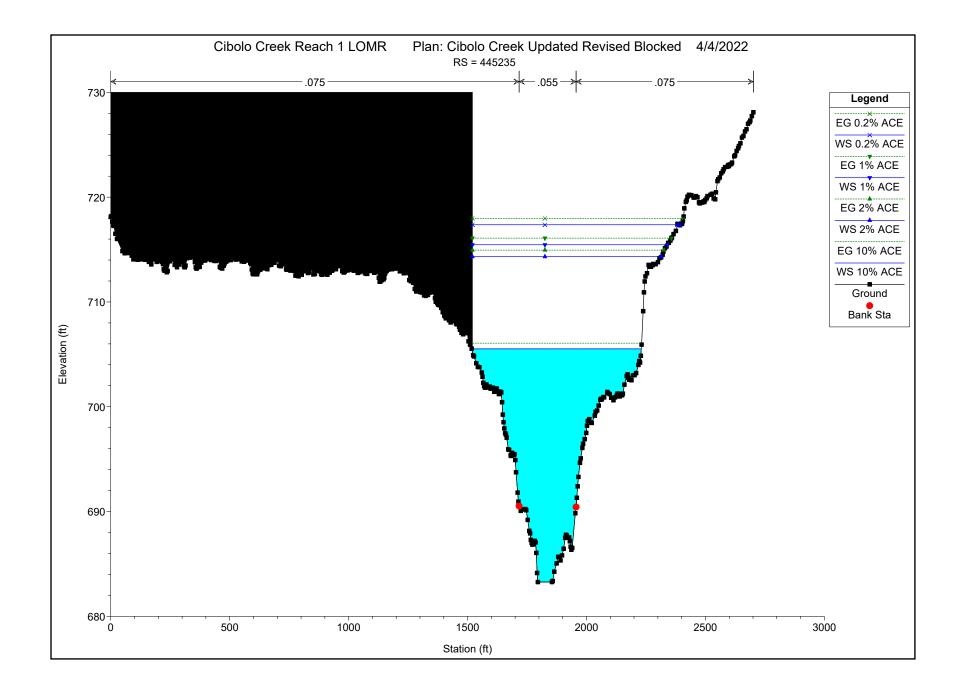
HEC-RAS HYDRAULIC RESULTS

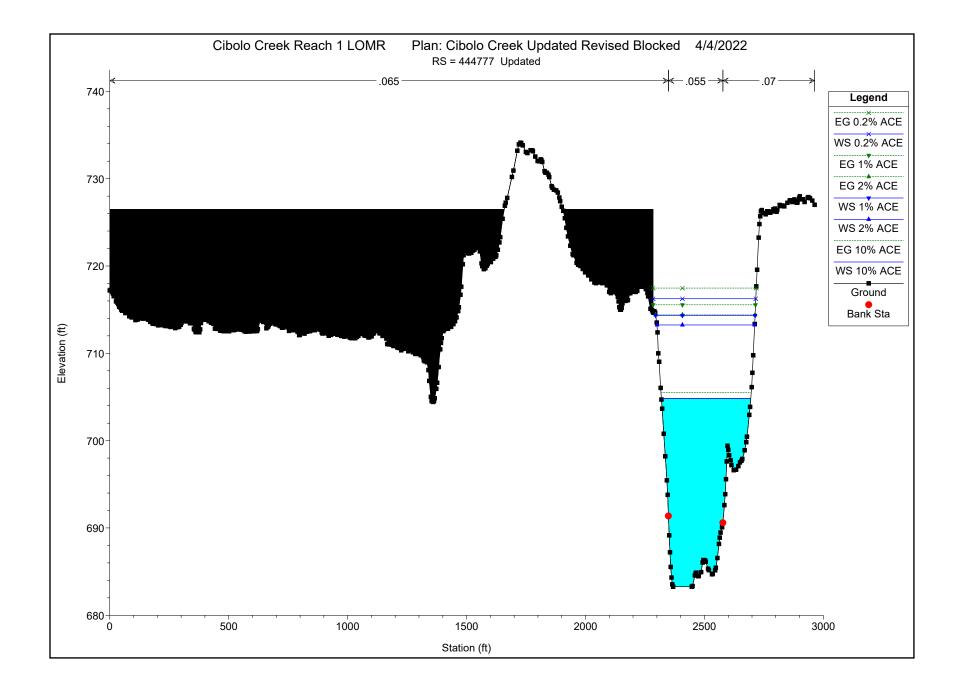
| | HEC- | RAS Plar | 1: Update | d Revised | Blocked | River: C | ibolo Cree | ek Reach | : Reach 1 | l Profile | : 1% ACE | |
|---------|-----------|----------|-----------|-----------|-----------|-----------|------------|------------|-----------|-----------|-----------|--------------|
| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Reach 1 | 446236 | 1% ACE | 83554.00 | 686.27 | 716.12 | | 718.00 | 0.002356 | 12.35 | 12083.89 | 1951.03 | 0.40 |
| Reach 1 | 446037 | 1% ACE | 83554.00 | 685.26 | 716.14 | | 717.43 | 0.001662 | 10.38 | 14568.45 | 2171.55 | 0.34 |
| Reach 1 | 445573 | 1% ACE | 83554.00 | 683.27 | 715.47 | | 716.64 | 0.001635 | 10.24 | 13853.91 | 1272.36 | 0.34 |
| Reach 1 | 445235 | 1% ACE | 74844.00 | 683.27 | 715.46 | | 716.09 | 0.000839 | 7.38 | 14446.55 | 819.21 | 0.24 |
| Reach 1 | 444777 | 1% ACE | 74844.00 | 683.27 | 714.34 | | 715.55 | 0.001357 | 9.41 | 9324.66 | 418.29 | 0.31 |
| Reach 1 | 444240 | 1% ACE | 74844.00 | 683.14 | 712.59 | | 714.56 | 0.002177 | 11.70 | 7112.57 | 303.76 | 0.39 |
| Reach 1 | 443555 | 1% ACE | 74844.00 | 682.52 | 712.24 | | 713.19 | 0.001159 | 8.05 | 9943.71 | 424.81 | 0.28 |
| Reach 1 | 442891 | 1% ACE | 74844.00 | 679.79 | 711.58 | | 712.49 | 0.000944 | 7.77 | 10195.40 | 409.13 | 0.25 |
| Reach 1 | 442214 | 1% ACE | 74844.00 | 678.90 | 709.72 | | 711.43 | 0.002485 | 12.16 | 8711.94 | 548.33 | 0.40 |
| Reach 1 | 441476 | 1% ACE | 74844.00 | 678.52 | 708.12 | | 709.76 | 0.001991 | 10.59 | 7947.43 | 421.93 | 0.36 |
| Reach 1 | 440762 | 1% ACE | 74844.00 | 677.76 | 705.81 | | 707.89 | 0.002707 | 11.80 | 6709.83 | 304.53 | 0.42 |
| Reach 1 | 439971 | 1% ACE | 74844.00 | 677.96 | 705.51 | | 705.71 | 0.000410 | 4.27 | 22216.60 | 1144.96 | 0.16 |
| Reach 1 | 438740 | 1% ACE | 74844.00 | 675.84 | 705.30 | | 705.41 | 0.000223 | 3.38 | 33040.49 | 1844.11 | 0.12 |
| Reach 1 | 437996 | 1% ACE | 74844.00 | 674.71 | 705.21 | | 705.29 | 0.000189 | 3,18 | 35176.72 | 1824.69 | 0.11 |
| Reach 1 | 437265 | 1% ACE | 74844.00 | 674.32 | 705.03 | | 705.18 | 0.000290 | 3.98 | 27754.92 | 1486.97 | 0.14 |
| Reach 1 | 436536 | 1% ACE | 74844.00 | 673.98 | 704.27 | | 704.82 | 0.000810 | 6.89 | 15281.89 | 921.79 | 0.23 |
| Reach 1 | 435810 | 1% ACE | 74844.00 | 672.59 | 703.05 | | 703.98 | 0.001244 | 8.45 | 10535.21 | 526.54 | 0.29 |
| Reach 1 | 435043 | 1% ACE | 74844.00 | 672.92 | 702.40 | | 703.12 | 0.000674 | 7.03 | 11817.77 | 513.44 | 0.24 |
| Reach 1 | 434453 | 1% ACE | 74844.00 | 672.90 | 701.08 | | 702.28 | 0.001688 | 9.93 | 10304.78 | 657.11 | 0.34 |
| Reach 1 | 433730 | 1% ACE | 74844.00 | 668.74 | 700.47 | | 701.07 | 0.001006 | 7.16 | 14270.50 | 937.56 | 0.24 |
| Reach 1 | 433539 | 1% ACE | 74844.00 | 667.11 | 700.39 | | 700.85 | 0.000790 | 6.40 | 16157.71 | 1041.30 | 0.21 |
| Reach 1 | 433408 | 1% ACE | 74844.00 | 667.31 | 700.34 | | 700.73 | 0.000749 | 6.22 | 17384.43 | 1111.20 | 0.21 |
| Reach 1 | 433181 | 1% ACE | 86791.00 | 667.56 | 700.20 | | 700.53 | 0.000716 | 5.98 | 23132.56 | 1884.55 | |

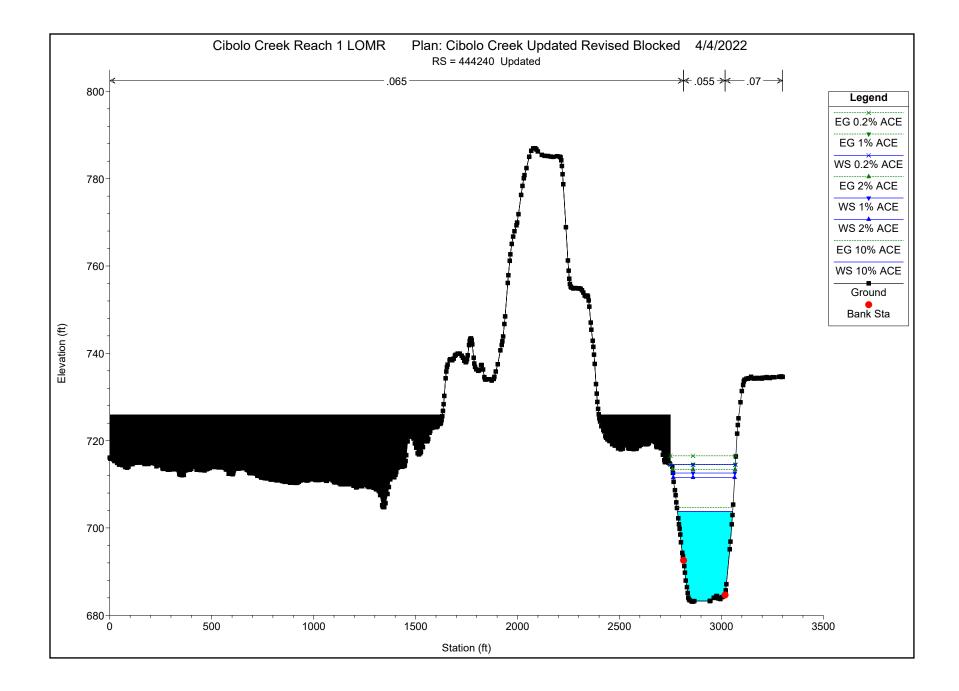


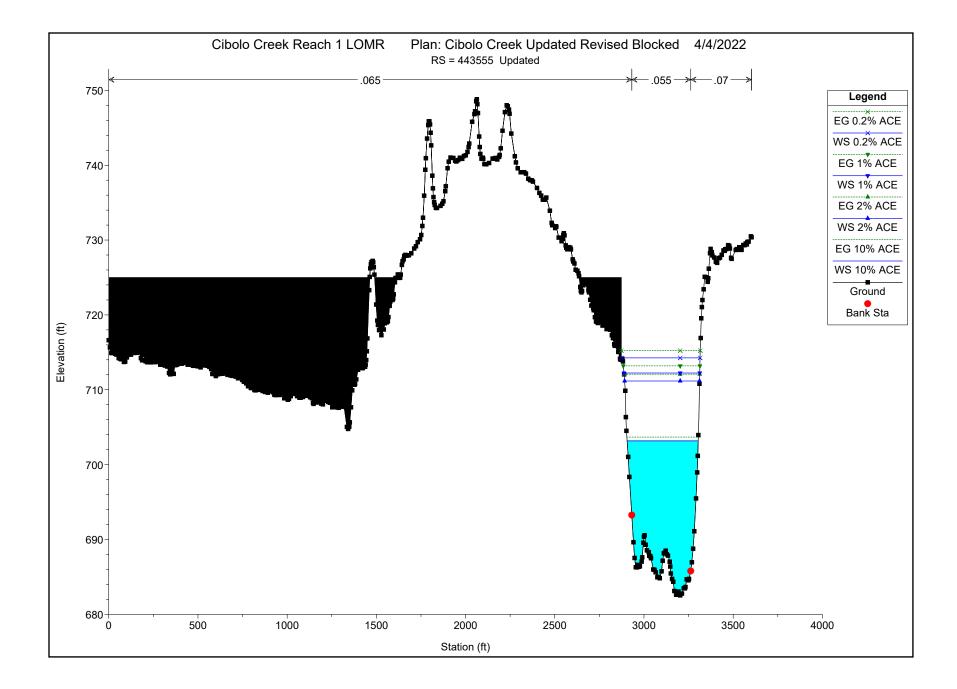


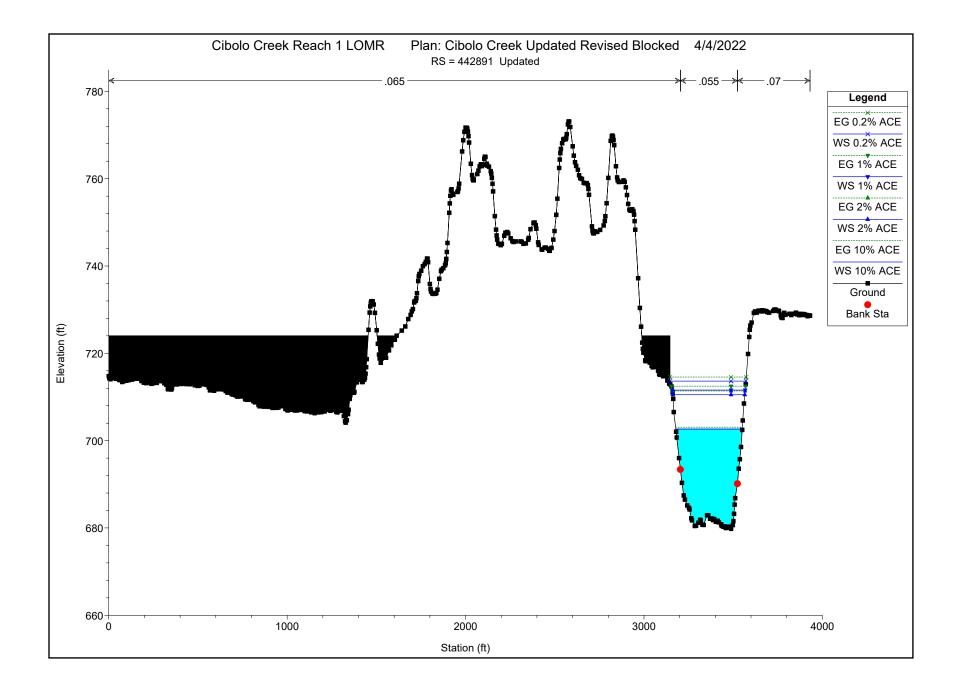


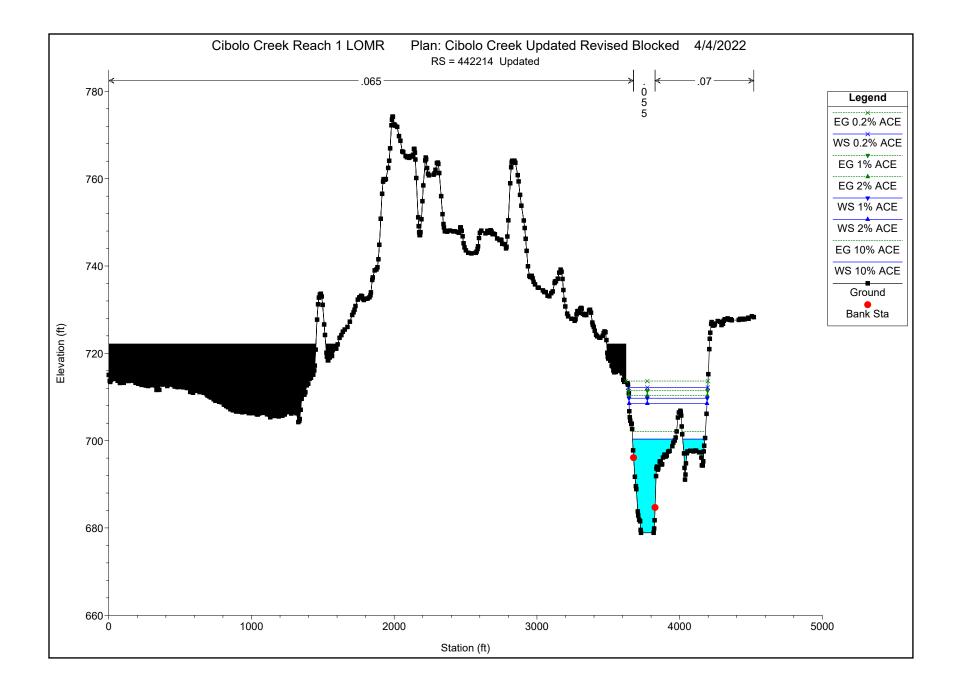


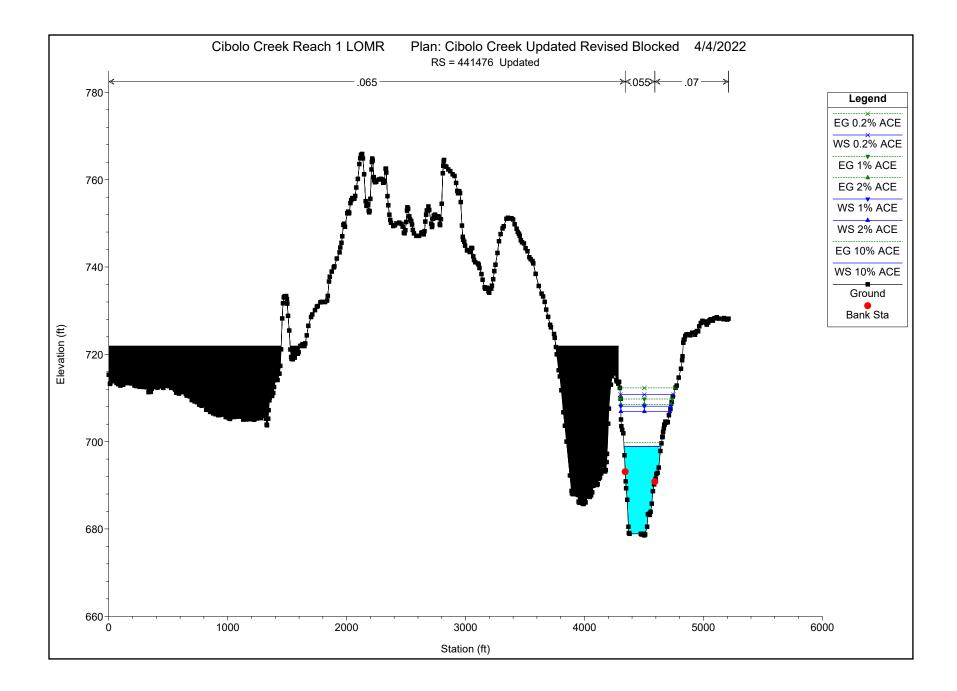


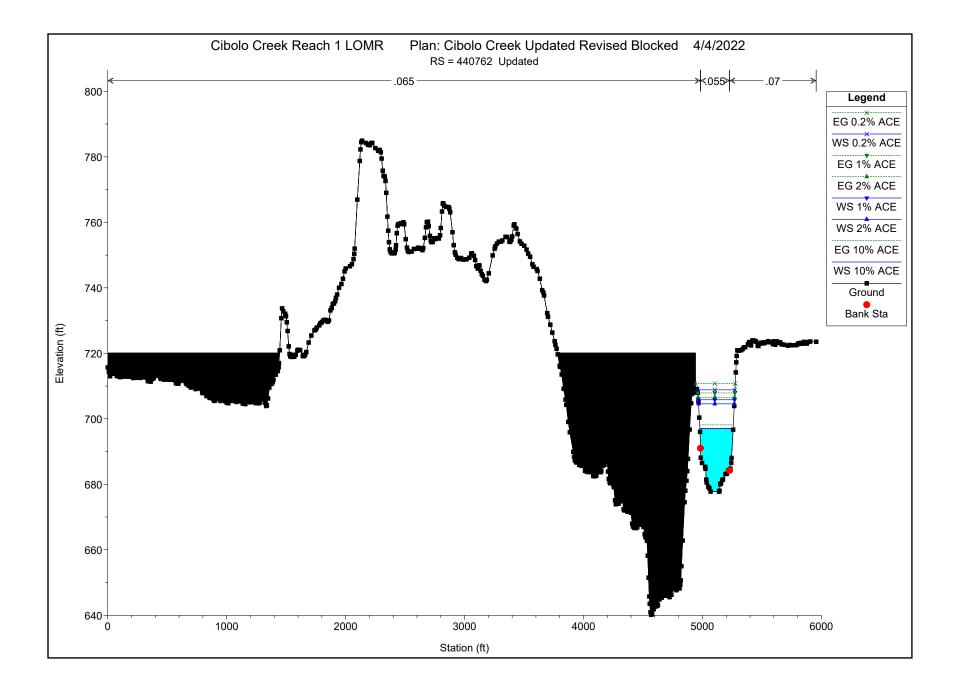


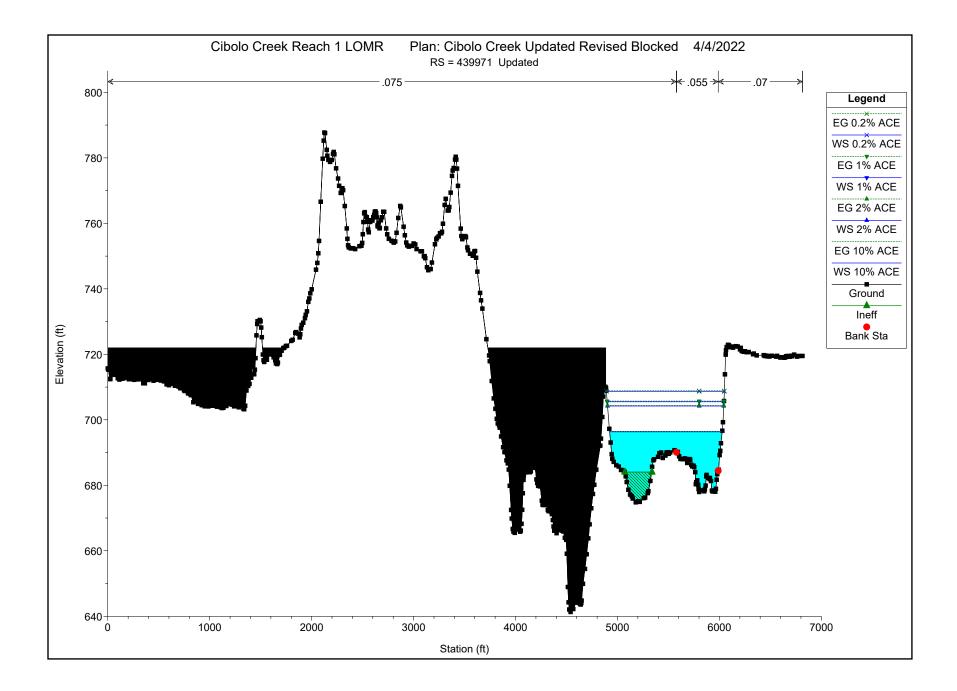


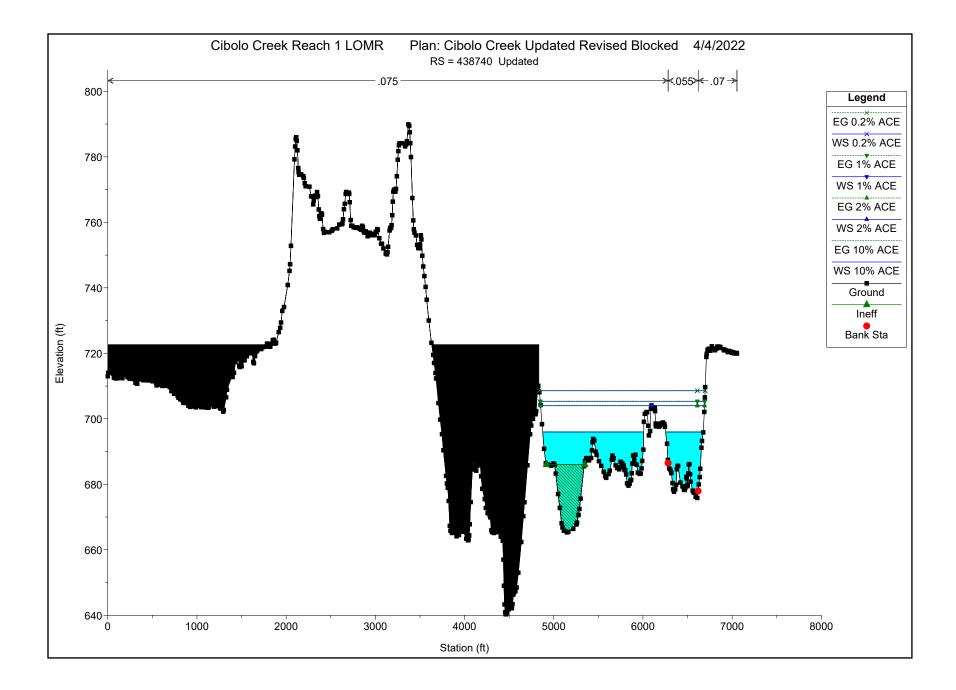


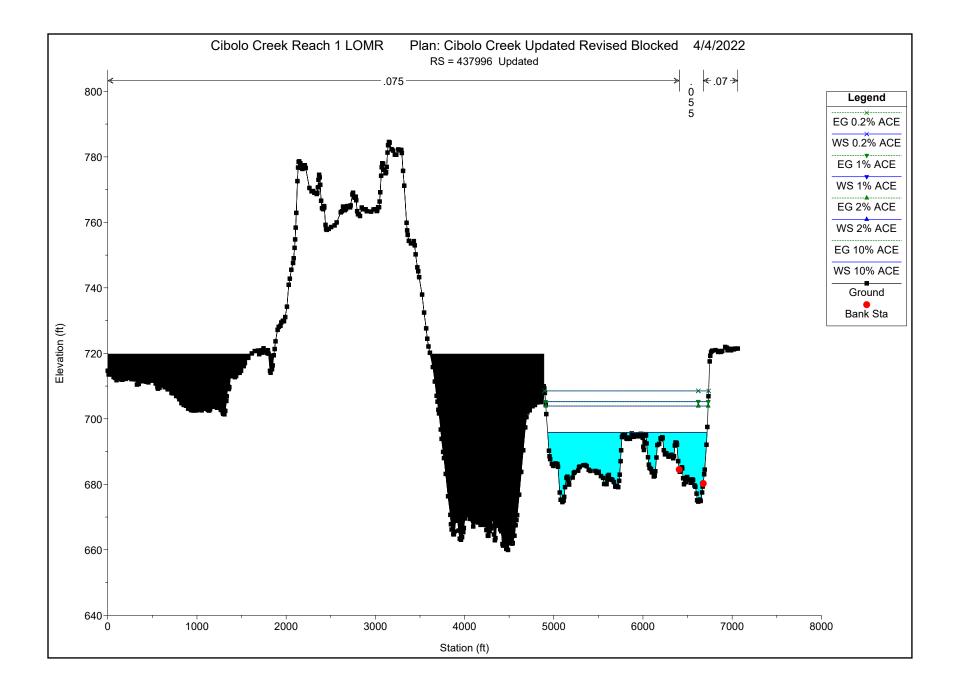


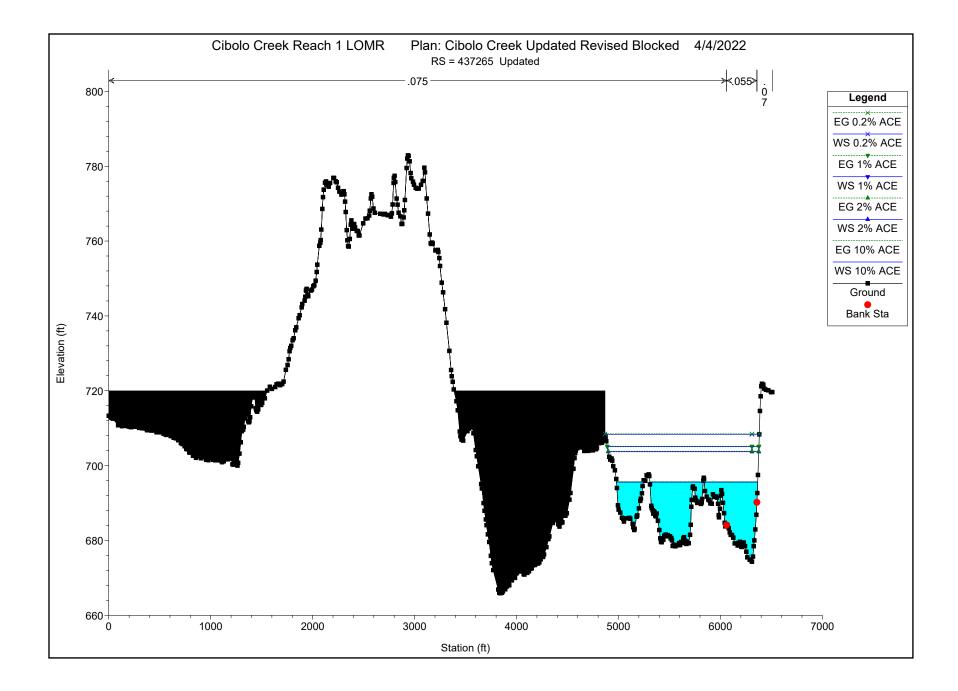


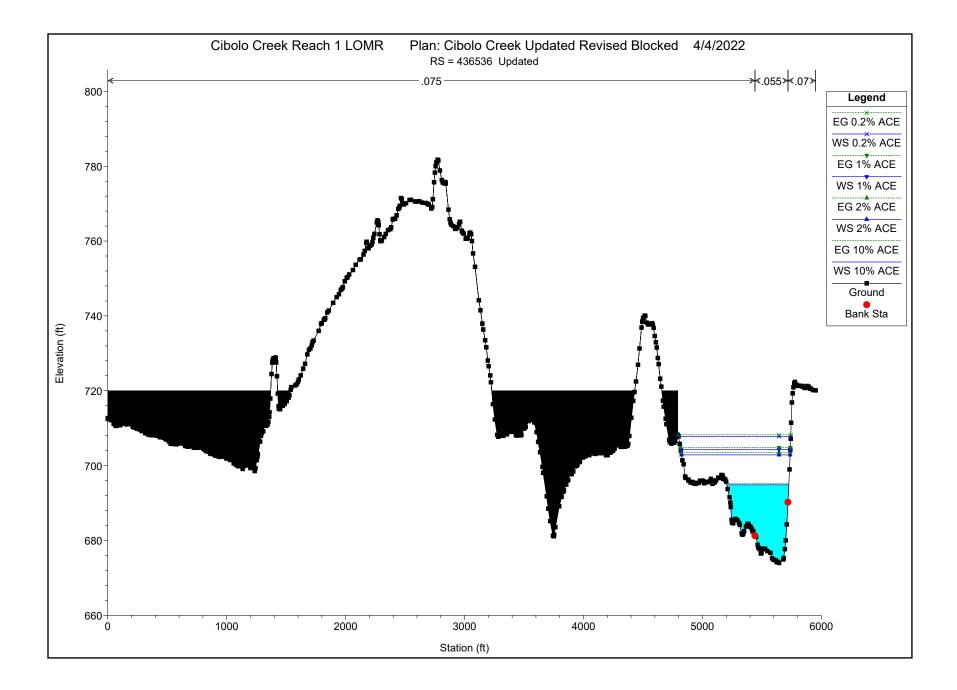


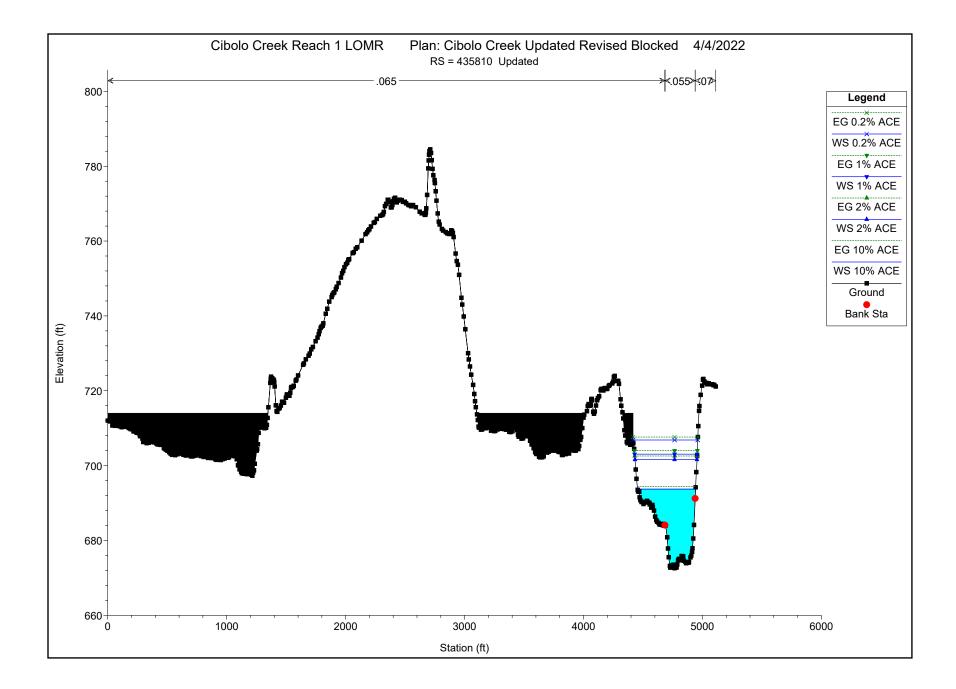


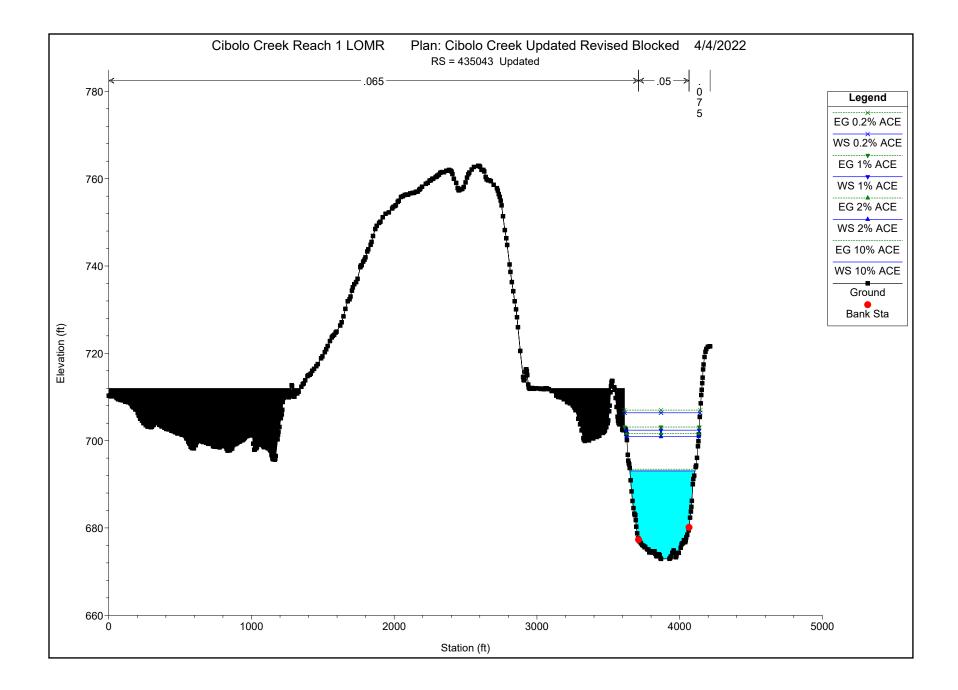


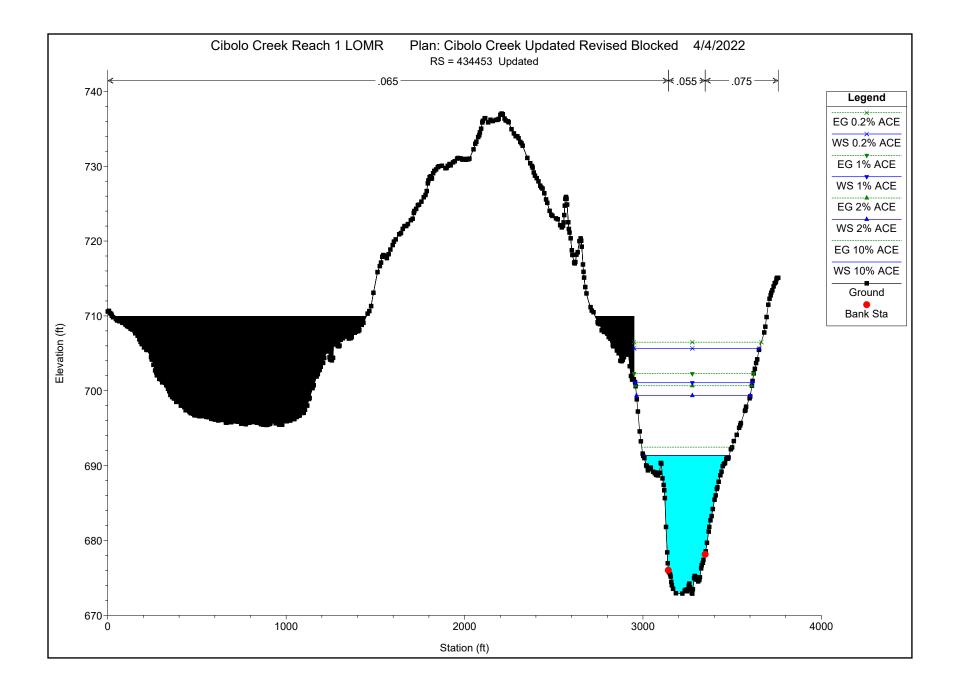


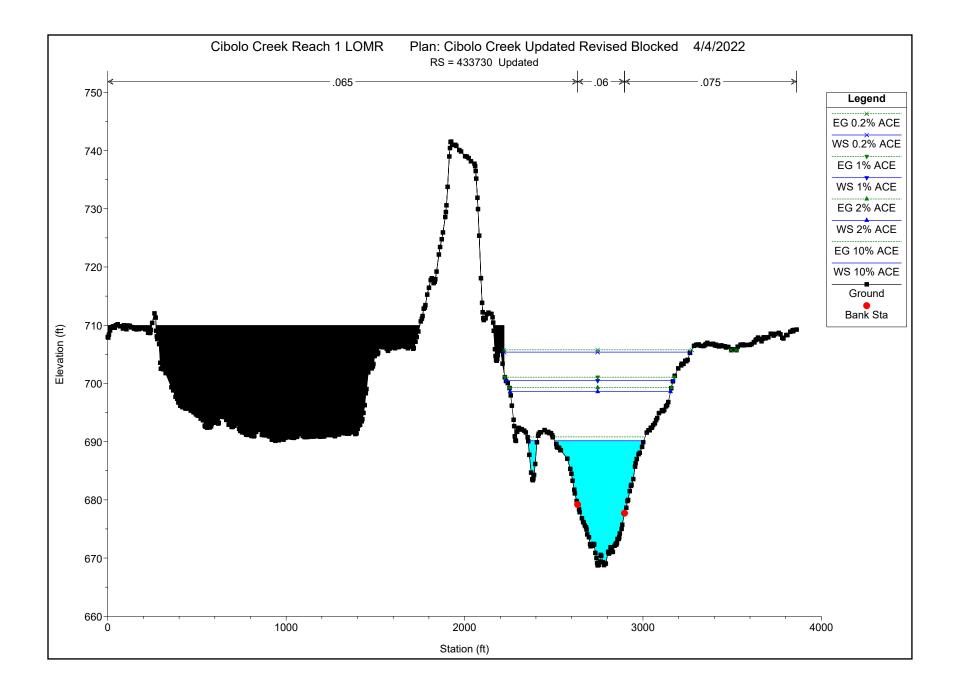


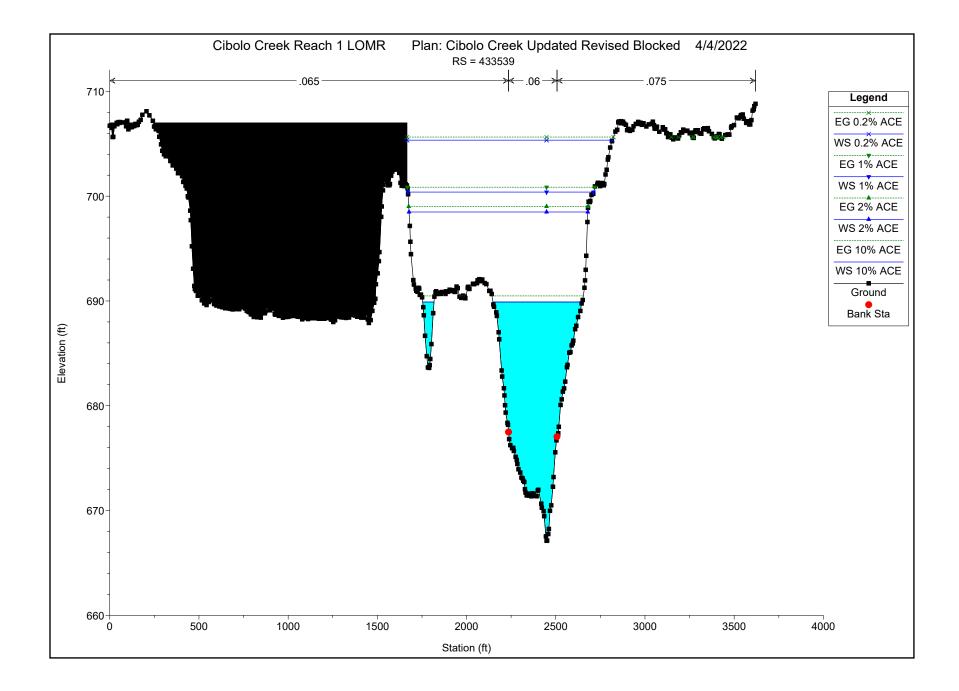


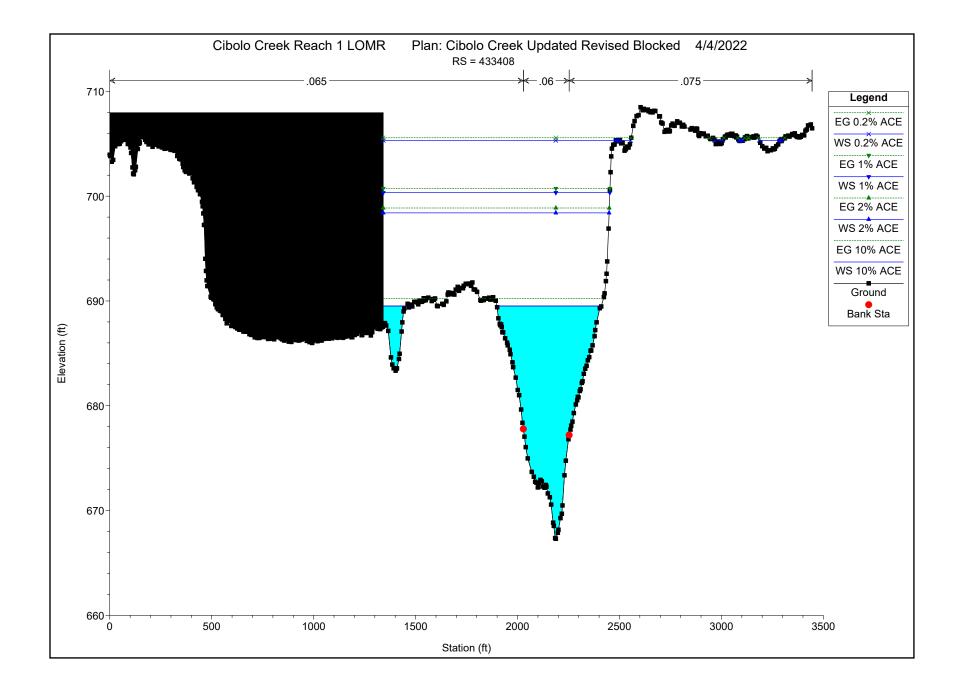


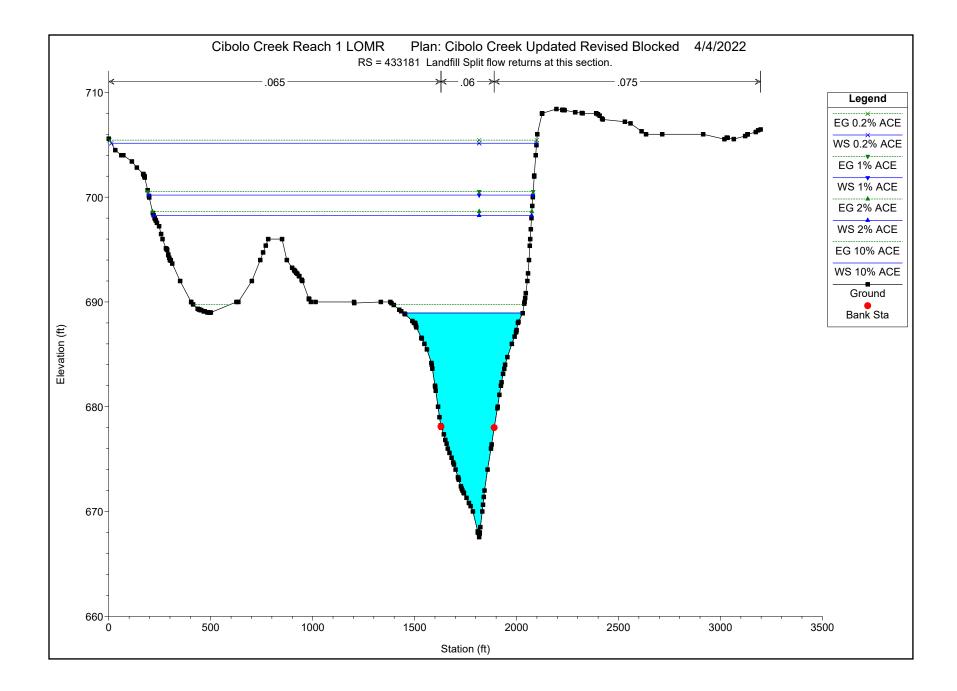












BECK LANDFILL APPENDIX C2-B No-Rise Certification for Proposed Stormwater Pond

City of Schertz

Floodplain Permit Permit PRGR202202064

Date Issued: October 20, 2022 Project Address: 550 FM 78; Expires: April 18, 2023

Subdivision:

Lot # Block #

Owner Information:

Contractor:

Proposed Use: Not Applicable

Description of Work:

- Floodplain:
- Clearing and Grading: Disturbing Soil (Greater than 1/10th of an Acre) Note: Permit is for construction of new detention basin for landfill.
- **Conditions:**

Issued By: Engineering Department

Kathig & Woodlee

Kathy Woodlee City Engineer (210) 619-1823

Permits are non-transferable and shall be displayed on site at all times.



NO RISE CERTIFICATION

PROPOSED STORMWATER POND



NAME OF PROJECT: Beck Landfill Stormwater Pond

OWNER: Nido, LTD

CITY, COUNTY: Schertz, Guadalupe County

August 15, 2022

Prepared by:



Civil & Environmental Consultants, Inc.

Texas Registration Number F-38 3711 S MoPac Expressway Building 1 Suite 550, Austin, Texas 78746 (512) 329-0006



EXECUTIVE SUMMARY

The Beck Landfill proposes to construct a new Stormwater Pond (Pond) located in the Cibolo Creek watershed southeast of the existing landfill (see Figure 1). The Pond will be excavated below grade and include above grade compacted soil berms to provide additional volume. The purpose of the pond is to provide detention and sedimentation capacity for the existing landfill. The pond will be constructed at the same location as the existing stormwater pond and the proposed soil berms will be tied into the existing landfill perimeter berm to minimize the encroachment on the floodplain. In order to offset the loss of flow area in the floodplain from the pond berm, the area south of the new pond is proposed to be excavated to enhance flow through Cibolo Creek. There is no increase in the calculated water surface elevation of the floodplain from the pond construction, since the areas along the creek will be excavated to completely offset any effects of the new pond. This report provides engineering support for a No Rise Certificate for the pond construction.

FEMA FLOODPLAIN

The proposed Pond site is located within the floodway of Cibolo Creek (see Figure 2). Given the location, under City of Schertz regulations there is to be no rise in the 1-percent annual exceedance probability (AEP) event water surface elevations associated with the installation of the facility.

HYDRAULIC MODELING

To evaluate the potential impact, the effective FEMA model for this reach of Cibolo Creek was utilized. The effective model was obtained from the San Antonio River Authority. FIRMATEK 3D Mapping Solutions (FIRMATEK) performed an aerial survey of the Beck Landfill site which included the Cibolo Creek channel around the facility in 2021. The effective model geometry (Cibolo Creek Reach 1) was updated around the landfill to reflect the latest topography (CiboloCkR1LOMR) and this model was utilized in the recently submitted LOMR application to the City of Schertz and FEMA.

A digital elevation model (DEM) was developed for the vicinity of the landfill to create the above noted Cibolo Creek Reach 1 LOMR geometry. The base topography for the area around the landfill was derived from the FEMA 2011 61 cm Comal, Guadalupe LiDAR dataset. For the area in and

around the landfill, the FIRMATEK dataset was utilized. Lastly, a third geometry (CiboloCreek-South) was developed for the site. It used the Cibolo Creek Reach 1 LOMR geometry DEM and a DEM that includes the proposed Pond contours.

Figure 3 shows the proposed pond and the cross-section locations from the models. Note that four cross sections (439971, 438740, 437996, and 437265) pass through the proposed Pond. Plots of the four cross sections comparing the elevations with and without the proposed Pond are found in Appendix A. The cross sections for both the LOMR configuration and the LOMR configuration with the Pond added, were evaluated using HEC-RAS 6.1. It is my opinion that the analyzed cross sections reasonably reflect the impact of the proposed Pond without needing supplemental cross sections. The flow values used in this evaluation are the same as the discharges from the effective model.

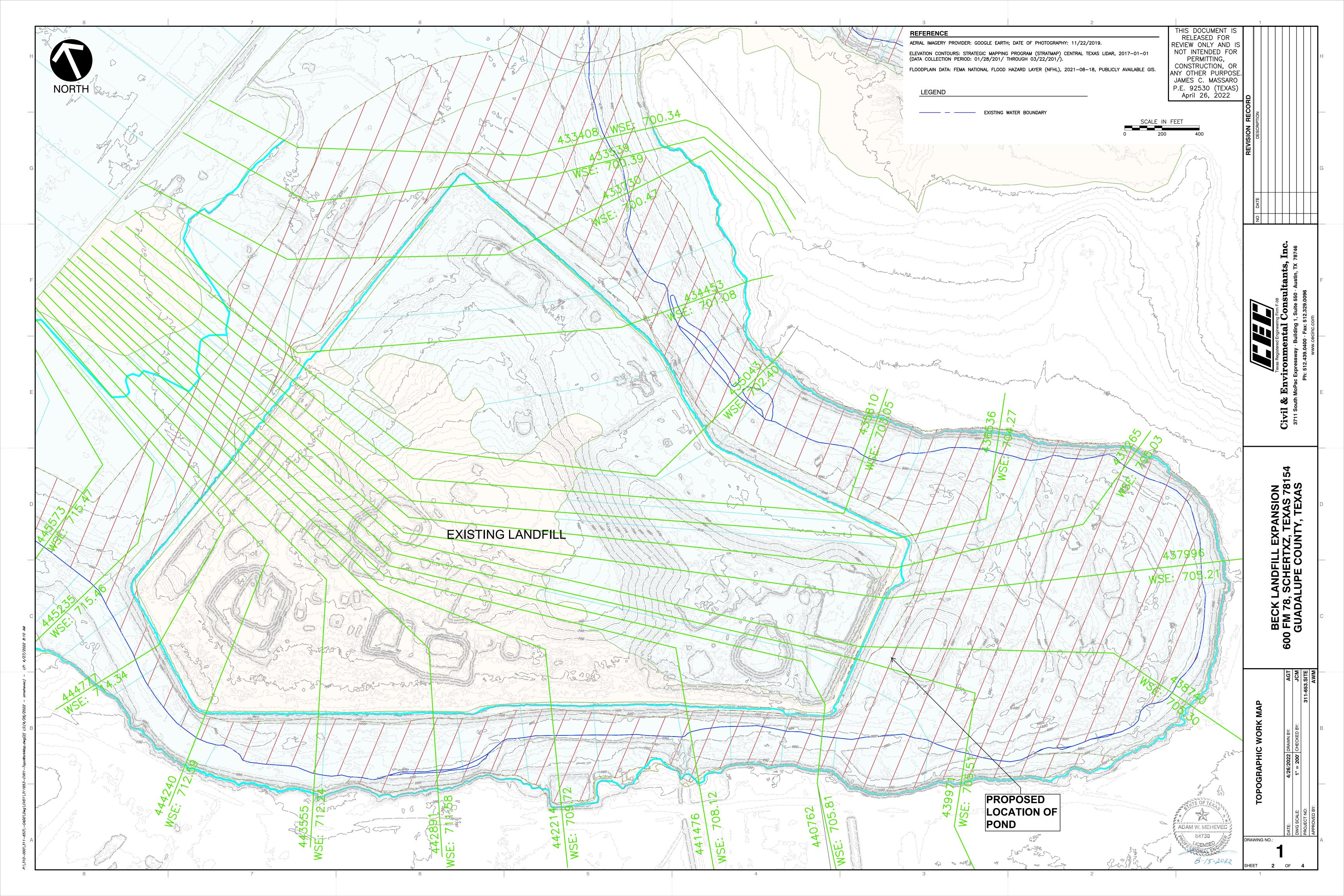
RESULTS

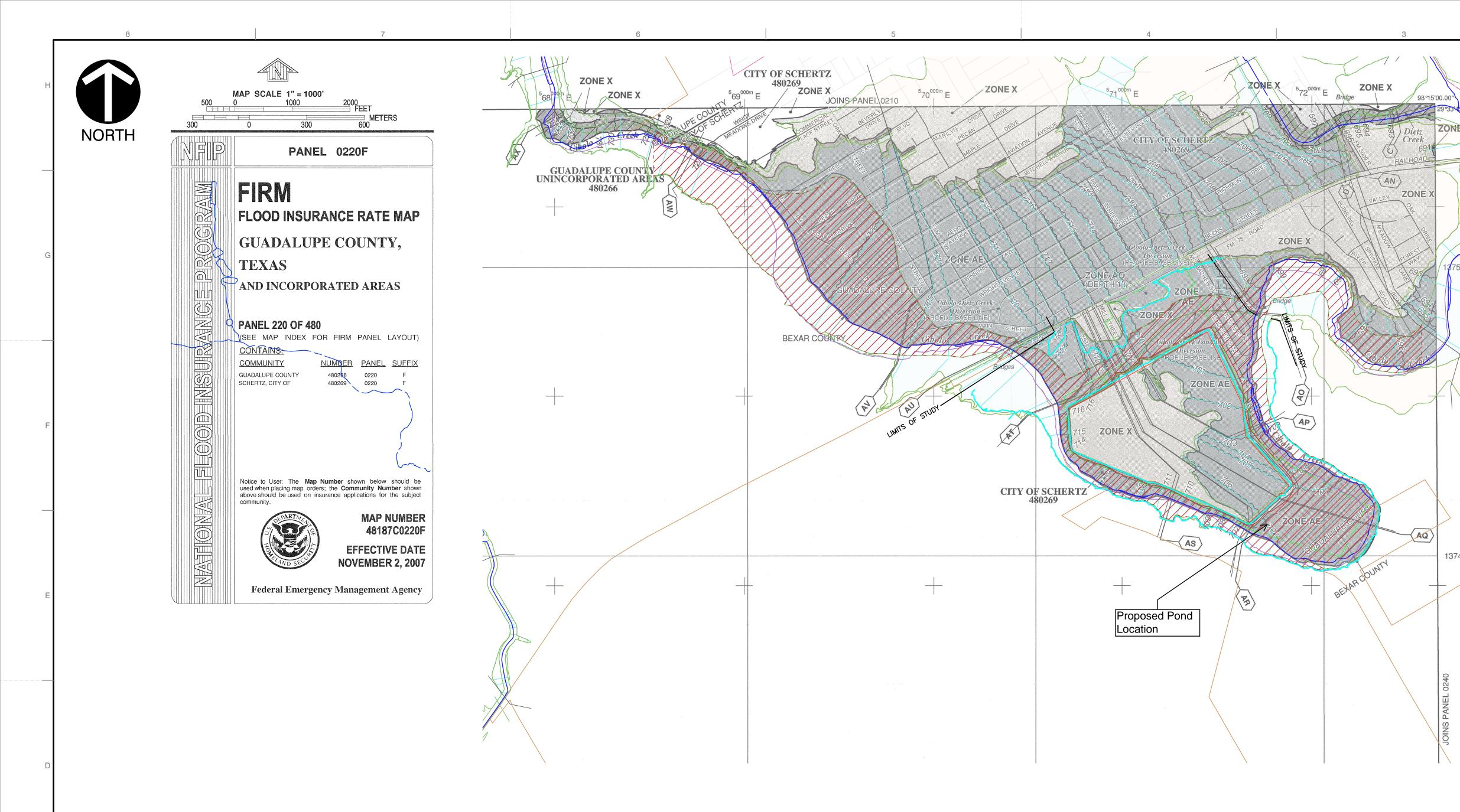
Both geometries (Cibolo Creek Reach 1 LOMR and Cibolo Creek-South) were run using the same inflow dataset. HEC-RAS output summary tables with the cross-sections effected by the Pond highlighted, are included in Appendix A. A summary of the results for the two models is also shown below in Table 1.

| Cross-Section | LOMR 1% Chance | Proposed Pond 1% Chance | Difference in Water |
|---------------|--------------------------|--------------------------|--------------------------|
| Label | Water Surface (Feet MSL) | Water Surface (Feet MSL) | Surface Elevation (Feet) |
| 439971 | 705.51 | 705.33 | -0.18 |
| 438740 | 705.30 | 705.21 | -0.09 |
| 437996 | 705.21 | 705.13 | -0.08 |
| 437265 | 705.03 | 705.03 | 0.00 |

 Table 1-Comparison of Water Surface Elevations

The proposed excavation more than offsets the proposed pond berm and all of the modeled crosssections either shown no change between the two models or show a slight reduction in water surface for the model including the Pond. Based on the results of the modeling, a No Rise Certificate is warranted for the proposed Pond.





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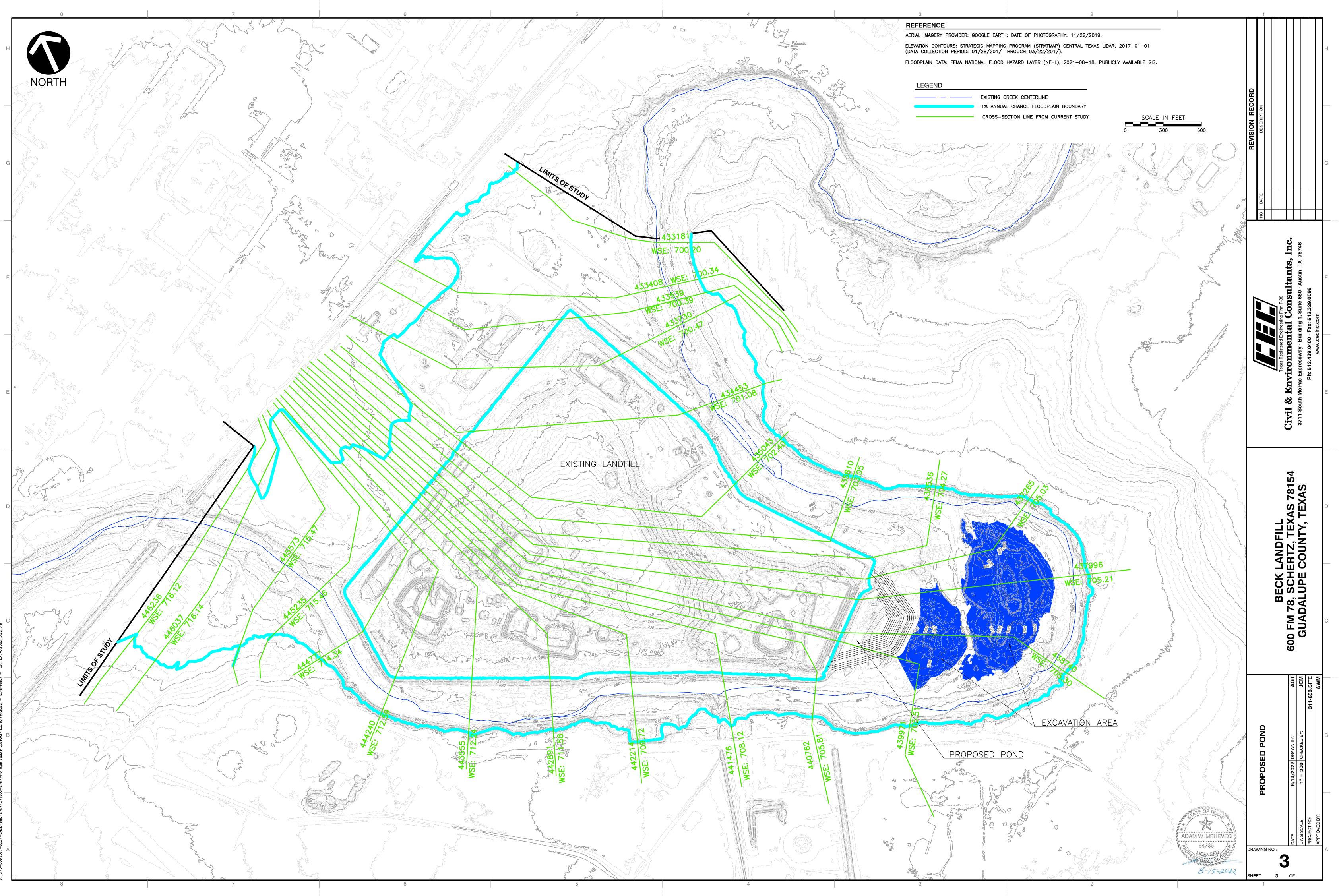
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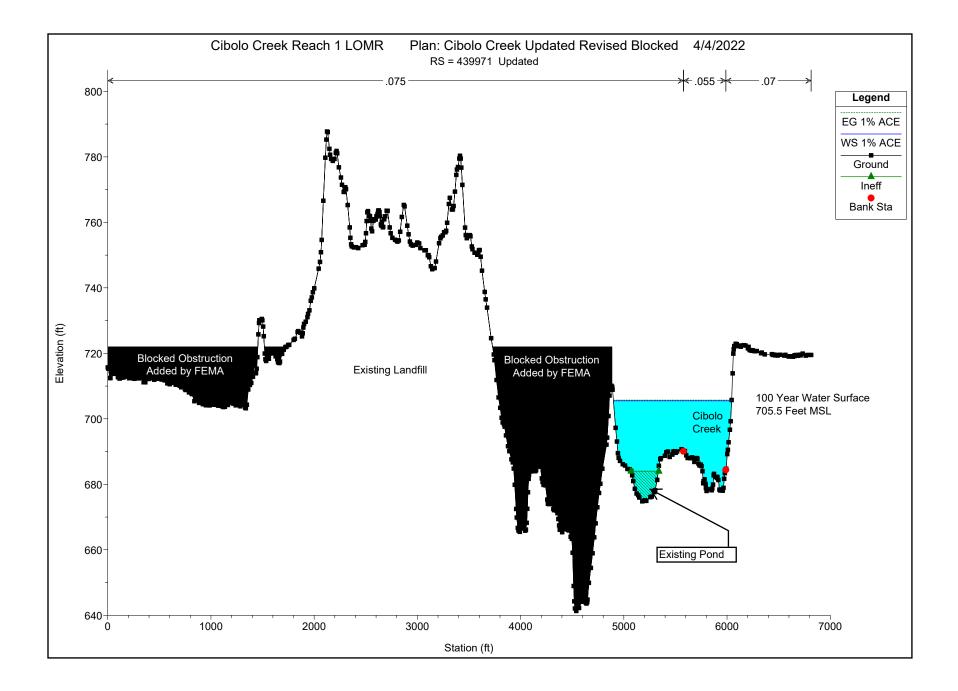
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| | | RATE AGT JCM St11-653.SITE AWM | | | |
| | | FLOOD INSURANCE FIRM) 48187C0220F 5/2/2022 DRAWN BY: 1" = 1000' CHECKED BY: 3 | | | |
| 3 | SCALE IN FEET 0 1000 2000 2 | DRAWING NO.: BHEET 3 OF 4 | | | |

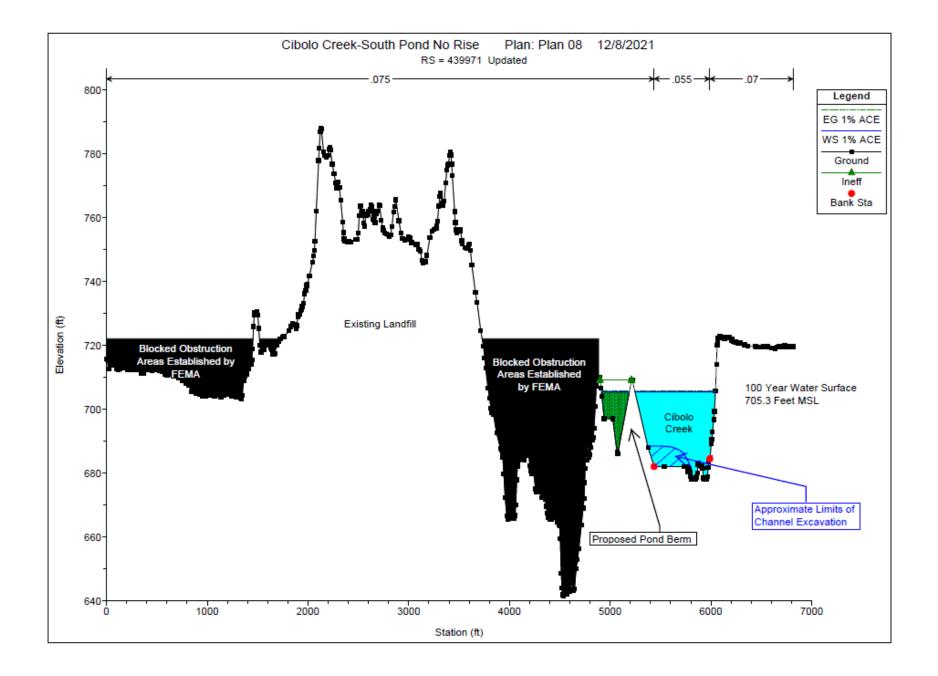


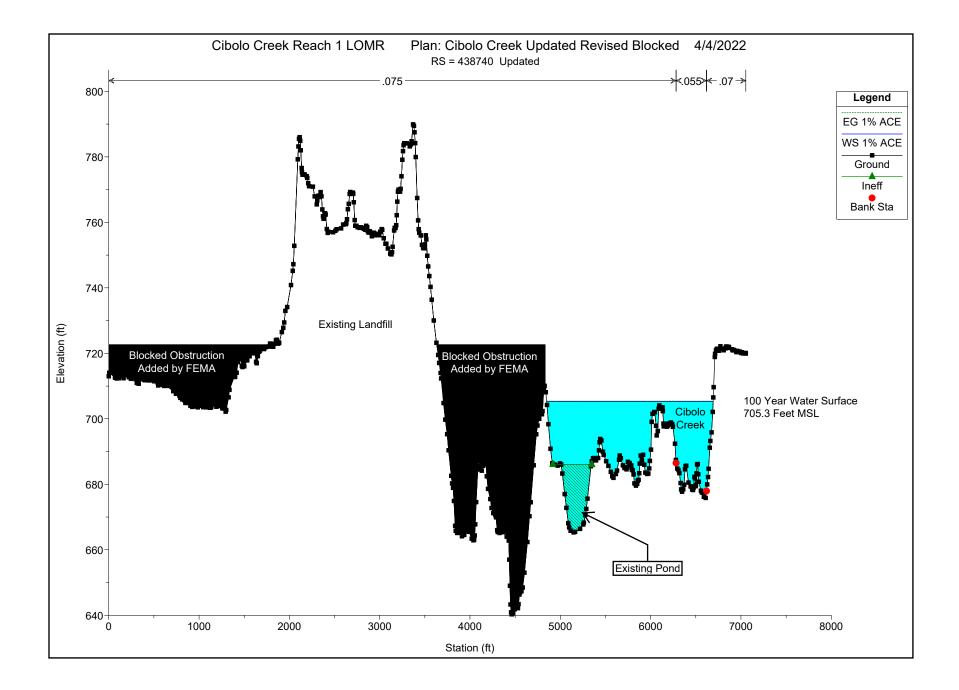
.000\311-653\-C4DD\Dwg\CV01\311653-CV01-No Rise Figure 3.dwg{2} LS:(8/14/2022 - amehevec) - LP: 8/14/

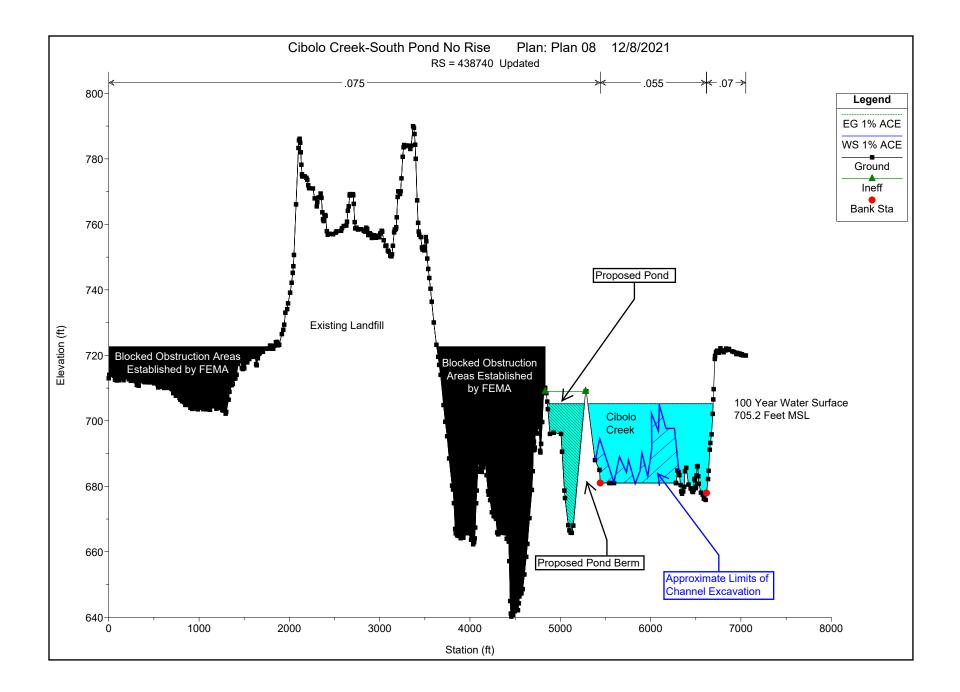
Appendix A

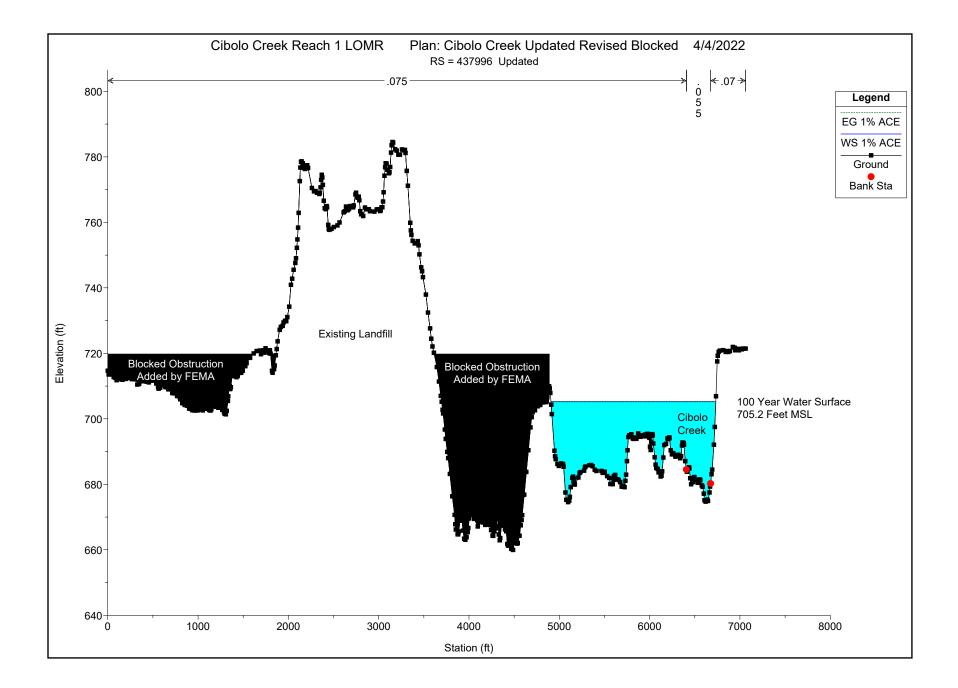
HEC-RAS Cross-Sections and Summary Tables

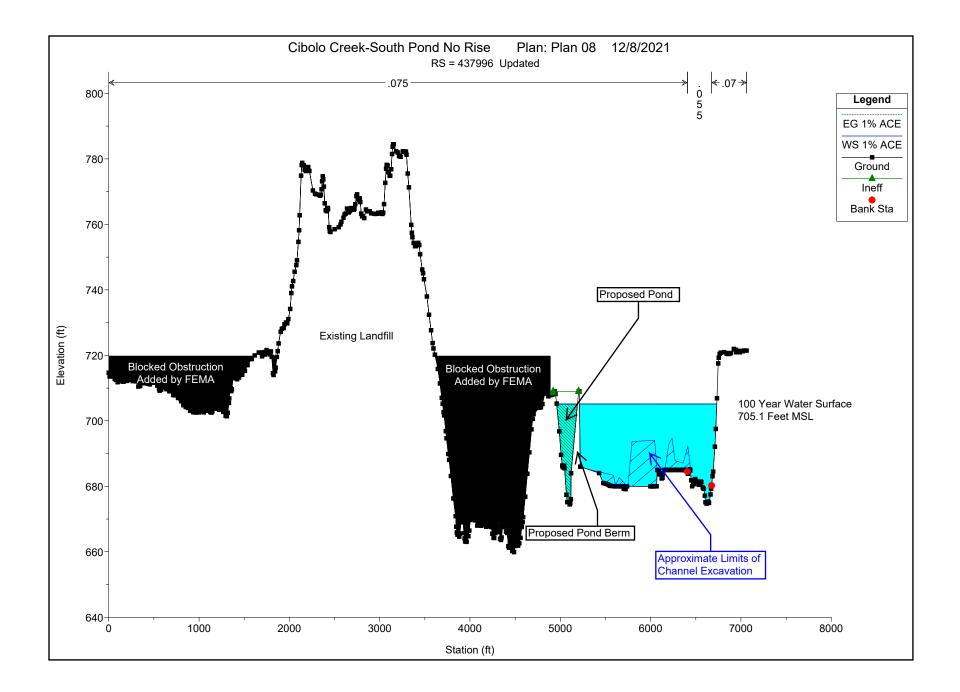


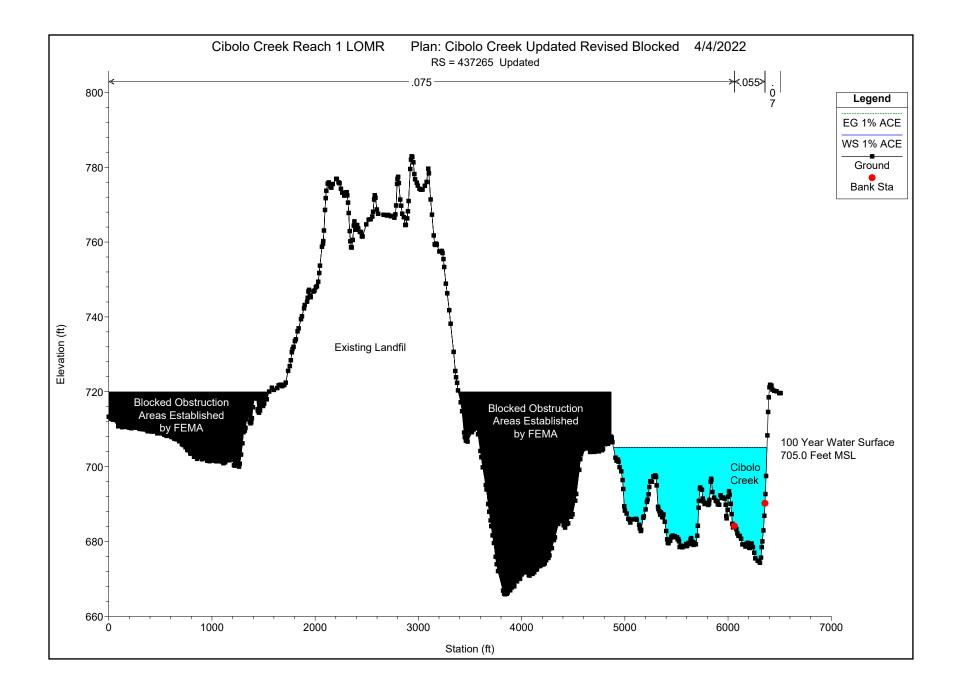


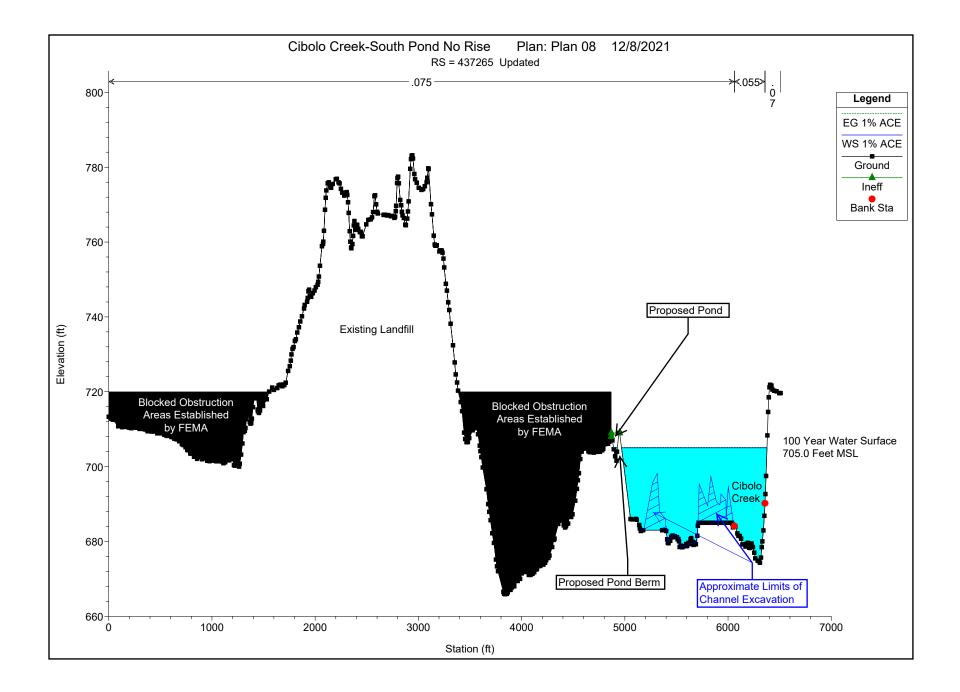












Existing Floodplain Model

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------------|-----------|-----------|--------------------|-----------|-----------|-----------|-----------|------------|----------|-----------|--------------------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Reach 1 | 471492 | 1% ACE | 99469.00 | 727.19 | 763.39 | | 763.62 | 0.000363 | 5.69 | 34601.18 | 2198.78 | 0.19 |
| Reach 1 | 471305 | 1% ACE | 99469.00 | 727.34 | 763.24 | 751.99 | 763.54 | 0.000502 | 6.67 | 32775.37 | 2378.41 | 0.22 |
| Reach 1 | 471274 | | Culvert | | | | | | | | | |
| Reach 1 | 471249 | 1% ACE | 99469.00 | 727.00 | 763.07 | | 763.48 | 0.000476 | 7.82 | 31870.88 | 2281.84 | 0.25 |
| Reach 1 | 471196 | 1% ACE | 99469.00 | 721.11 | 763.04 | | 763.41 | 0.000343 | 7.13 | 33581.38 | 2059.86 | 0.21 |
| Reach 1 | 470981 | 1% ACE | 99469.00 | 723.50 | 762.97 | | 763.33 | 0.000460 | 7.95 | 30999.64 | 1786.67 | 0.24 |
| Reach 1 | 470677 | 1% ACE | 99469.00 | 722.14 | 762.52 | | 763.13 | 0.000750 | 8.87 | 22466.57 | 1240.43 | 0.28 |
| Reach 1 | 470239 | 1% ACE | 99469.00 | 722.06 | 761.48 | | 762.67 | 0.001344 | 10.97 | 15299.25 | 813.35 | 0.34 |
| Reach 1 | 469943 | 1% ACE | 99469.00 | 726.08 | 760.41 | | 762.16 | 0.001764 | 12.09 | 11816.91 | 604.20 | 0.39 |
| Reach 1 | 469604 | 1% ACE | 99469.00 | 722.00 | 759.79 | | 761.57 | 0.001731 | 12.47 | 12261.42 | 652.03 | 0.39 |
| Reach 1 | 469298 | 1% ACE | 99469.00 | 725.79 | 759.46 | 747.88 | 760.99 | 0.001612 | 11.25 | 12723.09 | 768.96 | 0.37 |
| Reach 1 | 468962 | 1% ACE | 99469.00 | 720.47 | 759.04 | 747.79 | 760.45 | 0.001448 | 11.49 | 13295.75 | 717.29 | 0.35 |
| Reach 1 | 468846 | 1% ACE | 99469.00 | 727.87 | 758.89 | 748.23 | 760.25 | 0.001685 | 11.21 | 13163.75 | 735.53 | 0.37 |
| Reach 1 | 468803 | 1% ACE | 99469.00 | 728.39 | 758.74 | 748.00 | 760.17 | 0.001757 | 11.43 | 12859.89 | 730.35 | 0.38 |
| Reach 1 | 468557 | 1% ACE | 99469.00 | 723.63 | 758.18 | 747.86 | 759.75 | 0.001671 | 11.99 | 12723.47 | 679.51 | 0.38 |
| Reach 1 | 468267 | 1% ACE | 99469.00 | 724.43 | 757.54 | 745.26 | 759.29 | 0.001374 | 11.74 | 12328.48 | 764.28 | 0.38 |
| Reach 1 | 467781 | 1% ACE | 99469.00 | 725.38 | 757.35 | | 758.52 | 0.001097 | 10.40 | 15574.31 | 969.35 | 0.34 |
| Reach 1 | 467302 | 1% ACE | 99469.00 | 725.58 | 756.89 | | 757.98 | 0.001053 | 10.18 | 14072.04 | 630.59 | 0.33 |
| Reach 1 | 466729 | 1% ACE | 99423.00 | 720.67 | 755.65 | | 757.26 | 0.001413 | 12.33 | 13246.73 | 721.04 | 0.39 |
| Reach 1 | 466588 | 1% ACE | 99423.00 | 725.23 | 755.51 | 742.11 | 757.05 | 0.001169 | 10.56 | 13238.37 | 1339.60 | 0.35 |
| Reach 1 | 466560 | | Bridge | | | | | | | | | |
| Reach 1 | 466523 | 1% ACE | 99423.00 | 725.23 | 754.88 | | 756.39 | 0.001206 | 10.57 | 12502.43 | 1008.44 | 0.35 |
| Reach 1 | 466490 | 1% ACE | 99423.00 | 721.83 | 755.07 | 740.96 | 756.14 | 0.000893 | 9.83 | 13128.95 | 552.03 | 0.31 |
| Reach 1 | 466425 | | Bridge | | | | | | | | | |
| Reach 1 | 466354 | 1% ACE | 99423.00 | 721.83 | 754.75 | | 755.86 | 0.000928 | 9.96 | 12957.13 | 550.21 | 0.31 |
| Reach 1 | 466304 | 1% ACE | 99423.00 | 715.93 | 754.71 | 738.22 | 755.82 | 0.000769 | 9.73 | 15903.47 | 1426.61 | 0.29 |
| Reach 1 | 466270 | | Bridge | | | | | | | | | |
| Reach 1 | 466222 | 1% ACE | 99423.00 | 715.93 | 754.12 | | 755.32 | 0.000843 | 10.07 | 15228.43 | 1102.21 | 0.30 |
| Reach 1 | 466042 | 1% ACE | 99423.00 | 715.18 | 753.09 | | 754.92 | 0.001761 | 12.33 | 13270.99 | 1211.70 | 0.39 |
| Reach 1 | 465600 | 1% ACE | 99423.00 | 715.50 | 752.36 | | 754.12 | 0.001792 | 12.07 | 13679.66 | 1362.76 | 0.39 |
| Reach 1 | 464951 | 1% ACE | 99423.00 | 714.75 | 751.13 | | 752.86 | 0.002219 | 12.34 | 12943.91 | 1202.00 | 0.39 |
| Reach 1 | 464376 | 1% ACE | 99423.00 | 717.01 | 750.65 | | 751.71 | 0.001298 | 9.49 | 15094.04 | 1016.61 | 0.30 |
| Reach 1 | 463780 | 1% ACE | 99423.00 | 714.00 | 750.30 | | 750.92 | 0.001039 | 8.40 | 17758.21 | 927.53 | 0.25 |
| Reach 1 | 463167 | 1% ACE | 99423.00 | 712.90 | 749.06 | 734.71 | 750.15 | 0.001540 | 9.96 | 15382.57 | 1071.88 | 0.31 |
| Reach 1 | 462386 | 1% ACE | 99423.00 | 707.75 | 748.00 | 730.52 | 749.09 | 0.001254 | 9.06 | 14363.73 | 998.33 | 0.28 |
| Reach 1 | 461701 | 1% ACE | 99423.00 | 706.99 | 745.84 | 734.94 | 747.82 | 0.002534 | 13.04 | 11401.77 | 857.33 | 0.39 |
| Reach 1 | 460978 | 1% ACE | 99903.00 | 707.53 | 744.22 | 731.44 | 746.15 | 0.002076 | 12.15 | 11078.14 | 1532.76 | 0.38 |
| Reach 1 | 460345 | 1% ACE | 99903.00 | 705.78 | 743.39 | | 744.71 | 0.001913 | 12.14 | 15028.20 | 1186.20 | 0.37 |
| Reach 1 | 459910 | 1% ACE | 99903.00 | 704.38 | 741.75 | | 743.73 | 0.002360 | 13.66 | 12401.75 | 991.53 | 0.41 |
| Reach 1 | 459264 | 1% ACE | 99903.00 | 703.48 | 741.05 | | 742.25 | 0.001633 | 11.31 | 14141.04 | 817.55 | 0.34 |
| Reach 1 | 458814 | 1% ACE | 99903.00 | 704.51 | 738.56 | | 741.22 | 0.002421 | 14.72 | 9534.16 | 528.34 | 0.46 |
| Reach 1 | 458337 | 1% ACE | 99903.00 | 704.15 | 736.32 | | 739.87 | 0.002914 | 16.87 | 9485.20 | 736.96 | 0.54 |
| Reach 1 | 457901 | 1% ACE | 99903.00 | 703.93 | 736.12 | | 738.54 | 0.001862 | 13.79 | 10621.30 | 628.31 | 0.44 |
| Reach 1 | 457492 | 1% ACE | 99903.00 | 705.85 | 735.03 | | 737.66 | 0.002384 | 14.54 | 10080.05 | 611.40 | 0.49 |
| Reach 1 | 456713 | 1% ACE | 99903.00 | 703.29 | 734.33 | | 735.97 | 0.001534 | 11.94 | 12018.84 | 577.42 | 0.40 |
| Reach 1 | 456110 | 1% ACE | 99903.00 | 698.65 | 732.00 | | 734.86 | 0.002122 | 14.98 | 9525.05 | 503.88 | 0.47 |
| Reach 1 | 455642 | 1% ACE | 99903.00 | 699.00 | 731.20 | | 733.92 | 0.001927 | 13.66 | 8613.68 | 427.22 | 0.44 |
| Reach 1 | 455149 | 1% ACE | 99903.00 | 697.08 | 729.59 | | 732.70 | 0.003058 | 16.11 | 9203.39 | 585.96 | 0.55 |
| Reach 1 | 454703 | 1% ACE | 99903.00 | 697.00 | 728.76 | | 731.38 | 0.002325 | 14.12 | 9719.65 | 582.75 | 0.48 |
| Reach 1 | 454165 | 1% ACE | 99903.00 | 696.13 | 727.30 | | 730.11 | 0.002426 | 15.50 | 10563.10 | 701.85 | 0.50 |
| Reach 1 | 453783 | 1% ACE | 99903.00 | 695.45 | 726.66 | | 729.12 | 0.002377 | 14.75 | 11174.07 | 835.92 | 0.49 |
| Reach 1 | 453416 | 1% ACE | 99903.00 | 695.21 | 726.33 | | 728.15 | 0.001926 | 12.98 | 12759.13 | 931.88 | 0.44 |
| Reach 1 | 453007 | 1% ACE | 99903.00 | 694.00 | 726.35 | | 727.36 | 0.000979 | 9.78 | 15587.71 | 809.10 | 0.32 |
| Reach 1 | 452334 | 1% ACE | 99724.00 | 698.00 | 726.15 | | 726.69 | 0.000732 | 7.83 | 19628.12 | 1072.52 | 0.27 |
| Reach 1 | 451728 | 1% ACE | 99724.00 | 698.00 | 725.84 | | 726.29 | 0.000556 | 6.58 | 22683.73 | 1772.64 | 0.23 |
| Reach 1 | 451064 | 1% ACE | 99724.00 | 696.38 | 725.64 | | 725.95 | 0.000380 | 4.89 | 29761.14 | 2829.29 | 0.17 |
| Reach 1 | 450390 | 1% ACE | 99724.00 | 694.92 | 725.50 | | 725.66 | 0.000354 | 4.61 | 39483.48 | 3158.26 | 0.16 |
| Reach 1 | 449860 | 1% ACE | 99724.00 | 693.42 | 725.33 | | 725.46 | 0.000357 | 4.56 | 42404.83 | 3598.56 | 0.15 |
| Reach 1 | 449212 | 1% ACE | 99724.00 | 691.25 | 725.11 | | 725.26 | 0.000285 | 4.11 | 43286.68 | 3728.55 | 0.13 |
| Reach 1 | 448507 | 1% ACE | 99724.00 | 688.25 | 724.62 | 745 05 | 724.98 | 0.000497 | 5.63 | 32352.47 | 4178.10 | 0.17 |
| Reach 1 | 447828 | 1% ACE | 99724.00 | 685.72 | 720.46 | 715.65 | 723.97 | 0.003482 | 17.56 | 11159.22 | 1575.21 | 0.55 |
| Reach 1 Reach 1 | 447411 | 1% ACE | 99724.00 | 684.88 | 720.00 | 712.53 | 722.19 | 0.002220 | 14.12 | 12385.17 | 1154.88 | 0.44 |
| | 446945 | 1% ACE | 99724.00 | 684.58 | 719.35 | 705.90 | 720.98 | 0.001799 | 11.57 | 15100.73 | 2232.94 | 0.36 |
| Reach 1 | 446723 | 1% ACE | 83554.00 | 683.76 | 719.24 | 700 70 | 720.06 | 0.000730 | 8.99 | 19643.33 | 1775.99 2061.97 | 0.28 |
| Reach 1 | 446577 | 1% ACE | 83554.00 Bridge | 683.22 | 719.18 | 703.70 | 719.93 | 0.000701 | 7.23 | 15896.08 | 2001.97 | 0.26 |
| Reach 1 | 446515 | 1% ACE | Bridge | 602.00 | 740 40 | | 710.10 | 0.000014 | 0.00 | 11566.00 | 1014.04 | 0.00 |
| Reach 1 | 446493 | 1% ACE | 83554.00 | 683.22 | 718.12 | 701 71 | 719.12 | 0.000914 | 8.08 | 11566.08 | 1214.31 | 0.29 |
| Reach 1 | 446478 | 1% ACE | 83554.00 | 678.39 | 718.30 | 701.74 | 718.91 | 0.000507 | 6.52 | 16591.38 | 1748.63 | 0.22 |
| Reach 1 | 446440 | 40/ 4 2 - | Bridge | | | | | 0.0000 | | | | |
| Reach 1 | 446383 | 1% ACE | 83554.00 | 678.39 | 717.88 | | 718.52 | 0.000547 | 6.70 | 15749.16 | 1641.55 | 0.23 |
| Reach 1 | 446236 | 1% ACE | 83554.00 | 686.27 | 716.12 | | 718.00 | 0.002356 | 12.35 | 12083.89 | 1951.03 | 0.40 |
| Reach 1 | 446037 | 1% ACE | 83554.00 | 685.26 | 716.14 | | 717.43 | 0.001662 | 10.38 | 14568.45 | 2171.55 | 0.34 |
| Reach 1 | 445573 | 1% ACE | 83554.00 | 683.27 | 715.47 | | 716.64 | 0.001635 | 10.24 | 13853.91 | 1272.36 | 0.34 |
| Reach 1 | 445235 | 1% ACE | 74844.00 | 683.27 | 715.46 | | 716.09 | 0.000839 | 7.38 | 14446.55 | 819.21 | 0.24 |
| Reach 1 | 444777 | 1% ACE | 74844.00 | 683.27 | 714.34 | | 715.55 | 0.001357 | 9.41 | 9324.66 | 418.29 | 0.31 |

| Reach | River Sta | Profile | d River: Cibolo Q Total | Min Ch El | W.S. Elev | Profile: 1% ACE Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------------|------------------|------------------|----------------------------|------------------|------------------|------------------------------|------------------|------------|---------------|----------------------|-------------------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Reach 1 | 444240 | 1% ACE | 74844.00 | 683.14 | 712.59 | | 714.56 | 0.002177 | 11.70 | 7112.57 | 303.76 | 0.39 |
| Reach 1 | 443555 | 1% ACE | 74844.00 | 682.52 | 712.24 | | 713.19 | 0.001159 | 8.05 | 9943.71 | 424.81 | 0.28 |
| Reach 1 | 442891 | 1% ACE | 74844.00 | 679.79 | 711.58 | | 712.49 | 0.000944 | 7.77 | 10195.40 | 409.13 | 0.25 |
| Reach 1 | 442214 | 1% ACE | 74844.00 | 678.90 | 709.72 | | 711.43 | 0.002485 | 12.16 | 8711.94 | 548.33 | 0.40 |
| Reach 1 | 441476 | 1% ACE | 74844.00 | 678.52 | 708.12 | | 709.76 | 0.001991 | 10.59 | 7947.43 | 421.93 | 0.36 |
| Reach 1 | 440762 | 1% ACE | 74844.00 | 677.76 | 705.81 | | 707.89 | 0.002707 | 11.80 | 6709.83 | 304.53 | 0.42 |
| Reach 1 | 439971 | 1% ACE | 74844.00 | 677.96 | 705.51 | | 705.71 | 0.000410 | 4.27 | 22216.60 | 1144.96 | 0.16 |
| Reach 1 | 438740 | 1% ACE | 74844.00 | 675.84 | 705.30 | | 705.41 | 0.000223 | 3.38 | 33040.49 | 1844.11 | 0.12 |
| Reach 1 | 437996 | 1% ACE | 74844.00 | 674.71 | 705.21 | | 705.29 | 0.000189 | 3.18 | 35176.72 | 1824.69 | 0.11 |
| Reach 1 | 437265 | 1% ACE | 74844.00 | 674.32 | 705.03 | | 705.18 | 0.000290 | 3.98 | 27754.92 | 1486.97 | 0.14 |
| Reach 1 | 436536 | 1% ACE | 74844.00 | 673.98 | 704.27 | | 704.82 | 0.000810 | 6.89 | 15281.89 | 921.79 | 0.23 |
| Reach 1 Reach 1 | 435810 435043 | 1% ACE 1% ACE | 74844.00 74844.00 | 672.59 672.92 | 703.05 | | 703.98 703.12 | 0.001244 | 8.45 7.03 | 10535.21 | 526.54 513.44 | 0.29 |
| Reach 1 | 434453 | 1% ACE | 74844.00 | 672.92 | 702.40 | | 703.12 | 0.000674 | 9.93 | 11817.77 10304.78 | 657.11 | 0.24 |
| Reach 1 | 434455 | 1% ACE | 74844.00 | 668.74 | 701.08 | | 702.28 | 0.001006 | 9.93 7.16 | 14270.50 | 937.56 | 0.34 |
| Reach 1 | 433539 | 1% ACE | 74844.00 | 667.11 | 700.47 | | 701.07 | 0.000790 | 6.40 | 16157.71 | 1041.30 | 0.24 |
| Reach 1 | 433408 | 1% ACE | 74844.00 | 667.31 | 700.39 | | 700.83 | 0.000749 | 6.22 | 17384.43 | 1111.20 | 0.21 |
| Reach 1 | 433181 | 1% ACE | 86791.00 | 667.56 | 700.34 | | 700.53 | 0.000746 | 5.98 | 23132.56 | 1884.55 | 0.21 |
| Reach 1 | 432987 | 1% ACE | 86791.00 | 665.50 | 699.92 | 686.97 | 700.33 | 0.000710 | 6.73 | 20951.47 | 1542.86 | 0.20 |
| Reach 1 | 432930 | TRACE | Bridge | 000.00 | 033.32 | 000.37 | 700.04 | 0.000723 | 0.75 | 20331.47 | 1342.00 | 0.22 |
| Reach 1 | 432930 | 1% ACE | 86791.00 | 665.72 | 699.66 | | 700.17 | 0.000949 | 7.65 | 19846.78 | 1626.99 | 0.25 |
| Reach 1 | 432695 | 1% ACE | 86791.00 | 664.85 | 699.28 | | 699.98 | 0.000949 | 8.41 | 18273.86 | 1533.98 | 0.23 |
| Reach 1 | 432475 | 1% ACE | 86791.00 | 664.59 | 699.28 | | 699.73 | 0.001047 | 7.07 | 21018.98 | 1563.84 | 0.27 |
| Reach 1 | 431631 | 1% ACE | 86791.00 | 663.50 | 698.71 | | 699.12 | 0.000648 | 6.09 | 19799.95 | 1149.51 | 0.22 |
| Reach 1 | 430804 | 1% ACE | 86791.00 | 662.05 | 698.03 | | 698.58 | 0.000627 | 6.69 | 17626.60 | 977.00 | 0.21 |
| Reach 1 | 429757 | 1% ACE | 86791.00 | 659.79 | 697.35 | | 697.94 | 0.000607 | 6.49 | 16411.76 | 946.76 | 0.21 |
| Reach 1 | 428966 | 1% ACE | 86791.00 | 660.22 | 696.67 | | 697.37 | 0.000933 | 8.13 | 17012.12 | 1091.79 | 0.26 |
| Reach 1 | 428447 | 1% ACE | 86791.00 | 655.39 | 696.31 | | 696.97 | 0.000842 | 7.91 | 17600.38 | 1104.76 | 0.24 |
| Reach 1 | 427784 | 1% ACE | 86791.00 | 657.72 | 695.61 | | 696.42 | 0.000912 | 8.09 | 15742.63 | 1354.07 | 0.25 |
| Reach 1 | 427183 | 1% ACE | 86791.00 | 658.56 | 695.14 | | 695.88 | 0.000854 | 7.81 | 17395.66 | 1465.38 | 0.24 |
| Reach 1 | 426517 | 1% ACE | 86791.00 | 658.35 | 693.57 | | 694.97 | 0.001543 | 10.35 | 13492.51 | 1726.15 | 0.33 |
| Reach 1 | 425901 | 1% ACE | 86791.00 | 658.89 | 692.66 | | 694.01 | 0.001489 | 9.78 | 11945.38 | 1823.57 | 0.32 |
| Reach 1 | 425293 | 1% ACE | 86791.00 | 657.30 | 691.32 | | 692.91 | 0.001912 | 11.13 | 11674.76 | 1309.53 | 0.36 |
| Reach 1 | 424714 | 1% ACE | 99926.00 | 656.85 | 689.55 | | 691.50 | 0.002581 | 12.30 | 11744.29 | 1014.46 | 0.42 |
| Reach 1 | 424187 | 1% ACE | 99926.00 | 655.55 | 687.40 | | 689.74 | 0.003931 | 13.70 | 11114.38 | 1727.31 | 0.47 |
| Reach 1 | 423625 | 1% ACE | 99926.00 | 653.68 | 686.08 | | 687.57 | 0.002622 | 11.43 | 14768.28 | 2343.14 | 0.39 |
| Reach 1 | 422995 | 1% ACE | 99926.00 | 651.65 | 685.66 | | 686.27 | 0.001298 | 8.21 | 21717.47 | 2895.78 | 0.27 |
| Reach 1 | 422251 | 1% ACE | 99926.00 | 651.19 | 683.89 | | 685.01 | 0.002224 | 10.61 | 17479.30 | 2623.13 | 0.36 |
| Reach 1 | 421444 | 1% ACE | 99926.00 | 651.00 | 681.94 | | 683.14 | 0.002420 | 11.12 | 17377.66 | 2736.31 | 0.37 |
| Reach 1 | 420481 | 1% ACE | 99926.00 | 650.01 | 679.82 | | 680.85 | 0.002270 | 10.60 | 19928.69 | 3080.66 | 0.36 |
| Reach 1 | 419470 | 1% ACE | 99926.00 | 649.95 | 677.34 | | 678.56 | 0.002379 | 10.19 | 18437.24 | 3058.44 | 0.36 |
| Reach 1 | 418854 | 1% ACE | 99926.00 | 647.17 | 673.65 | 669.50 | 675.94 | 0.006762 | 14.94 | 14870.99 | 3220.12 | 0.55 |
| Reach 1 | 418726 | 1% ACE | 99926.00 | 645.66 | 673.16 | | 674.47 | 0.004272 | 12.13 | 18139.93 | 2987.12 | 0.47 |
| Reach 1 | 418630 | 1% ACE | 99926.00 | 646.57 | 673.02 | | 673.92 | 0.002823 | 10.06 | 20295.93 | 2916.49 | 0.38 |
| Reach 1 | 418516 | 1% ACE | 99926.00 | 645.77 | 672.91 | | 673.55 | 0.002067 | 8.78 | 22416.64 | 2924.63 | 0.33 |
| Reach 1 | 418186 | 1% ACE | 99926.00 | 646.00 | 671.63 | | 672.69 | 0.003618 | 11.74 | 18578.89 | 2782.59 | 0.43 |
| Reach 1 | 417994 | 1% ACE | 99926.00 | 646.22 | 671.06 | | 671.93 | 0.003361 | 10.79 | 19102.21 | 2394.25 | 0.39 |
| Reach 1 | 417303 | 1% ACE | 99986.00 | 641.33 | 670.19 | | 670.61 | 0.000819 | 6.50 | 22004.13 | 1458.89 | 0.22 |
| Reach 1 | 415588 | 1% ACE | 99986.00 | 642.08 | 669.19 | | 669.34 | 0.000576 | 4.31 | 36541.04 | 3494.54 | 0.17 |
| Reach 1 | 413959 | 1% ACE | 99986.00 | 639.83 | 668.36 | | 668.52 | 0.000467 | 4.23 | 35303.80 | 2983.67 | 0.16 |
| Reach 1 | 412994 | 1% ACE | 99986.00 | 638.91 | 668.04 | | 668.17 | 0.000370 | 3.62 | 38670.32 | 3239.86 | 0.13 |
| Reach 1 | 412056 | 1% ACE | 99986.00 | 638.83 | 667.80 | | 667.88 | 0.000269 | 3.10 | 46699.70 | 3143.43 | 0.11 |
| Reach 1 | 411408 | 1% ACE | 99986.00 | 637.92 | 667.67 | | 667.77 | 0.000315 | 3.42 | 44141.79 | 2987.15 | 0.12 |
| Reach 1 | 410660 | 1% ACE | 99986.00 | 634.42 | 667.29 | | 667.50 | 0.000395 | 5.15 | 35082.88 | 2425.33 | 0.18 |
| Reach 1 | 409107 | 1% ACE | 99986.00 | 633.83 | 666.16 | | 666.68 | 0.000548 | 6.73 | 22106.15 | 1237.07 | 0.22 |
| Reach 1 | 408599 | 1% ACE | 99986.00 | 631.17 | 666.00 | | 666.38 | 0.000494 | 5.43 | 22324.77 | 972.68 | 0.17 |
| Reach 1 | 408038 | 1% ACE | 99986.00 | 623.97 | 665.78 | | 666.14 | 0.000379 | 4.90 | 21923.51 | 800.76 | 0.15 |
| Reach 1 | 407323 | 1% ACE | 99986.00 | 625.42 | 662.33 | | 664.91 | 0.002816 | 14.57 | 9429.65 | 497.60 | 0.44 |
| Reach 1 | 406437 | 1% ACE | 99986.00 | 626.75 | 661.14 | | 662.21 | 0.001111 | 8.67 | 13701.50 | 733.71 | 0.28 |
| Reach 1 | 405800 405065 | 1% ACE 1% ACE | 99986.00 99986.00 | 625.19 623.87 | 661.04 | | 661.51 660.82 | 0.000414 | 5.60 10.91 | 19732.68 | 886.29 | 0.17 |
| Reach 1 Reach 1 | 405065 | 1% ACE 1% ACE | 99986.00 | 623.87 | 659.43 658.99 | | 659.84 | 0.002263 | 10.91 | 12846.01 15229.70 | 878.94 1004.13 | 0.36 |
| Reach 1 Reach 1 | 404559 | 1% ACE | 99986.00 | 624.37 | 658.45 | | 659.84 | 0.001392 | 6.69 | 18975.41 | 946.23 | 0.29 |
| Reach 1 | 403073 | 1% ACE | 99986.00 | 622.00 | 657.82 | | 658.60 | 0.000993 | 7.72 | 17770.30 | 1259.77 | 0.20 |
| Reach 1 | 403073 | 1% ACE | 99986.00 | 622.00 | 656.92 | | 657.98 | 0.000993 | 8.50 | 13724.82 | 852.67 | 0.24 |
| Reach 1 | 402310 | 1% ACE | 99986.00 | 620.86 | 656.77 | | 657.58 | 0.000595 | 7.58 | 17021.13 | 1085.78 | 0.20 |
| Reach 1 | 402110 | 1% ACE | 99986.00 | 617.34 | 656.80 | | 657.19 | 0.000548 | 5.88 | 23325.88 | 2226.19 | 0.23 |
| Reach 1 | 401038 | 1% ACE | 99986.00 | 618.50 | 654.83 | | 656.36 | 0.000348 | 11.35 | 16225.03 | 2700.87 | 0.15 |
| Reach 1 | 399722 | 1% ACE | 100009.00 | 614.28 | 653.98 | | 654.57 | 0.002107 | 6.73 | 23308.38 | 2700.87 | 0.35 |
| Reach 1 | 398748 | 1% ACE | 100009.00 | 610.94 | 652.50 | | 653.56 | 0.000718 | 8.60 | 15689.14 | 2141.77 | 0.21 |
| Reach 1 | 398061 | 1% ACE | 100009.00 | 612.67 | 651.63 | | 652.62 | 0.001221 | 8.88 | 17302.29 | 1963.08 | 0.27 |
| Reach 1 | 397096 | 1% ACE | 100009.00 | 611.67 | 650.05 | | 651.19 | 0.001445 | 9.29 | 17302.29 | 2785.04 | 0.29 |
| Reach 1 | 396117 | 1% ACE | 100009.00 | 612.77 | 648.24 | | 649.48 | 0.001564 | 9.29 | 16346.06 | 2765.04 | 0.30 |
| Reach 1 | 395546 | 1% ACE | 99891.00 | 612.04 | 644.74 | 637.89 | 649.48 | 0.001923 | 10.12 | 10346.06 | 1852.09 | 0.53 |
| Reach 1 | 395546 | 1% ACE | 99891.00 | 612.04 | 644.74 | 001.09 | 645.00 | 0.004709 | 14.00 | 9204.31 | 1083.60 | 0.51 |

HEC-RAS Plan: Updated Revised Blocked River: Cibolo Creek Reach: Reach 1 Profile: 1% ACE (Continued)

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|---------|-----------|---------|----------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Reach 1 | 394251 | 1% ACE | 99891.00 | 609.16 | 640.69 | | 642.38 | 0.002586 | 10.67 | 10801.81 | 896.98 | 0.38 |
| Reach 1 | 393283 | 1% ACE | 99891.00 | 605.09 | 640.57 | | 640.89 | 0.000407 | 4.71 | 24071.18 | 1971.56 | 0.15 |
| Reach 1 | 392124 | 1% ACE | 99891.00 | 603.00 | 639.29 | | 640.09 | 0.000925 | 7.32 | 16874.27 | 2662.70 | 0.23 |
| Reach 1 | 391531 | 1% ACE | 99891.00 | 600.99 | 638.24 | | 639.36 | 0.001235 | 8.73 | 14879.94 | 3221.42 | 0.29 |
| Reach 1 | 390995 | 1% ACE | 99891.00 | 601.37 | 637.85 | | 638.68 | 0.000852 | 7.90 | 19134.05 | 2997.57 | 0.24 |
| Reach 1 | 390516 | 1% ACE | 99891.00 | 597.90 | 637.61 | | 638.09 | 0.000859 | 7.02 | 27225.76 | 3853.10 | 0.24 |
| Reach 1 | 390125 | 1% ACE | 99891.00 | 597.14 | 637.67 | | 637.80 | 0.000145 | 3.46 | 49861.13 | 4814.63 | 0.10 |
| Reach 1 | 388545 | 1% ACE | 99891.00 | 596.19 | 637.17 | | 637.44 | 0.000352 | 4.56 | 36417.01 | 5373.92 | 0.14 |
| Reach 1 | 387329 | 1% ACE | 99891.00 | 597.51 | 636.48 | | 636.84 | 0.000718 | 5.65 | 31584.72 | 4631.85 | 0.20 |
| Reach 1 | 386808 | 1% ACE | 99891.00 | 600.00 | 635.44 | | 636.25 | 0.001411 | 8.97 | 26523.83 | 5095.13 | 0.28 |
| Reach 1 | 386042 | 1% ACE | 99891.00 | 600.00 | 635.30 | | 635.61 | 0.000271 | 4.91 | 37662.01 | 6497.65 | 0.17 |
| Reach 1 | 384847 | 1% ACE | 99891.00 | 594.65 | 633.95 | 617.86 | 634.89 | 0.000901 | 9.09 | 27736.11 | 6078.30 | 0.28 |

Summary Table Including Pond

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|--------------------|-----------|-----------|--------------------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Reach 1 | 471492 | 1% ACE | 99469.00 | 727.19 | 763.39 | | 763.62 | 0.000363 | 5.69 | 34603.86 | 2198.80 | 0.19 |
| Reach 1 | 471305 | 1% ACE | 99469.00 | 727.34 | 763.24 | 752.00 | 763.54 | 0.000502 | 6.67 | 32778.41 | 2378.44 | 0.22 |
| Reach 1 | 471274 | | Culvert | | | | | | | | | |
| Reach 1 | 471249 | 1% ACE | 99469.00 | 727.00 | 763.07 | | 763.48 | 0.000476 | 7.82 | 31873.67 | 2281.89 | 0.25 |
| Reach 1 | 471196 | 1% ACE | 99469.00 | 721.11 | 763.04 | | 763.41 | 0.000343 | 7.13 | 33583.77 | 2059.91 | 0.21 |
| Reach 1 | 470981 | 1% ACE | 99469.00 | 723.50 | 762.97 | | 763.33 | 0.000460 | 7.95 | 31001.71 | 1786.70 | 0.24 |
| Reach 1 | 470677 | 1% ACE | 99469.00 | 722.14 | 762.52 | | 763.13 | 0.000750 | 8.87 | 22468.09 | 1240.46 | 0.28 |
| Reach 1 | 470239 | 1% ACE | 99469.00 | 722.06 | 761.48 | | 762.67 | 0.001343 | 10.97 | 15300.34 | 813.38 | 0.34 |
| Reach 1 | 469943 | 1% ACE | 99469.00 | 726.08 | 760.41 | | 762.16 | 0.001764 | 12.09 | 11817.76 | 604.22 | 0.39 |
| Reach 1 | 469604 | 1% ACE | 99469.00 | 722.00 | 759.79 | | 761.58 | 0.001730 | 12.47 | 12262.42 | 652.06 | 0.39 |
| Reach 1 | 469298 | 1% ACE | 99469.00 | 725.79 | 759.47 | 747.88 | 760.99 | 0.001611 | 11.25 | 12724.41 | 769.03 | 0.37 |
| Reach 1 | 468962 | 1% ACE | 99469.00 | 720.47 | 759.04 | 747.79 | 760.45 | 0.001447 | 11.49 | 13296.89 | 717.42 | 0.35 |
| Reach 1 | 468846 | 1% ACE | 99469.00 | 727.87 | 758.90 | 748.23 | 760.25 | 0.001684 | 11.21 | 13165.05 | 735.56 | 0.37 |
| Reach 1 | 468803 | 1% ACE | 99469.00 | 728.39 | 758.74 | 748.00 | 760.17 | 0.001757 | 11.42 | 12861.22 | 730.57 | 0.38 |
| Reach 1 | 468557 | 1% ACE | 99469.00 | 723.63 | 758.18 | 747.87 | 759.75 | 0.001670 | 11.99 | 12724.96 | 679.54 | 0.38 |
| Reach 1 | 468267 | 1% ACE | 99469.00 | 724.43 | 757.54 | 745.26 | 759.29 | 0.001373 | 11.74 | 12330.34 | 764.34 | 0.38 |
| Reach 1 | 467781 | 1% ACE | 99469.00 | 725.38 | 757.35 | | 758.52 | 0.001097 | 10.39 | 15576.80 | 969.45 | 0.34 |
| Reach 1 | 467302 | 1% ACE | 99469.00 | 725.58 | 756.89 | | 757.98 | 0.001053 | 10.18 | 14073.73 | 630.65 | 0.33 |
| Reach 1 | 466729 | 1% ACE | 99423.00 | 720.67 | 755.65 | | 757.27 | 0.001412 | 12.33 | 13248.97 | 721.16 | 0.39 |
| Reach 1 | 466588 | 1% ACE | 99423.00 | 725.23 | 755.52 | 742.13 | 757.06 | 0.001169 | 10.56 | 13242.63 | 1341.25 | 0.35 |
| Reach 1 | 466560 | | Bridge | | | | | | | | | |
| Reach 1 | 466523 | 1% ACE | 99423.00 | 725.23 | 754.88 | | 756.40 | 0.001205 | 10.57 | 12505.76 | 1010.16 | 0.35 |
| Reach 1 | 466490 | 1% ACE | 99423.00 | 721.83 | 755.07 | 740.96 | 756.14 | 0.000893 | 9.83 | 13130.91 | 552.05 | 0.31 |
| Reach 1 | 466425 | | Bridge | | | | | | | | | |
| Reach 1 | 466354 | 1% ACE | 99423.00 | 721.83 | 754.76 | | 755.86 | 0.000928 | 9.96 | 12959.15 | 550.23 | 0.31 |
| Reach 1 | 466304 | 1% ACE | 99423.00 | 715.93 | 754.71 | 738.22 | 755.82 | 0.000769 | 9.73 | 15909.23 | 1432.46 | 0.29 |
| Reach 1 | 466270 | | Bridge | | | | | | | | | |
| Reach 1 | 466222 | 1% ACE | 99423.00 | 715.93 | 754.12 | | 755.32 | 0.000842 | 10.07 | 15232.27 | 1102.32 | 0.30 |
| Reach 1 | 466042 | 1% ACE | 99423.00 | 715.18 | 753.09 | | 754.92 | 0.001760 | 12.32 | 13276.31 | 1212.22 | 0.39 |
| Reach 1 | 465600 | 1% ACE | 99423.00 | 715.50 | 752.37 | | 754.13 | 0.001790 | 12.06 | 13687.73 | 1363.36 | 0.39 |
| Reach 1 | 464951 | 1% ACE | 99423.00 | 714.75 | 751.14 | | 752.87 | 0.002216 | 12.34 | 12952.27 | 1202.40 | 0.39 |
| Reach 1 | 464376 | 1% ACE | 99423.00 | 717.01 | 750.66 | | 751.72 | 0.001296 | 9.49 | 15101.61 | 1016.85 | 0.30 |
| Reach 1 | 463780 | 1% ACE | 99423.00 | 714.00 | 750.30 | | 750.93 | 0.001038 | 8.40 | 17765.46 | 927.86 | 0.25 |
| Reach 1 | 463167 | 1% ACE | 99423.00 | 712.90 | 749.07 | 734.72 | 750.15 | 0.001538 | 9.95 | 15393.04 | 1072.34 | 0.31 |
| Reach 1 | 462386 | 1% ACE | 99423.00 | 707.75 | 748.01 | 730.52 | 749.10 | 0.001255 | 9.07 | 14369.86 | 1004.12 | 0.28 |
| Reach 1 | 461701 | 1% ACE | 99423.00 | 706.99 | 745.85 | 734.95 | 747.82 | 0.002530 | 13.04 | 11409.57 | 857.98 | 0.39 |
| Reach 1 | 460978 | 1% ACE | 99903.00 | 707.53 | 744.23 | 731.45 | 746.16 | 0.002073 | 12.15 | 11087.09 | 1533.58 | 0.38 |
| Reach 1 | 460345 | 1% ACE | 99903.00 | 705.78 | 743.40 | | 744.73 | 0.001907 | 12.12 | 15048.04 | 1186.89 | 0.37 |
| Reach 1 | 459910 | 1% ACE | 99903.00 | 704.38 | 741.78 | | 743.75 | 0.002350 | 13.64 | 12425.73 | 992.56 | 0.41 |
| Reach 1 | 459264 | 1% ACE | 99903.00 | 703.48 | 741.08 | | 742.27 | 0.001627 | 11.30 | 14162.66 | 818.22 | 0.34 |
| Reach 1 | 458814 | 1% ACE | 99903.00 | 704.51 | 738.60 | | 741.25 | 0.002410 | 14.70 | 9553.04 | 529.31 | 0.46 |
| Reach 1 | 458337 | 1% ACE | 99903.00 | 704.15 | 736.39 | | 739.90 | 0.002885 | 16.81 | 9534.75 | 740.53 | 0.54 |
| Reach 1 | 457901 | 1% ACE | 99903.00 | 703.93 | 736.18 | | 738.59 | 0.001847 | 13.75 | 10662.95 | 630.96 | 0.44 |
| Reach 1 | 457492 | 1% ACE | 99903.00 | 705.85 | 735.12 | | 737.73 | 0.002351 | 14.47 | 10135.58 | 612.28 | 0.49 |
| Reach 1 | 456713 | 1% ACE | 99903.00 | 703.29 | 734.43 | | 736.05 | 0.001513 | 11.88 | 12077.46 | 578.20 | 0.39 |
| Reach 1 | 456110 | 1% ACE | 99903.00 | 698.65 | 732.14 | | 734.96 | 0.002084 | 14.89 | 9596.47 | 505.85 | 0.46 |
| Reach 1 | 455642 | 1% ACE | 99903.00 | 699.00 | 731.35 | | 734.04 | 0.001891 | 13.58 | 8680.92 | 429.05 | 0.43 |
| Reach 1 | 455149 | 1% ACE | 99903.00 | 697.08 | 729.83 | | 732.86 | 0.002949 | 15.92 | 9344.31 | 590.76 | 0.54 |
| Reach 1 | 454703 | 1% ACE | 99903.00 | 697.00 | 729.03 | | 731.58 | 0.002233 | 13.93 | 9882.62 | 588.14 | 0.47 |
| Reach 1 | 454165 | 1% ACE | 99903.00 | 696.13 | 727.69 | | 730.37 | 0.002294 | 15.21 | 10841.26 | 727.17 | 0.49 |
| Reach 1 | 453783 | 1% ACE | 99903.00 | 695.45 | 727.15 | | 729.44 | 0.002184 | 14.30 | 11582.39 | | 0.47 |
| Reach 1 | 453416 | 1% ACE | 99903.00 | 695.21 | 726.86 | | 728.54 | 0.001749 | 12.54 | 13257.83 | 940.00 | 0.42 |
| Reach 1 | 453007 | 1% ACE | 99903.00 | 694.00 | 726.87 | | 727.82 | 0.000908 | 9.53 | 16007.40 | 812.67 | 0.31 |
| Reach 1 | 452334 | 1% ACE | 99724.00 | 698.00 | 726.69 | | 727.20 | 0.000677 | 7.64 | 20211.48 | | 0.26 |
| Reach 1 | 451728 | 1% ACE | 99724.00 | 698.00 | 726.41 | | 726.83 | 0.000504 | 6.36 | 23701.85 | | 0.22 |
| Reach 1 | 451064 | 1% ACE | 99724.00 | 696.38 | 726.24 | | 726.52 | 0.000337 | 4.68 | 31475.13 | 2865.18 | 0.16 |
| Reach 1 | 450390 | 1% ACE | 99724.00 | 694.92 | 726.10 | | 726.26 | 0.000336 | 4.56 | 41448.16 | 3594.21 | 0.15 |
| Reach 1 | 449860 | 1% ACE | 99724.00 | 693.42 | 725.96 | | 726.08 | 0.000309 | 4.30 | 44680.14 | 3634.28 | 0.13 |
| Reach 1 | 449212 | 1% ACE | 99724.00 | 691.25 | 725.90 | | 725.90 | 0.000309 | 4.30 | 45753.06 | 3824.58 | 0.14 |
| Reach 1 | 448507 | 1% ACE | 99724.00 | 688.25 | 725.36 | | 725.66 | 0.000231 | 5.23 | 35489.20 | 4258.06 | 0.12 |
| Reach 1 | 440507 | 1% ACE | 99724.00 | 685.72 | 725.30 | 715.65 | 725.00 | 0.000416 | 16.86 | 13364.60 | 2197.47 | 0.16 |
| Reach 1 | 447411 | 1% ACE | 99724.00 | 684.88 | 721.39 | 713.03 | 724.75 | 0.003003 | 16.63 | 12391.02 | 2197.47 | 0.51 |
| Reach 1 | 446945 | 1% ACE | 99724.00 | 684.58 | 720.00 | 712.53 | 720.98 | 0.003078 | 11.57 | 15095.69 | | 0.36 |
| Reach 1 | 446945 | 1% ACE | 83554.00 | 683.76 | 719.35 | 100.91 | 720.96 | 0.001800 | 9.00 | 19639.21 | 1775.88 | 0.30 |
| Reach 1 | 446723 | 1% ACE | 83554.00 | 683.22 | 719.24 | 703.69 | 720.06 | 0.000730 | 7.23 | 15891.17 | 2061.55 | 0.26 |
| Reach 1 Reach 1 | 446515 | TRACE | | 003.22 | 1 19.18 | 103.09 | 1 19.93 | 0.000702 | 1.23 | 10091.17 | 2001.00 | 0.20 |
| | | 1% ACE | Bridge 83554.00 | 683.22 | 710 40 | | 719.11 | 0.000914 | 8.09 | 11569.00 | 1011 17 | 0.29 |
| Reach 1 | 446493 | 1% ACE | 83554.00 | | 718.12 | 704 70 | | | | 11563.26 | 1214.17 | |
| Reach 1 | 446478 | 1% ACE | 83554.00 Bridge | 678.39 | 718.30 | 701.78 | 718.91 | 0.000507 | 6.52 | 16587.43 | 1748.27 | 0.22 |
| Reach 1 | 446440 | 404 4 6 7 | Bridge | | | | | 0.0000 | | 400.000 | | |
| Reach 1 | 446383 | 1% ACE | 83554.00 | 678.39 | 717.87 | | 718.52 | 0.000548 | 6.70 | 15744.55 | 1641.23 | 0.23 |
| Reach 1 | 446236 | 1% ACE | 83554.00 | 686.27 | 716.11 | | 718.00 | 0.002359 | 12.36 | 12071.99 | 1947.70 | 0.40 |
| Reach 1 | 446037 | 1% ACE | 83554.00 | 685.26 | 716.13 | | 717.43 | 0.001665 | 10.39 | 14552.55 | 2171.10 | 0.34 |
| Reach 1 | 445573 | 1% ACE | 83554.00 | 683.27 | 715.46 | | 716.63 | 0.001638 | 10.24 | 13842.34 | 1272.20 | 0.34 |
| Reach 1 | 445235 | 1% ACE | 74844.00 | 683.27 | 715.45 | | 716.08 | 0.000840 | 7.38 | 14439.60 | 819.04 | 0.24 |
| Reach 1 | 444777 | 1% ACE | 74844.00 | 683.27 | 714.33 | | 715.54 | 0.001358 | 9.41 | 9320.71 | 418.22 | 0.31 |

| Reach | River Sta | Profile | Q Total (cfs) | Min Ch El (ft) | W.S. Elev (ft) | Crit W.S. (ft) | E.G. Elev (ft) | E.G. Slope (ft/ft) | Vel Chnl (ft/s) | Flow Area (sq ft) | Top Width (ft) | Froude # Chl |
|---------|-----------|---------|------------------|-------------------|-------------------|-------------------|-------------------|-----------------------|--------------------|----------------------|-------------------|--------------|
| Reach 1 | 444240 | 1% ACE | 74844.00 | 683.14 | 712.57 | (11) | 714.55 | 0.002181 | 11.70 | 7109.03 | 303.73 | 0.3 |
| Reach 1 | 443555 | 1% ACE | 74844.00 | 682.52 | 712.37 | | 713.18 | 0.002101 | 8.06 | 9938.32 | 424.75 | 0.3 |
| Reach 1 | 442891 | 1% ACE | 74844.00 | 679.79 | 711.56 | | 712.47 | 0.000946 | 7.78 | 10189.74 | 409.03 | 0.2 |
| Reach 1 | 442214 | 1% ACE | 74844.00 | 678.90 | 709.70 | | 711.42 | 0.002494 | 12.18 | 8700.73 | 548.28 | 0.4 |
| Reach 1 | 441476 | 1% ACE | 74844.00 | 678.52 | 708.09 | | 709.74 | 0.001998 | 10.60 | 7936.46 | 421.75 | 0.3 |
| Reach 1 | 440762 | 1% ACE | 74844.00 | 677.76 | 705.78 | | 707.86 | 0.002716 | 11.82 | 6702.37 | 303.83 | 0.4 |
| Reach 1 | 439971 | 1% ACE | 74844.00 | 677.96 | 705.33 | | 705.70 | 0.000510 | 5.08 | 16345.16 | 1073.76 | 0.1 |
| Reach 1 | 438740 | 1% ACE | 74844.00 | 675.84 | 705.21 | | 705.30 | 0.000121 | 2.49 | 31548.81 | 1797.33 | 0.0 |
| Reach 1 | 437996 | 1% ACE | 74844.00 | 674.71 | 705.13 | | 705.21 | 0.000159 | 2.91 | 34735.68 | 1750.08 | 0.1 |
| Reach 1 | 437265 | 1% ACE | 74844.00 | 674.32 | 705.03 | | 705.13 | 0.000203 | 3.33 | 30788.60 | 1446.20 | 0.1 |
| Reach 1 | 436536 | 1% ACE | 74844.00 | 673.98 | 704.27 | | 704.82 | 0.000810 | 6.89 | 15281.55 | 921.78 | 0.2 |
| Reach 1 | 435810 | 1% ACE | 74844.00 | 672.59 | 703.05 | | 703.98 | 0.001244 | 8.45 | 10534.99 | 526.54 | 0.2 |
| Reach 1 | 435043 | 1% ACE | 74844.00 | 672.92 | 702.40 | | 703.12 | 0.000674 | 7.03 | 11817.49 | 513.44 | 0.2 |
| Reach 1 | 434453 | 1% ACE | 74844.00 | 672.90 | 701.08 | | 702.28 | 0.001689 | 9.93 | 10304.26 | 657.10 | 0.3 |
| Reach 1 | 433730 | 1% ACE | 74844.00 | 668.74 | 700.47 | | 701.07 | 0.001006 | 7.16 | 14269.58 | 937.55 | 0.2 |
| Reach 1 | 433539 | 1% ACE | 74844.00 | 667.11 | 700.38 | | 700.85 | 0.000791 | 6.40 | 16156.82 | 1041.29 | 0.2 |
| Reach 1 | 433408 | 1% ACE | 74844.00 | 667.31 | 700.34 | | 700.73 | 0.000749 | 6.22 | 17383.42 | 1111.20 | 0.2 |
| Reach 1 | 433181 | 1% ACE | 86791.00 | 667.56 | 700.19 | | 700.53 | 0.000717 | 5.98 | 23131.06 | 1884.53 | 0.2 |
| Reach 1 | 432987 | 1% ACE | 86791.00 | 665.50 | 699.91 | 686.97 | 700.34 | 0.000723 | 6.73 | 20950.81 | 1542.85 | 0.2 |
| Reach 1 | 432930 | | Bridge | | | | | | | | | |
| Reach 1 | 432893 | 1% ACE | 86791.00 | 665.72 | 699.66 | | 700.17 | 0.000950 | 7.65 | 19845.98 | 1626.97 | 0.2 |
| Reach 1 | 432666 | 1% ACE | 86791.00 | 664.85 | 699.28 | | 699.98 | 0.001047 | 8.41 | 18273.21 | 1533.96 | 0.2 |
| Reach 1 | 432475 | 1% ACE | 86791.00 | 664.59 | 699.28 | | 699.73 | 0.000851 | 7.07 | 21018.31 | 1563.82 | 0.2 |
| Reach 1 | 431631 | 1% ACE | 86791.00 | 663.50 | 698.71 | | 699.12 | 0.000648 | 6.09 | 19799.53 | 1149.50 | 0.2 |
| Reach 1 | 430804 | 1% ACE | 86791.00 | 662.05 | 698.03 | | 698.58 | 0.000627 | 6.69 | 17626.24 | 976.99 | 0.2 |
| Reach 1 | 429757 | 1% ACE | 86791.00 | 659.79 | 697.35 | | 697.94 | 0.000607 | 6.50 | 16411.47 | 946.75 | 0.2 |
| Reach 1 | 428966 | 1% ACE | 86791.00 | 660.22 | 696.67 | | 697.37 | 0.000933 | 8.13 | 17012.05 | 1091.78 | 0.2 |
| Reach 1 | 428447 | 1% ACE | 86791.00 | 655.39 | 696.31 | | 696.97 | 0.000842 | 7.91 | 17600.31 | 1104.76 | 0.2 |
| Reach 1 | 427784 | 1% ACE | 86791.00 | 657.72 | 695.61 | | 696.42 | 0.000912 | 8.09 | 15742.55 | 1354.06 | 0.2 |
| Reach 1 | 427183 | 1% ACE | 86791.00 | 658.56 | 695.14 | | 695.88 | 0.000854 | 7.81 | 17395.57 | 1465.37 | 0.2 |
| Reach 1 | 426517 | 1% ACE | 86791.00 | 658.35 | 693.57 | | 694.97 | 0.001543 | 10.35 | 13491.88 | 1726.09 | 0.3 |
| Reach 1 | 425901 | 1% ACE | 86791.00 | 658.89 | 692.66 | | 694.01 | 0.001490 | 9.78 | 11944.60 | 1823.36 | 0.3 |
| Reach 1 | 425293 | 1% ACE | 86791.00 | 657.30 | 691.32 | | 692.91 | 0.001912 | 11.13 | 11674.04 | 1309.34 | 0.3 |
| Reach 1 | 424714 | 1% ACE | 99926.00 | 656.85 | 689.55 | | 691.50 | 0.002581 | 12.30 | 11743.42 | 1014.39 | 0.4 |
| Reach 1 | 424187 | 1% ACE | 99926.00 | 655.55 | 687.40 | | 689.74 | 0.003931 | 13.70 | 11114.45 | 1727.32 | 0.4 |
| Reach 1 | 423625 | 1% ACE | 99926.00 | 653.68 | 686.08 | | 687.57 | 0.002622 | 11.43 | 14768.42 | 2343.20 | 0.3 |
| Reach 1 | 422995 | 1% ACE | 99926.00 | 651.65 | 685.66 | | 686.27 | 0.001298 | 8.21 | 21717.76 | 2895.79 | 0.2 |
| Reach 1 | 422251 | 1% ACE | 99926.00 | 651.19 | 683.89 | | 685.01 | 0.002224 | 10.61 | 17479.55 | 2623.14 | 0.3 |
| Reach 1 | 421444 | 1% ACE | 99926.00 | 651.00 | 681.94 | | 683.14 | 0.002420 | 11.12 | 17377.94 | 2736.33 | 0.3 |
| Reach 1 | 420481 | 1% ACE | 99926.00 | 650.01 | 679.82 | | 680.85 | 0.002270 | 10.59 | 19929.20 | 3080.70 | 0.3 |
| Reach 1 | 419470 | 1% ACE | 99926.00 | 649.95 | 677.34 | | 678.56 | 0.002379 | 10.18 | 18439.85 | 3058.46 | 0.3 |
| Reach 1 | 418854 | 1% ACE | 99926.00 | 647.17 | 673.65 | 669.51 | 675.94 | 0.006766 | 14.95 | 14866.47 | 3220.08 | 0.5 |
| Reach 1 | 418726 | 1% ACE | 99926.00 | 645.66 | 673.16 | | 674.47 | 0.004275 | 12.13 | 18134.65 | 2987.08 | 0.4 |
| Reach 1 | 418630 | 1% ACE | 99926.00 | 646.57 | 673.02 | | 673.92 | 0.002825 | 10.06 | 20290.60 | 2916.43 | 0.3 |
| Reach 1 | 418516 | 1% ACE | 99926.00 | 645.77 | 672.91 | | 673.55 | 0.002067 | 8.78 | 22416.47 | 2924.63 | 0.3 |
| Reach 1 | 418186 | 1% ACE | 99926.00 | 646.00 | 671.63 | | 672.69 | 0.003618 | 11.74 | 18578.21 | 2782.56 | 0.4 |
| Reach 1 | 417994 | 1% ACE | 99926.00 | 646.22 | 671.06 | | 671.93 | 0.003361 | 10.79 | 19101.93 | 2394.25 | 0.3 |
| Reach 1 | 417303 | 1% ACE | 99986.00 | 641.33 | 670.18 | | 670.61 | 0.000819 | 6.50 | 22003.86 | 1458.88 | 0.2 |
| Reach 1 | 415588 | 1% ACE | 99986.00 | 642.08 | 669.19 | | 669.34 | 0.000576 | 4.31 | 36540.39 | 3494.53 | 0.1 |
| Reach 1 | 413959 | 1% ACE | 99986.00 | 639.83 | 668.36 | | 668.52 | 0.000467 | 4.23 | 35303.62 | 2983.66 | 0.1 |
| Reach 1 | 412994 | 1% ACE | 99986.00 | 638.91 | 668.04 | | 668.17 | 0.000370 | 3.62 | 38670.32 | 3239.86 | 0.1 |
| Reach 1 | 412056 | 1% ACE | 99986.00 | 638.83 | 667.80 | | 667.88 | 0.000269 | 3.10 | 46699.70 | 3143.43 | 0.1 |
| Reach 1 | 411408 | 1% ACE | 99986.00 | 637.92 | 667.67 | | 667.77 | 0.000315 | 3.42 | 44141.79 | 2987.15 | 0.1 |
| Reach 1 | 410660 | 1% ACE | 99986.00 | 634.42 | 667.29 | | 667.50 | 0.000395 | 5.15 | 35082.88 | 2425.33 | 0.1 |
| Reach 1 | 409107 | 1% ACE | 99986.00 | 633.83 | 666.16 | | 666.68 | 0.000548 | 6.73 | 22106.07 | 1237.07 | 0.2 |
| Reach 1 | 408599 | 1% ACE | 99986.00 | 631.17 | 666.00 | | 666.38 | 0.000494 | 5.43 | 22324.77 | 972.68 | 0.1 |
| Reach 1 | 408038 | 1% ACE | 99986.00 | 623.97 | 665.78 | | 666.14 | 0.000379 | 4.90 | 21923.51 | 800.76 | 0.1 |
| Reach 1 | 407323 | 1% ACE | 99986.00 | 625.42 | 662.33 | | 664.91 | 0.002816 | 14.57 | 9429.65 | 497.60 | 0.4 |
| Reach 1 | 406437 | 1% ACE | 99986.00 | 626.75 | 661.14 | | 662.21 | 0.001111 | 8.67 | 13701.45 | 733.70 | 0.2 |
| Reach 1 | 405800 | 1% ACE | 99986.00 | 625.19 | 661.04 | | 661.51 | 0.000414 | 5.60 | 19732.68 | 886.29 | 0.1 |
| Reach 1 | 405065 | 1% ACE | 99986.00 | 623.87 | 659.43 | | 660.82 | 0.002263 | 10.91 | 12846.01 | 878.94 | 0.3 |
| Reach 1 | 404559 | 1% ACE | 99986.00 | 624.37 | 658.99 | | 659.84 | 0.001392 | 8.88 | 15229.21 | 1004.11 | 0.2 |
| Reach 1 | 403683 | 1% ACE | 99986.00 | 622.00 | 658.45 | | 659.06 | 0.000544 | 6.69 | 18975.00 | 946.22 | 0.2 |
| Reach 1 | 403073 | 1% ACE | 99986.00 | 622.00 | 657.82 | | 658.60 | 0.000993 | 7.72 | 17770.07 | 1259.70 | 0.2 |
| Reach 1 | 402516 | 1% ACE | 99986.00 | 620.02 | 656.92 | | 657.98 | 0.001147 | 8.50 | 13724.62 | 852.64 | 0.2 |
| Reach 1 | 402110 | 1% ACE | 99986.00 | 620.86 | 656.77 | | 657.58 | 0.000595 | 7.58 | 17020.93 | 1085.75 | 0.2 |
| Reach 1 | 401658 | 1% ACE | 99986.00 | 617.34 | 656.80 | | 657.19 | 0.000548 | 5.88 | 23325.47 | 2225.77 | 0.1 |
| Reach 1 | 400921 | 1% ACE | 99986.00 | 618.50 | 654.83 | | 656.36 | 0.002107 | 11.35 | 16223.88 | 2700.76 | 0.3 |
| Reach 1 | 399722 | 1% ACE | 100009.00 | 614.28 | 653.98 | | 654.56 | 0.000718 | 6.73 | 23307.04 | 2741.70 | 0.2 |
| Reach 1 | 398748 | 1% ACE | 100009.00 | 610.94 | 652.50 | | 653.56 | 0.001221 | 8.60 | 15688.75 | 2166.98 | 0.2 |
| Reach 1 | 398061 | 1% ACE | 100009.00 | 612.67 | 651.63 | | 652.62 | 0.001446 | 8.88 | 17301.69 | 1963.04 | 0.2 |
| Reach 1 | 397096 | 1% ACE | 100009.00 | 611.67 | 650.05 | | 651.19 | 0.001564 | 9.29 | 17392.15 | 2784.85 | 0.3 |
| Reach 1 | 396117 | 1% ACE | 100009.00 | 612.77 | 648.24 | | 649.48 | 0.001924 | 10.12 | 16344.35 | 2012.64 | 0.3 |
| Reach 1 | 395546 | 1% ACE | 99891.00 | 612.04 | 644.73 | 637.89 | 647.69 | 0.001324 | 14.88 | 10344.33 | 1851.83 | 0.5 |
| Reach 1 | 393340 | 1% ACE | 99891.00 | 611.70 | 642.25 | 001.09 | 645.00 | 0.004710 | 14.86 | 9204.11 | 1083.55 | 0.4 |

HEC-RAS Plan: Plan 08 River: Cibolo Creek Reach: Reach 1 Profile: 1% ACE (Continued)

| Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|---------|-----------|---------|----------|-----------|-----------|-----------|-----------|------------|----------|-----------|-----------|--------------|
| | | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Reach 1 | 394251 | 1% ACE | 99891.00 | 609.16 | 640.69 | | 642.38 | 0.002586 | 10.67 | 10801.75 | 896.97 | 0.38 |
| Reach 1 | 393283 | 1% ACE | 99891.00 | 605.09 | 640.57 | | 640.89 | 0.000407 | 4.71 | 24071.05 | 1971.50 | 0.15 |
| Reach 1 | 392124 | 1% ACE | 99891.00 | 603.00 | 639.29 | | 640.09 | 0.000925 | 7.32 | 16874.11 | 2662.65 | 0.23 |
| Reach 1 | 391531 | 1% ACE | 99891.00 | 600.99 | 638.24 | | 639.36 | 0.001235 | 8.73 | 14879.74 | 3221.31 | 0.29 |
| Reach 1 | 390995 | 1% ACE | 99891.00 | 601.37 | 637.85 | | 638.68 | 0.000852 | 7.90 | 19133.87 | 2997.43 | 0.24 |
| Reach 1 | 390516 | 1% ACE | 99891.00 | 597.90 | 637.61 | | 638.09 | 0.000859 | 7.02 | 27225.53 | 3852.98 | 0.24 |
| Reach 1 | 390125 | 1% ACE | 99891.00 | 597.14 | 637.67 | | 637.80 | 0.000145 | 3.46 | 49860.83 | 4814.63 | 0.10 |
| Reach 1 | 388545 | 1% ACE | 99891.00 | 596.19 | 637.17 | | 637.44 | 0.000352 | 4.56 | 36416.35 | 5373.90 | 0.14 |
| Reach 1 | 387329 | 1% ACE | 99891.00 | 597.51 | 636.48 | | 636.84 | 0.000718 | 5.65 | 31583.87 | 4631.85 | 0.20 |
| Reach 1 | 386808 | 1% ACE | 99891.00 | 600.00 | 635.44 | | 636.25 | 0.001411 | 8.97 | 26523.83 | 5095.13 | 0.28 |
| Reach 1 | 386042 | 1% ACE | 99891.00 | 600.00 | 635.30 | | 635.61 | 0.000271 | 4.91 | 37662.01 | 6497.65 | 0.17 |
| Reach 1 | 384847 | 1% ACE | 99891.00 | 594.65 | 633.95 | 617.85 | 634.89 | 0.000901 | 9.09 | 27736.11 | 6078.30 | 0.28 |

FOR PERMIT PURPOSES ONLY

Part III – Attachment C2 – Flood Control Analysis Beck Landfill, Permit No. MSW-1848A

BECK LANDFILL APPENDIX C2-C FEMA Correspondence



Beck Landfill Revised (9/23) Part III-Attachment C2

Civil & Environmental Consultants, Inc.

C2-6



FEMA PRODUCTION AND TECHNICAL SERVICES CONTRACTOR

July 18, 2023

Adam W. Mehevec, P.E. Civil and Environmental Consultants, Inc. 3711 South Mopac Expressway Building 1, Suite 550 Austin, TX 78745 IN REPLY REFER TO: Case No.: 22-06-2567P Communities: City of Schertz and Unincorporated Areas of Bexar County, Texas Community Nos.: 480269 and 480035

316-AD

Dear Adam Mehevec:

This is in regard to your request dated August 5, 2022, that the Department of Homeland Security's Federal Emergency Management Agency (FEMA) issue a revision to the Flood Insurance Rate Map (FIRM) for the above-referenced communities. Pertinent information about the request is listed below.

Identifier:

Flooding Source:

FIRM Panel Affected:

48187C0220F and 48029C0295F

Beck Landfill

Cibolo Creek

The data required to complete our review, which must be submitted within 90 days of the date of this letter, are listed on the attached summary.

If we do not receive the required data within 90 days, we will suspend our processing of your request. Any data submitted after 90 days will be treated as an original submittal and will be subject to all submittal/payment procedures.

FEMA receives a very large volume of requests and cannot maintain inactive requests for an indefinite period of time. Therefore, we are unable to grant extensions for the submission of required data/fee for revision requests. If a requester is informed by letter that additional data are required to complete our review of a request, the data **must** be submitted within 90 days of the date of the letter. Any fees already paid will be forfeited if the requested data are not received within 90 days.

If you have general questions about your request, FEMA policy, or the National Flood Insurance Program (NFIP), please contact the FEMA Mapping and Insurance eXchange (FMIX), toll free, at 1-877-FEMA MAP (1-877-336-2627). If you have specific questions concerning your request, please contact your case reviewer, M. Tariq Makhdoom, Ph.D., CFM, by e-mail at TMakhdoom@taylorengineering.com or by telephone at (904) 553-5760, or the Revisions Coordinator for your state, Sushban Shrestha, P.E., CFM, by e-mail at <u>sushban.shrestha@aecom.com</u> or by telephone at (682) 316-7670.

Sincerely,

Benjamin Kaiser, P.E., CFM Revisions Manager Compass PTS JV

Attachments: Summary of Additional Data

cc: Doug Letbetter, CFM Floodplain Administrator City of Schertz, Texas

> Robert Brach, P.E., CFM Development Services Engineer / Floodplain Administrator Bexar County



FEMA PRODUCTION AND TECHNICAL SERVICES CONTRACTOR

Summary of Additional Data Required to Support a Letter of Map Revision (LOMR)

Case No.: 22-06-2567P

Requester: Adam W. Mehevec, P.E.

Communities: City of Schertz, and Unincorporated Areas of Bexar County, Texas Community Nos.: 480269 and 480035

The issues listed below must be addressed before we can continue the review of your request.

 Subparagraph 65.6(a)(2) of the National Flood Insurance Program (NFIP) regulations states that to avoid discontinuities between revised and unrevised flood data, hydraulic analyses must have a logical transition between revised elevations of the 1-percent-annual chance (base) flood and those developed previously for areas not affected by the revision. Therefore, revised base flood elevation (BFE) must tie-in to the effective BFE within 0.5 feet, or within 0.0 feet if practical, at the upstream and downstream ends of the revised reach. The graphical tie-in between the post-project and effective delineations of the base floodplain, 0.2-percent-annual-chance floodplain and regulatory floodway can be shown at, or just upstream and downstream of, the BFE tie-in locations at both ends.

Our review of the submitted post-project conditions model revealed no BFE tie-in at the upstream end. The submitted topographic work map showed limits of the revised reach at the upstream end at Cross Section 446236, which is located at the downstream side of FM 78 Bridge. However, there was no BFE tie-in within 0.5 feet until Cross Section 454165.

A revised post-project conditions hydraulic analysis was submitted on July 10, 2023, in response to our e-mail of July 7, 2023. Our review of the submitted revised post-project conditions model indicates that:

- a. The limit of the revised reach at the upstream end is shown at Cross Section 446478 which is located just upstream of FM 78 Bridge, where the difference between post-project and effective BFE is 0.49 feet. However, BFE difference between the post-project and effective BFEs are 0.53 and 0.93 feet, respectively, at the upstream cross sections, which are located just downstream and upstream of the Southern Pacific Railroad, respectively.
- b. The revised hydraulic analysis used effective topography for all cross sections upstream of Cross Section 445335.
- c. The revised hydraulic analysis used higher flow compared to the effective flows at all cross sections except two downstream cross sections where the revised analysis used lower flows compared to the effective.

Please extend the limit of the revised reach to Cross Section 454165, where there is a BFE tie-in as indicated above and submit revised post-project conditions hydraulic analyses or provide justification for using lower or higher flows compared to the effective flows without providing any supporting hydrologic analysis and use of old effective topographic data upstream of Cross Section 445335 instead of new topography.

- 2. Please submit a revised copy of the topographic work map and annotated Flood Insurance Rate Map (FIRM). Please also provide a copy of the Geographic Information System (GIS) data that reflects the revised topographic work map.
- 3. Please note that the submitted copy of the draft property owner notification will be reviewed after all technical comments have been addressed. Please do not distribute the final notification letters until we have approved the revised draft notice.

Please upload the required data using the Online LOMC website at https://hazards.fema.gov/femaportal/onlinelomc/signin.

For identification purposes, please include the case number referenced above on all correspondence.

Mehevec, Adam

| From: | Tariq Makhdoom <tmakhdoom@taylorengineering.com></tmakhdoom@taylorengineering.com> |
|----------|---|
| Sent: | Friday, June 2, 2023 4:00 PM |
| То: | Mehevec, Adam |
| Cc: | Lokulutu, Bosulu; Shrestha, Sushban |
| Subject: | Additional Data Received for the City of Schertz and Bexar County, Texas, LOMR Case |
| | Number (22-06-2567P) – Response Requested |

Dear Adam Mehevec:

We have received your submittal of additional data for Case Number (22-06- 2567P). This case number is for a request that the Department of Homeland Security's Federal Emergency Management Agency (FEMA) issue a revision to the Flood Insurance Rate Map (FIRM) for the City of Schertz and Bexar County, Texas. This e-mail is being sent to officially acknowledge the receipt of your additional data for the above-referenced case number and replaces the paper copy acknowledgement letters previously issued by FEMA. We ask that you please respond directly to this e-mail to verify that it has been received.

We are reviewing your submitted data and will contact you if additional information is required to process your request.

If additional information is not required, we will issue a final letter of determination within 90 days of receiving your submittal.

If you have general questions about your request, FEMA policy, or the National Flood Insurance Program, please call the FEMA Mapping and Insurance eXchange (FMIX), toll free, at 1-877-FEMA MAP (1-877-336-2627). If you have specific questions concerning your request, please contact the case reviewer using the information listed below, or the Revisions Coordinator for your request, Mr. Sushban Shrestha, P.E., CFM, by e-mail at <u>sushban.shrestha@aecom.com</u> or by telephone at (682) 316-7670.

Please be assured we will do our best to respond to all inquiries in a timely manner.

Thank you,

M. Tariq Makhdoom, Ph.D., CFM Taylor Engineering, Inc., a member of Compass PTS JV 10199 Southside Blvd., Suite 310, Jacksonville, FL 32256 Main: 904-731-7040 | Direct: 904 -553 - 5760 TMakhdoom@Taylorengineering.Com

| 5. Basis for Request and Type of Revision: | |
|--|--|
| a. The basis for this revision request is (check all that apply) | |
| Physical Change Improved Methodology/Data | Regulatory Floodway Revision 🗌 Base Map Changes |
| Coastal Analysis Hydraulic Analysis | X Hydrologic Analysis Corrections |
| Weir-Dam Changes Levee Certification | Alluvial Fan Analysis Natural Changes |
| X New Topographic Data Other (Attach Description) | |
| Note: A photograph and narrative description of the area of conc | ern is not required, but is very helpful during review. |
| b. The area of revision encompasses the following structures (cr | neck all that apply) |
| Structures: Channelization Levee/Floodwall | Bridge/Culvert |
| Dam Fill | Other (Attach Description) |
| 6. Documentation of ESA compliance is submitted (required to information. | o initiate CLOMR review). Please refer to the instructions for more |
| C. REVI | EW FEE |
| Has the review fee for the appropriate request category been included | ? X Yes Fee amount: \$ 8,000 |
| | No, Attach Explanation |
| Please see the DHS-FEMA Web site at <u>http://www.fema.ge</u> | |
| <u>map-related-fees</u> for Fee Amounts and Exemption | |
| D. SIGN | |
| 1. REQUESTOR'S SIGNATURE | |
| All documents submitted in support of this request are correct to the I punishable by fine or imprisonment under Title 18 of the United States (| best of my knowledge. I understand that any false statement may be Code, Section 1001. |
| Name: Adam Mehevec | Company: Civil and Environmental Consultants, Inc. |
| Mailing Address: | Daytime Telephone: 512-225-8103 Fax No.: 512-329-0096 |
| 1221 S. Mopac Expressway, Suite 350 | E-mail Address: amehevec@cecinc.com |
| Austin, TX 78746 | Date: MAY, 2023 |
| Signature of Requestor (required): | |
| 2. COMMUNITY CONCURRENCE | |
| (LOMR) or conditional LOMR request. Based upon the community's review, we community floodplain management requirements, including the requirements for State, and local permits have been, or in the case of a conditional LOMR, will Endangered Species Act (ESA) compliance to FEMA prior to FEMA's review compliance with Sections 9 and 10 of the ESA has been achieved independent Federal or State agencies, documentation from the agency showing its completermined that the land and any existing or proposed structures to be removed 44CFR 65.2(c), and that we have available upon request by FEMA, all analyses | cknowledge that we have received and reviewed this Letter of Map Revision e find the completed or proposed project meets or is designed to meet all of the or when fill is placed in the regulatory floodway, and that all necessary Federal, I be obtained. For Conditional LOMR requests, the applicant has documented of the Conditional LOMR application. For LOMR requests, I acknowledge that titly of FEMA's process. For actions authorized, funded, or being carried out by iance with Section 7(a)(2) of the ESA will be submitted. In addition, we have ved from the SFHA are or will be reasonably safe from flooding as defined in and documentation used to make this determination. |
| Community Official's Name and Title: Robert Brach, P.E., CFM | |
| Mailing Address: 1948 Probandt Street | Community Name: Bexar County |
| San Antonio, TX 78214 | Daytime Telephone: 210-335-2011 Fax No.: |
| 71.57 | E-mail Address: RBrach@bexar.org |
| Community Official's Signature (required): | Date: 5/12/23 |

3. CERTIFICATION BY REGISTERED PROFESSIONAL ENGINEER AND/OR LAND SURVEYOR

This certification is to be signed and sealed by a licensed land surveyor, registered professional engineer, or architect authorized by law to certify elevation information data, hydrologic and hydraulic analysis, and any other supporting information as per NFIP regulations paragraph 65.2(b) and as described in the MT-2 Forms Instructions. All documents submitted in support of this request are correct to the best of my knowledge. I understand that any false statement may be punishable by fine or imprisonment under Title 18 of the United States Code, Section 1001.

| Certifier's Name: Adam W. Mehev | rec, PE | License No.: 84736 | Expiration Date: 12/31/2023 |
|---------------------------------|---------------------------|---|-----------------------------|
| Company Name: Civil and Environ | nmental Consultants, Inc. | Mailing Address: 1221 S. Mopac Expressway, | |
| Telephone No.: 512-225-8103 | Fax No.: 512-329-0096 | Suite 350 Austin, TX 78746 | |
| E-mail Address: amehevec@ceci | inc.com | | |
| Signature: | h 14- | | Date: 5-7-2023 |

Ensure the forms that are appropriate to your revision request are included in your submittal.

| Form Name and (Number) | Required if | A E OF TEL |
|---|---|-----------------|
| X Riverine Hydrology and Hydraulics Form (Form 2) | New or revised discharges or water- surface elevations | |
| Riverine Structures Form (Form 3) | Channel is modified, addition/revision of bridge/culverts, addition/revision of levee/floodwall, addition/revision of dam | ADAM W. MEHEVEC |
| Coastal Analysis Form (Form 4) | New or revised coastal elevations | 1 MONALE SALAS |
| Coastal Structures Form (Form 5) | Addition/revision of coastal structure | 5-7-2923 |
| Alluvial Fan Flooding Form (Form 6) | Flood control measures on alluvial fans | Seal (Optional) |

LETTER OF MAP REVISION REQUEST FOR CIBOLO CREEK FIRM PANELS 48029C0295F AND 48187C0210F



COMPANIES BECK LANDFILL 550 FARM TO MARKET ROAD 78 SCHERTZ, GUADALUPE COUNTY, TEXAS

Prepared By:

CIVIL & ENVIRONMENTAL CONSULTANTS, INC. AUSTIN, TEXAS (TEXAS P.E. FIRM F-38)

CEC Project 311-653

JUNE 2022





Civil & Environmental Consultants, Inc.

DEPARTMENT OF HOMELAND SECURITY Federal Emergency Management Agency OVERVIEW & CONCURRENCE FORM

OMB Control Number: 1660-0016 Expiration: 1/31/2024

PAPERWORK BURDEN DISCLOSURE NOTICE

Public reporting burden for this form is estimated to average 1 hours per response. The burden estimate includes the time for reviewing instructions, searching existing data sources, gathering and maintaining the needed data, and completing, reviewing, and submitting the form. You are not required to respond to this collection of information unless it displays a valid OMB control number. Send comments regarding the accuracy of the burden estimate and any suggestions for reducing this burden to: Information Collections Management, Department of Homeland Security, Federal Emergency Management Agency, 500 C Street, SW, Washington, DC 20472, Paperwork Reduction Project (1660-0016). Submission of the form is required to obtain or retain benefits under the National Flood Insurance Program. **Please do not send your completed survey to the above address**.

PRIVACY ACT STATEMENT

AUTHORITY: The National Flood Insurance Act of 1968, Public Law 90-448, as amended by the Flood Disaster Protection Act of 1973, Public Law 93-234.

PRINCIPAL PURPOSE(S): This information is being collected for the purpose of determining an applicant's eligibility to request changes to National Flood Insurance Program (NFIP) Flood Insurance Rate Maps (FIRM).

ROUTINE USE(S): The information on this form may be disclosed as generally permitted under 5 U.S.C § 552a(b) of the Privacy Act of 1974, as amended. This includes using this information as necessary and authorized by the routine uses published in DHS/FEMA/NFIP/LOMA-1 National Flood Insurance Program (NFIP); Letter of Map Amendment (LOMA) February 15, 2006, 71 FR 7990.

DISCLOSURE: The disclosure of information on this form is voluntary; however, failure to provide the information requested may delay or prevent FEMA from processing a determination regarding a requested change to a (NFIP) Flood Insurance Rate Maps (FIRM).

A. REQUESTED RESPONSE FROM DHS-FEMA

This request is for a (check one):

CLOMR: A letter from DHS-FEMA commenting on whether a proposed project, if built as proposed, would justify a map

proposed hydrology changes (See 44 CFR Ch. 1, Parts 60, 65 & 72). All CLOMRs require documentation of compliance with the Endangered Species Act. Refer to the Instructions for details.

LOMR: A letter from DHS-FEMA officially revising the current NFIP map to show the changes to floodplains, regulatory floodway or flood elevations. (See 44 CFR Ch. 1, Parts 60, 65 & 72).

| | B. OVERVIEW | | | | |
|---------------------|---|-------------|----------------|--------------|----------------|
| 1. The NFIP map p | anel(s) affected for all impacted communities is (are): | | | | |
| Community No. | Community Name | State | Map No. | Panel No. | Effective Date |
| 480269 | City of Schertz; Guadalupe County | ТХ | 48187C | 0220F | 11/2/07 |
| 480035 | Unincorporated Bexar County | тх | 48029C | 0295F | 9/29/10 |
| | | | | | |
| 2. a. Flooding Sour | rce: Cibolo Creek | | | | |
| b. Types of Floo | ding: 🔀 Riverine 🗌 Coastal 🔲 Shalle | ow Floodi | ng (e.g., Zone | s AO and AH) | |
| | Alluvial Fan Lakes Other | r (Attach E | Description) | | |
| 3. Project Name/Id | entifier: Beck Landfill | | | | |
| 4. FEMA zone desi | gnations (choices: A, AH, AO, A1-A30, A99, AE, AR, V, V1-V30, | VE, B, C, | D, X) | | |
| a. Effective: AE | | | | | |
| b. Revised: AE | | | | | |



COUNTY OF BEXAR

PUBLIC WORKS DEPARTMENT

1948 Probandt San Antonio, Texas 78214 Main 210-335-6700

To: Civil & Environmental Consultants, Inc. 10101 Reunion Place, Suite 400 San Antonio, TX 78216 Date: May 12, 2023

Attention: Adam W. Mehevec, P.E.

Re: Letter of Map Revision Beck Landfill – Cibolo Creek

DESCRIPTION

Attached is the Bexar County endorsed FEMA MT-2 FORMS.

WITH THE FOLLOWING EXHIBITS:

Beck Landfill - Cibolo Creek

Digital Files

Submitted 5/12/2023

Endorsed with the following exceptions:

- 1. There are increases in Water Surface Elevations greater than allowed by FEMA and Bexar County Court order due to the following:
 - a. FEMA has different flow rates and water surface elevations for both communities for the SAME creek (Cibolo Creek)
 - b. There are topography changes in Beck Landfill since the (SARA) Best Available Models were modeled.

FROM: TERRANCE JACKSON, P.E., PhD CIVIL ENGINEER (210) 335-3048



FEMA PRODUCTION AND TECHNICAL SERVICES CONTRACTOR

February 13, 2023

Adam W. Mehevec, P.E. Civil and Environmental Consultants, Inc. 3711 South Mopac Expressway Building 1, Suite 550 Austin, TX 78745 IN REPLY REFER TO: Case No.: 22-06-2567P Communities: City of Schertz and Unincorporated Areas of Bexar County, Texas Community Nos.: 480269 and 480035

316-AD

Dear Adam Mehevec:

This is in regard to your request dated August 5, 2022, that the Department of Homeland Security's Federal Emergency Management Agency (FEMA) issue a revision to the Flood Insurance Rate Map (FIRM) for the above-referenced communities. Pertinent information about the request is listed below.

| Identifier: | Beck Landfill |
|----------------------|---------------|
| Flooding Source: | Cibolo Creek |
| FIRM Panel Affected: | 48187C0220F |

The data required to complete our review, which must be submitted within 90 days of the date of this letter, are listed on the attached summary.

If we do not receive the required data within 90 days, we will suspend our processing of your request. Any data submitted after 90 days will be treated as an original submittal and will be subject to all submittal/payment procedures.

FEMA receives a very large volume of requests and cannot maintain inactive requests for an indefinite period of time. Therefore, we are unable to grant extensions for the submission of required data/fee for revision requests. If a requester is informed by letter that additional data are required to complete our review of a request, the data **must** be submitted within 90 days of the date of the letter. Any fees already paid will be forfeited if the requested data are not received within 90 days.

If you have general questions about your request, FEMA policy, or the National Flood Insurance Program (NFIP), please contact the FEMA Mapping and Insurance eXchange (FMIX), toll free, at 1-877-FEMA MAP (1-877-336-2627). If you have specific questions concerning your request, please contact your case reviewer, M. Tariq Makhdoom, Ph.D., CFM, by e-mail at TMakhdoom@Taylorengineering.com or by telephone at (904) 553-5760, or the Revisions Coordinator for your state, Mr. Bosulu Lokulutu, E.I.T, CFM, by e-mail at bosulu.lokulutu@aecom.com or by telephone at (972) 735-7093.

Sincerely,

Benjamin Kaiser, P.E., CFM Revisions Manager Compass PTS JV

Attachments:

Summary of Additional Data Legal Notification Templates

cc: Dough Letbetter, CFM Floodplain Administrator City of Schertz, Texas

> Robert Brach Development Services Engineer / Floodplain Administrator Bexar County



FEMA PRODUCTION AND TECHNICAL SERVICES CONTRACTOR

Summary of Additional Data Required to Support a Letter of Map Revision (LOMR)

Case No.: 22-06-2567P

Requester: Adam W. Mehevec, P.E.

Communities: City of Schertz, and Unincorporated Areas of Bexar County, Texas Community Nos.: 480269 and 480035

The issues listed below must be addressed before we can continue the review of your request.

- 1. As indicated previously, please submit a copy of MT-2 Application/Certification Form 1, entitled "Overview and Concurrence Form," where the second signature block has been signed by a Bexar County official (preferably the Floodplain Administrator). Alternatively, please provide documentation that the corporate limits shown on the Flood Insurance Rate Map (FIRM) are not accurate and Bexar County is not actually affected by this revision. Acceptable documentation includes a current corporate limits map provided by the community along with an annexation agreement, if applicable.
- 2. As indicated by you in your e-mail dated February 3, 2023, Bexar County is withholding its concurrence because they would like you to use revised hydrology to match the National Oceanic and Atmospheric Administration (NOAA) Atlas 14 rainfall data, which would cause a significant increase in the 1-percent-annual-chance (base) flood elevation (BFE) and implementing this level of change in the BFE for just a small portion of Cibolo Creek located within Bexar County would not allow for a smooth transition back to the existing BFE at the upstream and downstream limits of study. You believe that you can work out the current Bexar County comments in the next 45 to 90 days, so you would like to request that we issue another round of comments and allow 90 days to acquire the Bexar County concurrence and adequately respond to our comment.
- 3. You have also indicated in your e-mail above, you might end up revising hydrology which would result in revised hydraulic analyses, topographic work map, and annotated FIRM. Please submit revised hydrologic and hydraulic analyses, topographic work map, and annotated FIRM, if the resolution of our comment 1 above results in revised hydrology as indicated by you.
- 4. Please provide a copy of the Geographic Information System (GIS) data that reflects the revised topographic work map.
- 5. Please submit a copy of the newspaper notice distributed by the City of Schertz and Bexar County stating their intent to revise the flood hazard information (i.e., revise or establish BFEs, the base floodplain, and regulatory floodway) along Cibolo Creek. Alternatively, please submit documentation that individual legal notices were sent to all property owners affected by any changes in the flood hazard information. Documentation of legal notice may take the form of a signed copy of the letter sent and either a mailing list or certified mailing receipts. Individual notices that are not sent on community letterhead must also include certification from the community that all affected property owners have been notified of the floodway revision. The newspaper notices or the

individual legal notices must include the extent of revision and contact information for any interested parties and must also mention the community's intent to revise the regulatory floodway. **Please submit a draft copy of the notification for verification of content, prior to publication or distribution.** One of the attached templates may be used to prepare the draft notification.

Please note that the draft property owner notification or newspaper notification will be reviewed after the hydraulic model and work map are finalized. Please do not distribute the final notification until we have approved the draft notice.

Please upload the required data using the Online LOMC website at https://hazards.fema.gov/femaportal/onlinelomc/signin.

For identification purposes, please include the case number referenced above on all correspondence.



November 30, 2022

Tariq Makhdoom Taylor Engineering, Inc. 10199 Southside Blvd., Ste.310 Jacksonville, FL 32256

Dear Mr. Makhdoom :

Subject: City of Schertz, and Unincorporated Areas of Bexar County LOMR Case No.: 22-06-2567P Community Nos.: 480269 and 480035 CEC Project 311-653

We received your comments related to LOMR Case No. 22-06-2567P on September 1, 2022 and have addressed them as follows:

- 1. From our review of the submitted annotated Flood Insurance Rate Map (FIRM), it appears that the Unincorporated Areas of Bexar County are also affected by this LOMR. Please submit a copy of MT-2 Application/Certification Form 1, entitled "Overview and Concurrence Form," where the second signature block has been signed by a Bexar County official (preferably the Floodplain Administrator). Alternatively, please provide documentation that the corporate limits shown on the FIRM are not accurate and Bexar County is not actually affected by this revision. Acceptable documentation includes a current corporate limits map provided by the community along with an annexation agreement, if applicable.
 - We contacted the floodplain administrator at Bexar County on September 4th to determine the submittal requirements necessary to obtain their concurrence. We submitted a concurrence request package on October 12th, but have not received approval from Bexar County as of this date. We will provide the requested concurrence form as soon as we receive it from Bexar County.
- 2. Our review revealed that the submittal does not include floodway analysis for the duplicate effective and as-built plan for Cibolo Creek. Please submit floodway analysis for Cibolo Creek. Please ensure that the surcharges do not exceed the 1.0-foot maximum allowed and there are no surcharges that are less than 0.0 feet. Also please ensure that the encroachment stations are located in the flood fringe, the area between the channel banks and the boundary of the base floodplain.
 - A floodway analysis is included for Cibolo Creek. The floodway is outside of the area where the updated topography has been provided, so there is no difference between the floodway for the duplicate effective and the as-built plans. The floodway was delineated between cross-sections 446236 and 433181. The largest surcharge calculated in the studied section is 0.9 feet at section 446236. The minimum surcharge calculated is 0.01 feet at

Tariq Makhdoom – Taylor Engineering, Inc. CEC Project 311-653 Page 2 November 30, 2022

section 434453. The encroachment stations do not infringe into the main channel bank area. The HEC-RAS analysis with the floodway delineation is included in the file labelled "floodway.prj".

3. The submitted topographic work map, entitled "Topographic Work Map – Beck Landfill Expansion, 600 FM 78, Schertz, Texas 78154, Guadalupe County, Texas," prepared by Civil & Environmental Consultants, Inc., certified dated June 15, 2022, does not provide some of the essential information required to complete our review of this request. Please submit a revised topographic work map, certified by a registered Professional Engineer (P.E.), which shows all applicable items listed in Section C of Application/Certification Form 2, entitled "Riverine Hydrology and Hydraulics Form," including the following information. Please ensure that there is consistency between the work map,

revised hydraulic model and the annotated FIRM.

- A revised topographic work map has been provided.
 - a. Please show the boundary delineations of the revised conditions base 0.2-percentannual- chance floodplain, and regulatory floodway. The floodplain boundaries should generally follow the proposed contours and should be delineated to the elevations calculated in the revised conditions hydraulic model. It is helpful to use different colored lines as well as line types to distinguish the boundary delineations.
 - The edge of the 0.2% annual chance floodplain is shown in brown on the topographic work map and the regulatory floodway is shown as a magenta border with cross-hatching.
 - b. Please show smooth graphical tie-ins between the revised and effective flood hazard boundary delineations at the upstream and downstream ends of the revised reach. Please ensure that the revised delineations tie-in directly to the effective delineations and that the tie-ins occur a short distance upstream of the upstream most cross section in the revised conditions hydraulic model and a short distance downstream of the downstream most cross section, where there is a base flood elevation (BFE) tie-in between the revised and effective conditions. Please label tie-in locations.
 - The 1% and 0.2% floodplains and the regulated floodway tie-ins have been shown on the revised topographic work map.
 - c. The work map does not seem to be created on the scale shown on the map. Please create the map on the scale shown on the work map and also indicate the scale (1 inch = x feet).
 - The scale bar shown on the map is correct and we have added text stating that the scale is 1 inch=300 feet, as requested.
 - d. In view of the above comment, we could not verify top widths of the base floodplain, 0.2- percent-annual-chance floodplain, and regulatory floodway, as shown on the

Tariq Makhdoom – Taylor Engineering, Inc. CEC Project 311-653 Page 3 November 30, 2022

above-referenced work map. We could also not verify reach lengths between the revised cross section as shown on the above referenced work map.

- Comment acknowledged
- 4. Please provide a copy of the Geographic Information System (GIS) data that reflects the revised topographic work map. Please ensure the digital data are spatially referenced and cite what projection (coordinate system, example: Universal Transverse Mercator [UTM]/State Plane) was used, so that the data may be used for accurate mapping. The important data to show on the digital work map are the contour information, the stream centerline, the cross section lines, the road crossings and hydraulic structures, the preliminary and proposed flood hazard delineations, and the tie-in locations. Everything should be clearly labeled, and all information should be contained within the drawing and not externally referenced.

The submitted digital data must be spatially referenced and include what projection (coordinate system, e.g., UTM/State Plane) was used. The submitted digital data do not contain a projection and cannot be used for accurate mapping. Please resubmit Computed-Aided Design (CAD)/GIS data that are correctly referenced and projected.

- The topographic work map is spatially referenced to the TX83-SCF: NAD83 Texas State Planes, South Central Zone and the units are US foot. This reference information also appears on the drawing.
- 5. Based on any changes to the work map due to the resolution of the items at comment 4 above, please submit an updated annotated FIRM that shows the revised boundary delineations of the 1-percent- annual-chance (base) floodplain, 0.2-percent-annual-chance floodplain, and regulatory floodway as shown on the updated work map and how they tie-in to the boundary delineations shown on the effective FIRM at the downstream and upstream ends of the revised reach. Please use different colors to differentiate the proposed and effective boundary delineations. Also, please show the title block of the effective FIRM on the annotated FIRM.

• Revised annotated FIRM panels 48187C0220F and 48029C0295F have been provided.

6. Please submit a copy of the newspaper notice distributed by the City of Schertz and Bexar County stating their intent to revise the flood hazard information (i.e., revise or establish base flood elevations [BFEs], the base floodplain, and regulatory floodway) along Cibolo Creek. Alternatively, please submit documentation that individual legal notices were sent to all the property owners affected by any changes in the flood hazard information. Documentation of legal notice may take the form of a signed copy of the letter sent and either a mailing list or certified mailing receipts. Individual notices that are not sent on community letterhead must also include certification from the community that all affected property owners have been notified of the floodway revision. The newspaper notices or the individual legal notices must include the extent of revision and contact information for any interested parties and must also mention the community's intent to revise the regulatory floodway. **Please submit a draft copy of the notification for verification of content, prior to publication or distribution.** One of the attached templates may be used to prepare the draft notification.

Tariq Makhdoom – Taylor Engineering, Inc. CEC Project 311-653 Page 4 November 30, 2022

• Draft templates of both the newspaper notice and individual legal notice letter are attached. Based on final input from the community(s), we will determine whether to publish the newspaper notice or mail the individual legal notices.

If you have any questions or comments, please contact me directly at <u>amehevec@cecinc.com</u> or at 512-329-0006.

Sincerely,

CIVIL & ENVIRONMENTAL CONSULTANTS, INC.

Adam Mehevec, PE Principal

Enclosures:

cc:



| | | | ations: User De | | | | | | | | | | |
|--------------|----------|-----------|-----------------|-------------------|----------------|----------------|-----------|----------------|---------------------|-----------------|---------------------|-----------------|--------------|
| River | Reach | River Sta | Profile | Q Total | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
| Cibolo Creek | Reach 1 | 446236 | 1% ACE | (cfs) 83554.00 | (ft) 686.27 | (ft) 716.12 | (ft) | (ft) 718.00 | (ft/ft) 0.002356 | (ft/s) 12.35 | (sq ft) 12083.89 | (ft) 1951.03 | 0.40 |
| Cibolo Creek | Reach 1 | 446236 | 0.2% ACE | 99095.00 | 686.27 | 718.06 | | 710.00 | 0.002350 | 12.33 | 16415.88 | 2318.70 | 0.40 |
| OIDOID OFCCR | Redon i | 440200 | 0.2 /0 HOL | 00000.00 | 000.27 | 710.00 | | 113.10 | 0.002104 | 12.00 | 10410.00 | 2010.70 | 0.00 |
| Cibolo Creek | Reach 1 | 446037 | 1% ACE | 83554.00 | 685.26 | 716.14 | | 717.43 | 0.001662 | 10.38 | 14568.45 | 2171.55 | 0.34 |
| Cibolo Creek | Reach 1 | 446037 | 0.2% ACE | 99095.00 | 685.26 | 718.08 | | 719.24 | 0.001500 | 10.30 | 18941.32 | 2313.16 | 0.32 |
| | | | | | | | | | | | | | |
| Cibolo Creek | Reach 1 | 445573 | 1% ACE | 83554.00 | 683.27 | 715.47 | | 716.64 | 0.001635 | 10.24 | 13853.91 | 1272.36 | 0.34 |
| Cibolo Creek | Reach 1 | 445573 | 0.2% ACE | 99095.00 | 683.27 | 717.33 | | 718.52 | 0.001615 | 10.61 | 16286.39 | 1335.62 | 0.34 |
| Cibolo Creek | Reach 1 | 445235 | 1% ACE | 74844.00 | 683.27 | 715.46 | | 716.09 | 0.000839 | 7.38 | 14446.55 | 819.21 | 0.24 |
| Cibolo Creek | Reach 1 | 445235 | 0.2% ACE | 81545.00 | 683.27 | 717.36 | | 717.98 | 0.000761 | 7.33 | 16055.63 | 866.11 | 0.23 |
| | | | | | | | | | | | | | |
| Cibolo Creek | Reach 1 | 444777 | 1% ACE | 74844.00 | 683.27 | 714.34 | | 715.55 | 0.001357 | 9.41 | 9324.66 | 418.29 | 0.31 |
| Cibolo Creek | Reach 1 | 444777 | 0.2% ACE | 81545.00 | 683.27 | 716.25 | | 717.47 | 0.001272 | 9.50 | 10142.33 | 431.62 | 0.30 |
| | | | | | | | | | | | | | |
| Cibolo Creek | Reach 1 | 444240 | 1% ACE | 74844.00 | 683.14 | 712.59 | | 714.56 | 0.002177 | 11.70 | 7112.57 | 303.76 | 0.39 |
| Cibolo Creek | Reach 1 | 444240 | 0.2% ACE | 81545.00 | 683.14 | 714.51 | | 716.53 | 0.002059 | 11.88 | 7703.66 | 317.53 | 0.38 |
| Cibolo Creek | Reach 1 | 443555 | 1% ACE | 74844.00 | 682.52 | 712.24 | | 713.19 | 0.001159 | 8.05 | 9943.71 | 424.81 | 0.28 |
| Cibolo Creek | Reach 1 | 443555 | 0.2% ACE | 81545.00 | 682.52 | 712.24 | | 715.19 | 0.001159 | 8.13 | 10812.30 | 424.61 | 0.28 |
| | | | | 2.2.2.00 | | | | | | 2.10 | | | 5.21 |
| Cibolo Creek | Reach 1 | 442891 | 1% ACE | 74844.00 | 679.79 | 711.58 | | 712.49 | 0.000944 | 7.77 | 10195.40 | 409.13 | 0.25 |
| Cibolo Creek | Reach 1 | 442891 | 0.2% ACE | 81545.00 | 679.79 | 713.64 | | 714.57 | 0.000884 | 7.87 | 11058.46 | 425.44 | 0.25 |
| | | | | | | | | | | | | | |
| Cibolo Creek | Reach 1 | 442214 | 1% ACE | 74844.00 | 678.90 | 709.72 | | 711.43 | 0.002485 | 12.16 | 8711.94 | 548.33 | 0.40 |
| Cibolo Creek | Reach 1 | 442214 | 0.2% ACE | 81545.00 | 678.90 | 712.18 | | 713.66 | 0.001982 | 11.48 | 10069.67 | 557.25 | 0.37 |
| Cibolo Creek | Reach 1 | 441476 | 1% ACE | 74844.00 | 678.52 | 708.12 | | 709.76 | 0.001991 | 10.59 | 7947.43 | 421.93 | 0.36 |
| Cibolo Creek | Reach 1 | 441476 | 0.2% ACE | 81545.00 | 678.52 | 710.80 | | 712.32 | 0.001646 | 10.35 | 9107.17 | 446.61 | 0.33 |
| | riodon r | | 0.2.777102 | 01010.00 | 010.02 | 110.00 | | 112.02 | 0.001010 | 10.20 | 010111 | 110.01 | 0.00 |
| Cibolo Creek | Reach 1 | 440762 | 1% ACE | 74844.00 | 677.76 | 705.81 | | 707.89 | 0.002707 | 11.80 | 6709.83 | 304.53 | 0.42 |
| Cibolo Creek | Reach 1 | 440762 | 0.2% ACE | 81545.00 | 677.76 | 708.85 | | 710.78 | 0.002152 | 11.38 | 7655.50 | 318.80 | 0.38 |
| | | | | | | | | | | | | | |
| Cibolo Creek | Reach 1 | 439971 | 1% ACE | 74844.00 | 677.96 | 705.51 | | 705.71 | 0.000410 | 4.27 | 22216.60 | 1144.96 | 0.16 |
| Cibolo Creek | Reach 1 | 439971 | 0.2% ACE | 81545.00 | 677.96 | 708.70 | | 708.87 | 0.000299 | 3.99 | 25887.58 | 1156.97 | 0.14 |
| Cibolo Creek | Reach 1 | 438740 | 1% ACE | 74844.00 | 675.84 | 705.30 | | 705.41 | 0.000223 | 3.38 | 33040.49 | 1844.11 | 0.12 |
| Cibolo Creek | Reach 1 | 438740 | 0.2% ACE | 81545.00 | 675.84 | 705.50 | | 705.41 | 0.000223 | 3.30 | 39078.01 | 1860.54 | 0.12 |
| | | | 0.2.777102 | 01010.00 | 010.01 | 100.00 | | 100.00 | 0.000100 | 0.01 | 00070.01 | 1000.01 | 0.10 |
| Cibolo Creek | Reach 1 | 437996 | 1% ACE | 74844.00 | 674.71 | 705.21 | | 705.29 | 0.000189 | 3.18 | 35176.72 | 1824.69 | 0.11 |
| Cibolo Creek | Reach 1 | 437996 | 0.2% ACE | 81545.00 | 674.71 | 708.50 | | 708.57 | 0.000136 | 2.92 | 41200.72 | 1839.25 | 0.10 |
| | | | | | | | | | | | | | |
| Cibolo Creek | Reach 1 | 437265 | 1% ACE | 74844.00 | 674.32 | 705.03 | | 705.18 | 0.000290 | 3.98 | 27754.92 | 1486.97 | 0.14 |
| Cibolo Creek | Reach 1 | 437265 | 0.2% ACE | 81545.00 | 674.32 | 708.36 | | 708.49 | 0.000207 | 3.65 | 32756.35 | 1513.77 | 0.12 |
| Cibolo Creek | Reach 1 | 436536 | 1% ACE | 74844.00 | 673.98 | 704.27 | | 704.82 | 0.000810 | 6.89 | 15281.89 | 921.79 | 0.23 |
| Cibolo Creek | Reach 1 | 436536 | 0.2% ACE | 81545.00 | 673.98 | 707.80 | | 708.23 | 0.000557 | 6.20 | 18580.31 | 943.67 | 0.20 |
| | | | | | | | | | | | | | |
| Cibolo Creek | Reach 1 | 435810 | 1% ACE | 74844.00 | 672.59 | 703.05 | | 703.98 | 0.001244 | 8.45 | 10535.21 | 526.54 | 0.29 |
| Cibolo Creek | Reach 1 | 435810 | 0.2% ACE | 81545.00 | 672.59 | 706.85 | | 707.63 | 0.000882 | 7.77 | 12568.74 | 544.12 | 0.25 |
| | | | | | | | | | | | | | |
| Cibolo Creek | Reach 1 | 435043 | 1% ACE | 74844.00 | 672.92 | 702.40 | | 703.12 | 0.000674 | 7.03 | 11817.77 | 513.44 | 0.24 |
| Cibolo Creek | Reach 1 | 435043 | 0.2% ACE | 81545.00 | 672.92 | 706.38 | | 707.00 | 0.000496 | 6.60 | 13907.23 | 529.56 | 0.21 |
| Cibolo Creek | Reach 1 | 434453 | 1% ACE | 74844.00 | 672.90 | 701.08 | | 702.28 | 0.001688 | 9.93 | 10304.78 | 657.11 | 0.34 |
| Cibolo Creek | Reach 1 | 434453 | 0.2% ACE | 81545.00 | 672.90 | 705.67 | | 706.50 | 0.000994 | 8.46 | 13433.79 | 702.88 | 0.27 |
| | | | | | | | | | | | | | |
| Cibolo Creek | Reach 1 | 433730 | 1% ACE | 74844.00 | 668.74 | 700.47 | | 701.07 | 0.001006 | 7.16 | 14270.50 | 937.56 | 0.24 |
| Cibolo Creek | Reach 1 | 433730 | 0.2% ACE | 81545.00 | 668.74 | 705.38 | | 705.77 | 0.000555 | 5.93 | 19135.51 | 1044.01 | 0.18 |
| 011 | 5 | 400565 | 401 4 07 | | | | | | | | 10 | | |
| Cibolo Creek | Reach 1 | 433539 | 1% ACE | 74844.00 | 667.11 | 700.39 | | 700.85 | 0.000790 | 6.40 | 16157.71 | 1041.30 | 0.21 |
| Cibolo Creek | Reach 1 | 433539 | 0.2% ACE | 81545.00 | 667.11 | 705.34 | | 705.64 | 0.000430 | 5.26 | 21676.32 | 1150.69 | 0.16 |
| Cibolo Creek | Reach 1 | 433408 | 1% ACE | 74844.00 | 667.31 | 700.34 | | 700.73 | 0.000749 | 6.22 | 17384.43 | 1111.20 | 0.21 |
| Cibolo Creek | Reach 1 | 433408 | 0.2% ACE | 81545.00 | 667.31 | 705.32 | | 705.57 | 0.000394 | 5.03 | 23061.25 | 1358.07 | 0.21 |
| | | | | | | | | | | | | | |
| Cibolo Creek | Reach 1 | 433181 | 1% ACE | 86791.00 | 667.56 | 700.20 | | 700.53 | 0.000716 | 5.98 | 23132.56 | 1884.55 | 0.20 |
| CIDOIO CIEEK | | 433181 | 0.2% ACE | | | | | 705.44 | 0.000557 | 5.90 | 32834.44 | | 0.18 |

E.A. * ADAM W. MEHEVEC 11-30-22

| HEC-RAS Plan: | Updated Revis | ed Blocked Lo | cations: User D | Defined | | | | | | | | | | |
|------------------------------|--------------------|------------------|--------------------|------------------|---------------|------------------|--------------------|--------------------|----------------------|----------------------|-----------|--------------------|--------------------|-----------|
| River | Reach | River Sta | Profile | W.S. Elev | Prof Delta WS | E.G. Elev | Top Wdth Act | Q Left | Q Channel | Q Right | Enc Sta L | Ch Sta L | Ch Sta R | Enc Sta R |
| | | | | (ft) | (ft) | (ft) | (ft) | (cfs) | (cfs) | (cfs) | (ft) | (ft) | (ft) | (ft) |
| Cibolo Creek Cibolo Creek | Reach 1 Reach 1 | 446236 446236 | 1% ACE Floodway | 716.12 | 0.90 | 718.00 718.81 | 1951.03 1002.17 | 4900.10 5877.34 | 65683.06 64922.15 | 12970.84 12754.51 | 172.87 | 903.73 903.73 | 1087.06 1087.06 | 1175.04 |
| CIDDIO Creek | Reactin | 440230 | Floodway | /17.02 | 0.90 | / 10.01 | 1002.17 | 5677.54 | 04922.15 | 12/ 54.51 | 1/2.0/ | 903.73 | 1007.00 | 1175.04 |
| Cibolo Creek | Reach 1 | 446037 | 1% ACE | 716.14 | | 717.43 | 2171.55 | 4782.71 | 63702.82 | 15068.46 | | 943.50 | 1153.19 | |
| Cibolo Creek | Reach 1 | 446037 | Floodway | 716.69 | 0.55 | 718.38 | 454.83 | 777.42 | 70137.90 | 12638.68 | 929.35 | 943.50 | 1153.19 | 1384.18 |
| | | | | | | | | | | | | | | |
| Cibolo Creek | Reach 1 | 445573 | 1% ACE | 715.47 | | 716.64 | 1272.36 | 6390.85 | 57313.04 | 19850.11 | | 1349.41 | 1542.79 | |
| Cibolo Creek | Reach 1 | 445573 | Floodway | 716.32 | 0.85 | 717.45 | 555.54 | 6769.31 | 56620.63 | 20164.06 | 1201.92 | 1349.41 | 1542.79 | 1757.46 |
| Cibolo Creek | Reach 1 | 445235 | 1% ACE | 715.46 | | 716.09 | 819.21 | 10421.24 | 51523.95 | 12898.82 | | 1717.02 | 1956.28 | |
| Cibolo Creek | Reach 1 | 445235 | Floodway | 716.26 | 0.80 | 716.96 | 565.82 | 9028.64 | 54081.38 | 11733.98 | 1577.28 | 1717.02 | 1956.28 | 2143.10 |
| | | | í í | | | | | | | | | | | |
| Cibolo Creek | Reach 1 | 444777 | 1% ACE | 714.34 | | 715.55 | 418.29 | 2154.21 | 63308.85 | 9380.94 | | 2348.62 | 2577.53 | |
| Cibolo Creek | Reach 1 | 444777 | Floodway | 714.49 | 0.15 | 716.28 | 246.91 | | 73171.14 | 1672.86 | 2348.62 | 2348.62 | 2577.53 | 2595.53 |
| Cibolo Creek | Reach 1 | 444240 | 1% ACE | 712.59 | | 714.56 | 303.76 | 2666.21 | 67828.48 | 4349.30 | | 2814.71 | 3018.07 | |
| Cibolo Creek | Reach 1 Reach 1 | 444240 | Floodway | 712.59 | 0.75 | 714.56 | 303.76 | 2801.47 | 67618.69 | 4349.30 4423.84 | 0.00 | 2814.71 2814.71 | 3018.07 | 3300.15 |
| OIDOID OFCCK | Readin | 444240 | Tioodway | 110.00 | 0.15 | 110.13 | 500.52 | 2001.47 | 0/010.03 | 4420.04 | 0.00 | 2014.71 | 3010.07 | |
| Cibolo Creek | Reach 1 | 443555 | 1% ACE | 712.24 | | 713.19 | 424.81 | 1499.44 | 69577.54 | 3767.02 | | 2931.67 | 3262.25 | |
| Cibolo Creek | Reach 1 | 443555 | Floodway | 712.82 | 0.58 | 713.87 | 348.46 | | 73164.02 | 1679.99 | 2931.67 | 2931.67 | 3262.25 | 3280.13 |
| | | | | | | | | | | | | | | |
| Cibolo Creek | Reach 1 | 442891 | 1% ACE | 711.58 | 0.05 | 712.49 | 409.13 | 1348.93 | 72058.54 | 1436.54 | 0404.04 | 3204.30 | 3524.42 | 0540.05 |
| Cibolo Creek | Reach 1 | 442891 | Floodway | 712.23 | 0.65 | 713.12 | 365.04 | 1056.15 | 72652.52 | 1135.35 | 3181.31 | 3204.30 | 3524.42 | 3546.35 |
| Cibolo Creek | Reach 1 | 442214 | 1% ACE | 709.72 | | 711.43 | 548.33 | 787.75 | 51439.71 | 22616.54 | | 3677.07 | 3827.83 | |
| Cibolo Creek | Reach 1 | 442214 | Floodway | 710.23 | 0.52 | 712.04 | 461.28 | 101.10 | 52965.77 | 21878.23 | 3677.07 | 3677.07 | 3827.83 | 4138.35 |
| | | | , í | | | | | | | | | | | |
| Cibolo Creek | Reach 1 | 441476 | 1% ACE | 708.12 | | 709.76 | 421.93 | 966.24 | 69857.55 | 4020.21 | | 4342.78 | 4591.52 | |
| Cibolo Creek | Reach 1 | 441476 | Floodway | 708.47 | 0.35 | 710.20 | 288.58 | | 71677.22 | 3166.78 | 4342.78 | 4342.78 | 4591.52 | 4631.36 |
| Ollegia Organia | Desch 4 | 440700 | 40/ 405 | 705.04 | | 707.00 | 004.50 | 005.00 | 74054 70 | 0000.00 | | 4000.00 | 5000 50 | |
| Cibolo Creek Cibolo Creek | Reach 1 Reach 1 | 440762 440762 | 1% ACE Floodway | 705.81 706.45 | 0.65 | 707.89 708.42 | 304.53 306.91 | 365.99 396.81 | 71254.79 71160.34 | 3223.23 3286.85 | 0.00 | 4983.33 4983.33 | 5228.52 5228.52 | 5956.00 |
| CIDOID CICCI | Redon | 440702 | Tioodway | 100.40 | 0.05 | 100.42 | 500.51 | 000.01 | 71100.04 | 5200.05 | 0.00 | 4300.00 | 5220.52 | 0000.00 |
| Cibolo Creek | Reach 1 | 439971 | 1% ACE | 705.51 | | 705.71 | 1144.96 | 34854.49 | 38552.44 | 1437.07 | | 5578.80 | 5988.60 | |
| Cibolo Creek | Reach 1 | 439971 | Floodway | 706.20 | 0.69 | 706.39 | 1147.63 | 34986.38 | 38383.43 | 1474.19 | 0.00 | 5578.80 | 5988.60 | 6814.76 |
| | | | | | | | | | | | | | | |
| Cibolo Creek | Reach 1 | 438740 | 1% ACE | 705.30 | | 705.41 | 1844.11 | 44777.09 | 28058.68 | 2008.24 | | 6282.64 | 6619.35 | |
| Cibolo Creek | Reach 1 | 438740 | Floodway | 706.02 | 0.72 | 706.12 | 1847.61 | 45151.82 | 27671.04 | 2021.14 | 0.00 | 6282.64 | 6619.35 | 7054.13 |
| Cibolo Creek | Reach 1 | 437996 | 1% ACE | 705.21 | | 705.29 | 1824.69 | 51836.41 | 21598.66 | 1408.93 | | 6407.33 | 6675.95 | |
| Cibolo Creek | Reach 1 | 437996 | Floodway | 705.94 | 0.73 | 706.02 | 1827.73 | 52081.36 | 21343.22 | 1419.42 | 0.00 | 6407.33 | 6675.95 | 7062.49 |
| | | | | | | | | | | | | | | |
| Cibolo Creek | Reach 1 | 437265 | 1% ACE | 705.03 | | 705.18 | 1486.97 | 44260.34 | 30391.10 | 192.55 | | 6061.46 | 6357.85 | |
| Cibolo Creek | Reach 1 | 437265 | Floodway | 705.28 | 0.25 | 705.75 | 747.42 | 26180.06 | 48663.94 | | 5610.44 | 6061.46 | 6357.85 | 6357.85 |
| Cibolo Creek | Reach 1 | 436536 | 1% ACE | 704.27 | | 704.82 | 921.79 | 22511.71 | 52046.61 | 285.67 | | 5441.48 | 5719.48 | |
| Cibolo Creek | Reach 1 | 436536 | Floodway | 704.27 | 0.52 | 704.82 | 925.29 | 23063.72 | 51479.22 | 301.05 | 0.00 | 5441.48 | 5719.48 | 5951.68 |
| | | 100000 | rioounuy | 101110 | 0.02 | 100.00 | 020.20 | 20000.12 | 01110.22 | 001.00 | 0.00 | 0111.10 | 07.10.10 | 0001.00 |
| Cibolo Creek | Reach 1 | 435810 | 1% ACE | 703.05 | | 703.98 | 526.54 | 16563.79 | 58081.49 | 198.72 | | 4685.27 | 4939.04 | |
| Cibolo Creek | Reach 1 | 435810 | Floodway | 703.14 | 0.09 | 704.34 | 366.56 | 11157.48 | 63686.52 | | 4572.48 | 4685.27 | 4939.04 | 4939.04 |
| 011 1 0 1 | | 105010 | 101.105 | | | | | | | | | | | |
| Cibolo Creek Cibolo Creek | Reach 1 Reach 1 | 435043 435043 | 1% ACE Floodway | 702.40 | 0.08 | 703.12 703.20 | 513.44 467.01 | 4279.59 4203.83 | 68559.70 68716.49 | 2004.70 1923.67 | 3650.42 | 3712.57 3712.57 | 4066.13 4066.13 | 4117.43 |
| CIDDIO Creek | Reactin | 435043 | Floodway | 702.46 | 0.06 | 703.20 | 407.01 | 4203.03 | 667 10.49 | 1923.07 | 3030.42 | 3/12.3/ | 4000.13 | 4117.43 |
| Cibolo Creek | Reach 1 | 434453 | 1% ACE | 701.08 | | 702.28 | 657.11 | 9617.22 | 55027.95 | 10198.83 | | 3142.32 | 3348.79 | |
| Cibolo Creek | Reach 1 | 434453 | Floodway | 701.09 | 0.01 | 702.33 | 509.31 | 9406.53 | 55451.41 | 9986.06 | 2993.92 | 3142.32 | 3348.79 | 3503.24 |
| | | | | | | | | | | | | | | |
| Cibolo Creek | Reach 1 | 433730 | 1% ACE | 700.47 | | 701.07 | 937.56 | 14895.09 | 52078.04 | 7870.86 | | 2634.02 | 2896.74 | |
| Cibolo Creek | Reach 1 | 433730 | Floodway | 700.50 | 0.03 | 701.11 | 938.27 | 14923.74 | 52033.67 | 7886.59 | 0.00 | 2634.02 | 2896.74 | 3861.55 |
| Cibolo Creek | Reach 1 | 433539 | 1% ACE | 700.39 | | 700.85 | 1041.30 | 18641.81 | 48790.01 | 7412.17 | | 2235.56 | 2507.18 | |
| Cibolo Creek | Reach 1 Reach 1 | 433539 | Floodway | 700.39 | 0.04 | 700.85 | 1041.30 | 18684.49 | 48790.01 | 7412.17 7413.66 | 0.00 | 2235.56 | 2507.18 | 3619.57 |
| 5.00. | | | | 100.12 | 0.04 | , 00.00 | 10.2.00 | | . 57 10.00 | | 0.00 | | | 2010.07 |
| Cibolo Creek | Reach 1 | 433408 | 1% ACE | 700.34 | | 700.73 | 1111.20 | 25890.60 | 39223.45 | 9729.95 | | 2028.53 | 2253.30 | |
| Cibolo Creek | Reach 1 | 433408 | Floodway | 700.37 | 0.04 | 700.76 | 1111.26 | 25934.34 | 39175.76 | 9733.89 | 0.00 | 2028.53 | 2253.30 | 3444.80 |
| | - | | | | | | | | | | | | | |
| Cibolo Creek | Reach 1 | 433181 | 1% ACE | 700.20 | | 700.53 | 1884.55 | 36801.04 | 42484.07 | 7505.90 | | 1629.56 | 1890.52 | |
| Cibolo Creek | Reach 1 | 433181 | Floodway | 700.23 | 0.04 | 700.56 | 1885.10 | 36882.98 | 42402.05 | 7505.96 | 0.00 | 1629.56 | 1890.52 | 3197.20 |





FEMA PRODUCTION AND TECHNICAL SERVICES CONTRACTOR

September 1, 2022

Adam W. Mehevec, P.E. Civil and Environmental Consultants, Inc. 3711 South Mopac Expressway Building 1, Suite 550 Austin, TX 78745 IN REPLY REFER TO: Case No.: 22-06-2567P Communities: City of Schertz and Unincorporated Areas of Bexar County, Texas Community Nos.: 480269 and 480035

316-AD

Dear Adam Mehevec:

This is in regard to your request dated August 5, 2022, that the Department of Homeland Security's Federal Emergency Management Agency (FEMA) issue a revision to the Flood Insurance Rate Map (FIRM) for the above-referenced communities. Pertinent information about the request is listed below.

| Identifier: | Beck Landfill |
|----------------------|---------------|
| Flooding Source: | Cibolo Creek |
| FIRM Panel Affected: | 48187C0220F |

The data required to complete our review, which must be submitted within 90 days of the date of this letter, are listed on the attached summary.

If we do not receive the required data within 90 days, we will suspend our processing of your request. Any data submitted after 90 days will be treated as an original submittal and will be subject to all submittal/payment procedures.

FEMA receives a very large volume of requests and cannot maintain inactive requests for an indefinite period of time. Therefore, we are unable to grant extensions for the submission of required data/fee for revision requests. If a requester is informed by letter that additional data are required to complete our review of a request, the data **must** be submitted within 90 days of the date of the letter. Any fees already paid will be forfeited if the requested data are not received within 90 days.

If you have general questions about your request, FEMA policy, or the National Flood Insurance Program (NFIP), please contact the FEMA Mapping and Insurance eXchange (FMIX), toll free, at 1-877-FEMA MAP (1-877-336-2627). If you have specific questions concerning your request, please contact your case reviewer, M. Tariq Makhdoom, Ph.D., CFM, by e-mail at TMakhdoom@Taylorengineering.com or by telephone at (904) 553-5760, or the Revisions Coordinator for your state, Mr. Bosulu Lokulutu, E.I.T, CFM, by e-mail at bosulu.lokulutu@aecom.com or by telephone at (972) 735-7093.

Sincerely,

Benjamin Kaiser, P.E., CFM Revisions Manager Compass PTS JV

Attachments:

Summary of Additional Data Legal Notification Templates

cc: Dough Letbetter, CFM Floodplain Administrator City of Schertz, Texas

> Robert Brach Development Services Engineer / Floodplain Administrator Bexar County



FEMA PRODUCTION AND TECHNICAL SERVICES CONTRACTOR

Summary of Additional Data Required to Support a Letter of Map Revision (LOMR)

Case No.: 22-06-2567P

Requester: Adam W. Mehevec, P.E.

Communities: City of Schertz, and Unincorporated Areas of Bexar County, Texas

Community Nos.: 480269 and 480035

The issues listed below must be addressed before we can continue the review of your request.

- 1. From our review of the submitted annotated Flood Insurance Rate Map (FIRM), it appears that the Unincorporated Areas of Bexar County are also affected by this LOMR. Please submit a copy of MT-2 Application/Certification Form 1, entitled "Overview and Concurrence Form," where the second signature block has been signed by a Bexar County official (preferably the Floodplain Administrator). Alternatively, please provide documentation that the corporate limits shown on the FIRM are not accurate and Bexar County is not actually affected by this revision. Acceptable documentation includes a current corporate limits map provided by the community along with an annexation agreement, if applicable.
- 2. Our review revealed that the submittal does not include floodway analysis for the duplicate effective and as-built plan for Cibolo Creek. Please submit floodway analysis for Cibolo Creek. Please ensure that the surcharges do not exceed the 1.0-foot maximum allowed and there are no surcharges that are less than 0.0 feet. Also, please ensure that the encroachment stations are located in the flood fringe, the area between the channel banks and the boundary of the base floodplain.
- 3. The submitted topographic work map, entitled "Topographic Work Map Beck Landfill Expansion, 600 FM 78, Schertz, Texas 78154, Guadalupe County, Texas," prepared by Civil & Environmental Consultants, Inc., certified dated June 15, 2022, does not provide some of the essential information required to complete our review of this request. Please submit a revised topographic work map, certified by a registered Professional Engineer (P.E.), which shows all applicable items listed in Section C of Application/Certification Form 2, entitled "Riverine Hydrology and Hydraulics Form," including the following information. Please ensure that there is consistency between the work map, revised hydraulic model and the annotated FIRM.
 - a. Please show the boundary delineations of the revised conditions base 0.2-percent-annualchance floodplain, and regulatory floodway. The floodplain boundaries should generally follow the proposed contours and should be delineated to the elevations calculated in the revised conditions hydraulic model. It is helpful to use different colored lines as well as line types to distinguish the boundary delineations.
 - b. Please show smooth graphical tie-ins between the revised and effective flood hazard boundary delineations at the upstream and downstream ends of the revised reach. Please ensure that the revised delineations tie-in directly to the effective delineations and that the tie-ins occur a short distance upstream of the upstream most cross section in the revised conditions hydraulic model and a short distance downstream of the downstream most cross section, where there is a base flood elevation (BFE) tie-in between the revised and effective conditions. Please label tie-in locations.

- c. The work map does not seem to be created on the scale shown on the map. Please create the map on the scale shown on the work map and also indicate the scale (1 inch = x feet).
- d. In view of the above comment, we could not verify topwidths of the base floodplain, 0.2percent-annual-chance floodplain, and regulatory floodway, as shown on the abovereferenced work map. We could also not verify reach lengths between the revised cross section as shown on the above referenced work map.
- 4. Please provide a copy of the Geographic Information System (GIS) data that reflects the revised topographic work map. Please ensure the digital data are spatially referenced and cite what projection (coordinate system, example: Universal Transverse Mercator [UTM]/State Plane) was used, so that the data may be used for accurate mapping. The important data to show on the digital work map are the contour information, the stream centerline, the cross section lines, the road crossings and hydraulic structures, the preliminary and proposed flood hazard delineations, and the tie-in locations. Everything should be clearly labeled, and all information should be contained within the drawing and not externally referenced.

The submitted digital data must be spatially referenced and include what projection (coordinate system, e.g., UTM/State Plane) was used. The submitted digital data do not contain a projection and cannot be used for accurate mapping. Please resubmit Computed-Aided Design (CAD)/ GIS data that are correctly referenced and projected.

- 5. Based on any changes to the work map due to the resolution of the items at comment 4 above, please submit an updated annotated FIRM that shows the revised boundary delineations of the 1-percent-annual-chance (base) floodplain, 0.2-percent-annual-chance floodplain, and regulatory floodway as shown on the updated work map and how they tie-in to the boundary delineations shown on the effective FIRM at the downstream and upstream ends of the revised reach. Please use different colors to differentiate the proposed and effective boundary delineations. Also, please show the title block of the effective FIRM on the annotated FIRM.
- 6. Please submit a copy of the newspaper notice distributed by the City of Schertz and Bexar County stating their intent to revise the flood hazard information (i.e., revise or establish base flood elevations [BFEs], the base floodplain, and regulatory floodway) along Cibolo Creek. Alternatively, please submit documentation that individual legal notices were sent to all the property owners affected by any changes in the flood hazard information. Documentation of legal notice may take the form of a signed copy of the letter sent and either a mailing list or certified mailing receipts. Individual notices that are not sent on community letterhead must also include certification from the community that all affected property owners have been notified of the floodway revision. The newspaper notices or the individual legal notices must include the extent of revision and contact information for any interested parties and must also mention the community's intent to revise the regulatory floodway. **Please submit a draft copy of the notification for verification of content, prior to publication or distribution.** One of the attached templates may be used to prepare the draft notification.

Please note that the draft property owner notification or newspaper notification will be reviewed after the hydraulic model and work map are finalized. Please do not distribute the final notification until we have approved the draft notice. Please upload the required data using the Online LOMC website at https://hazards.fema.gov/femaportal/onlinelomc/signin.

For identification purposes, please include the case number referenced above on all correspondence.

MUNICIPAL SOLID WASTE PERMIT MAJOR AMENDMENT

PART III-ATTACHMENT C3 DRAINAGE SYSTEM PLANS AND DETAILS



NAME OF PROJECT: Beck Landfill MSW PERMIT APPLICATION NO.: 1848A OWNER: Nido, LTD (CN603075011) OPERATOR: Beck Landfill (RN102310968) CITY, COUNTY: Schertz, Guadalupe County Major Amendment: Revised September 2023

Prepared by:



Civil & Environmental Consultants, Inc.

Texas Registration Number F-38 3711 S MoPac Expressway Building 1 Suite 550, Austin, Texas 78746 (512) 329-0006

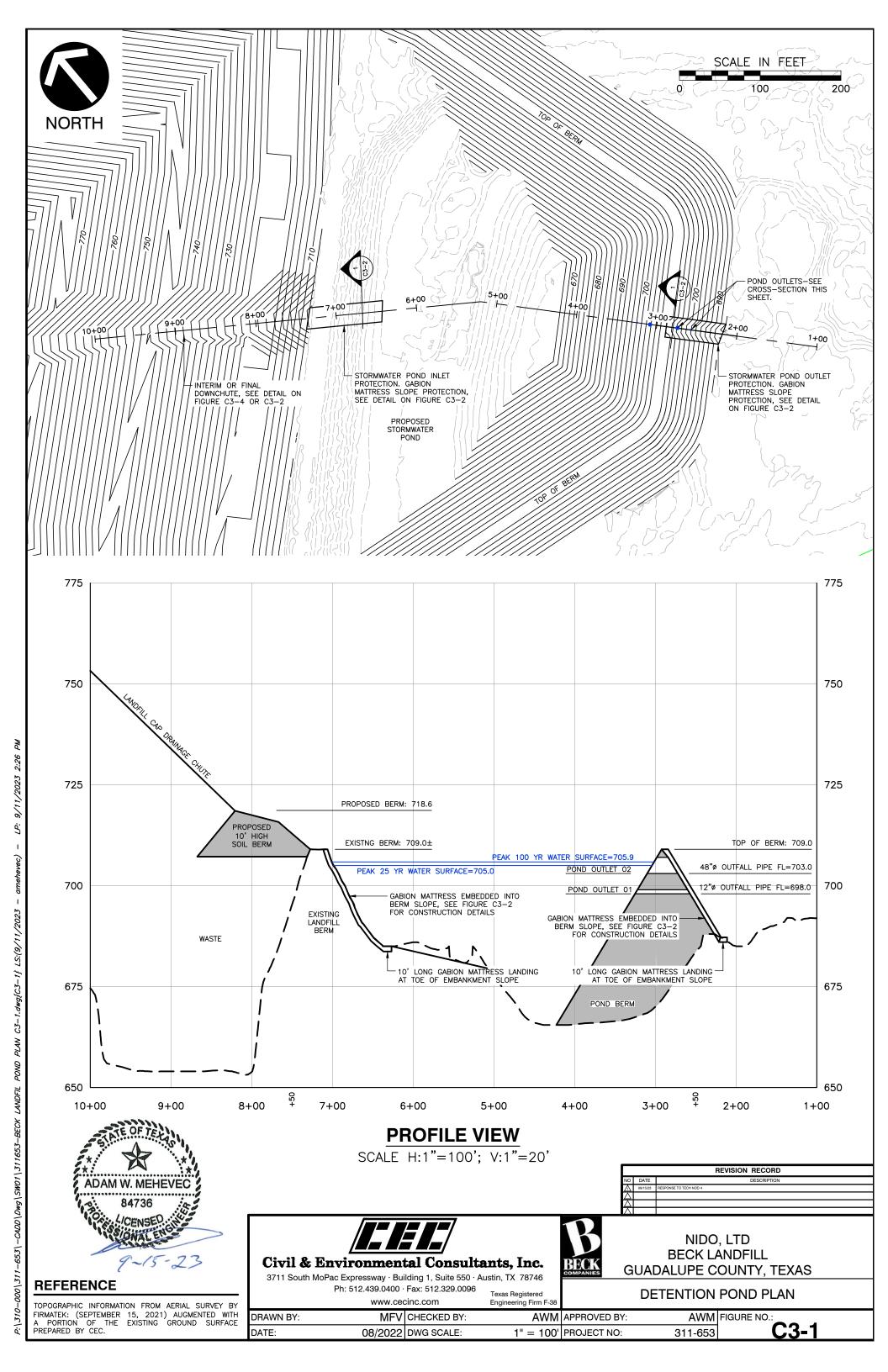


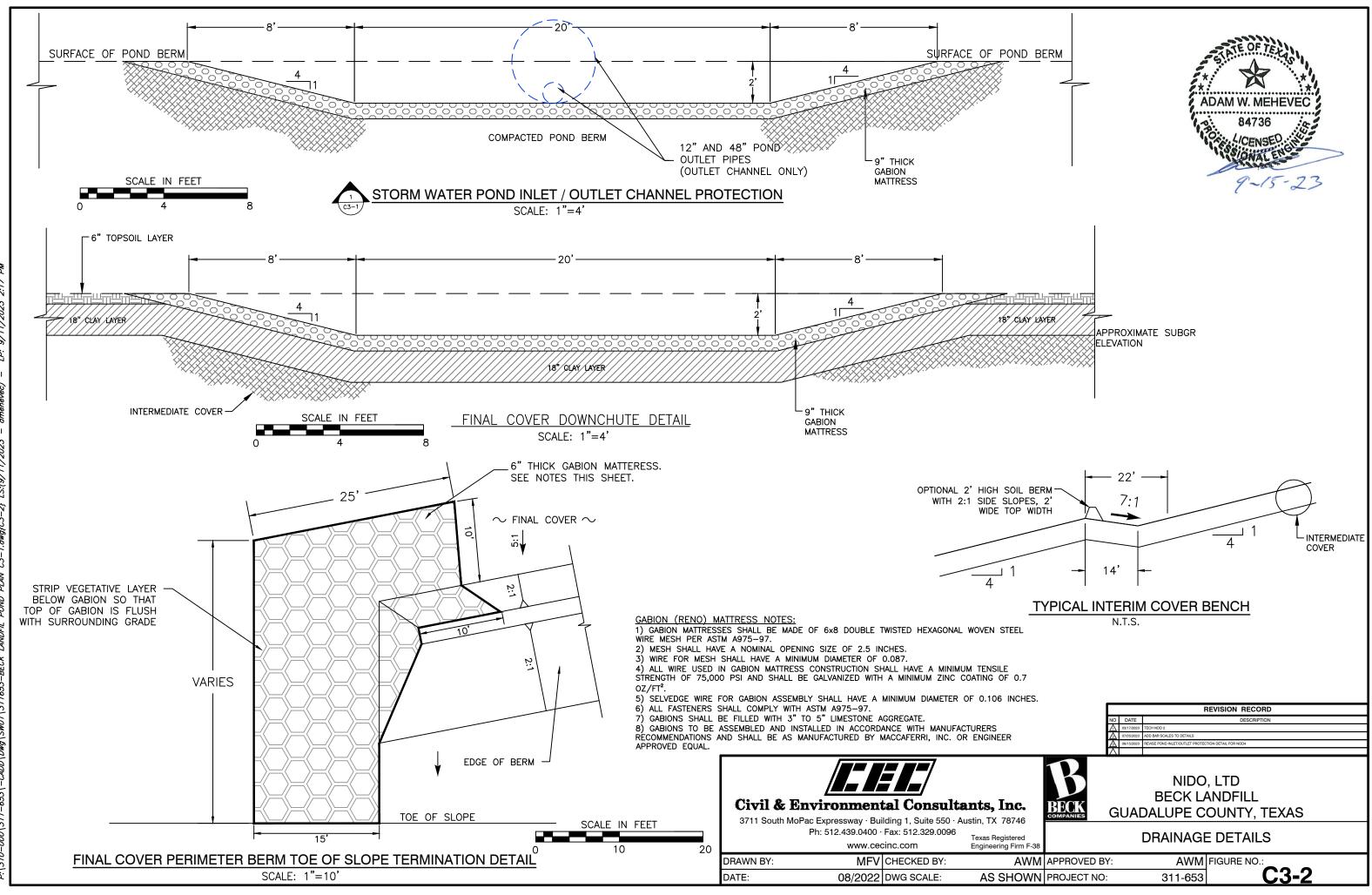
LIST OF FIGURES

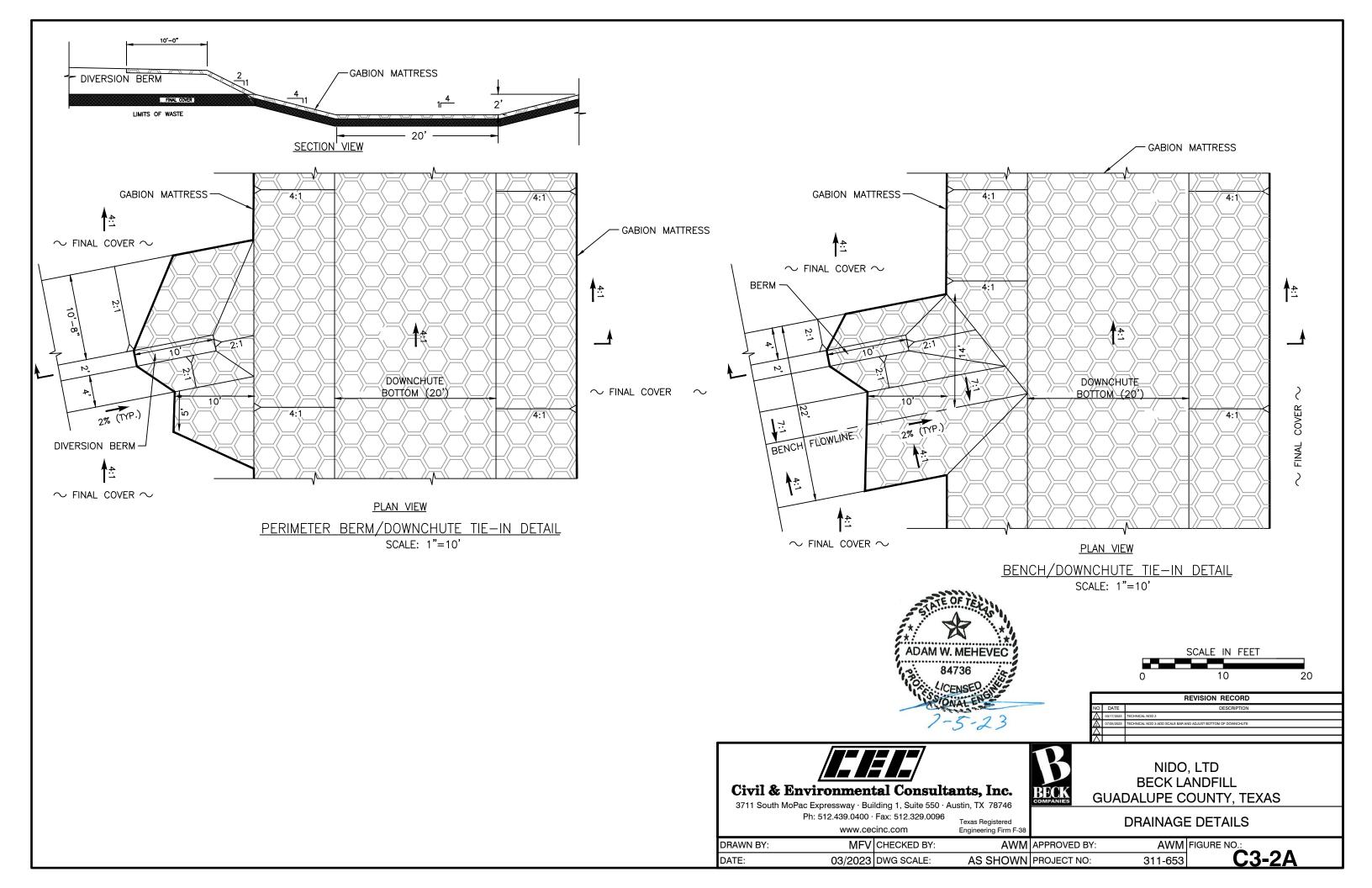
FIGURE C3-1DETENTION POND PLANFIGURE C3-2DRAINAGE DETAILSFIGURE C3-2ADRAINAGE DETAILSFIGURE C3-2BDRAINAGE DETAILSFIGURE C3-3DRAINAGE DETAILSFIGURE C3-4INTERIM DRAINAGE DETAILS

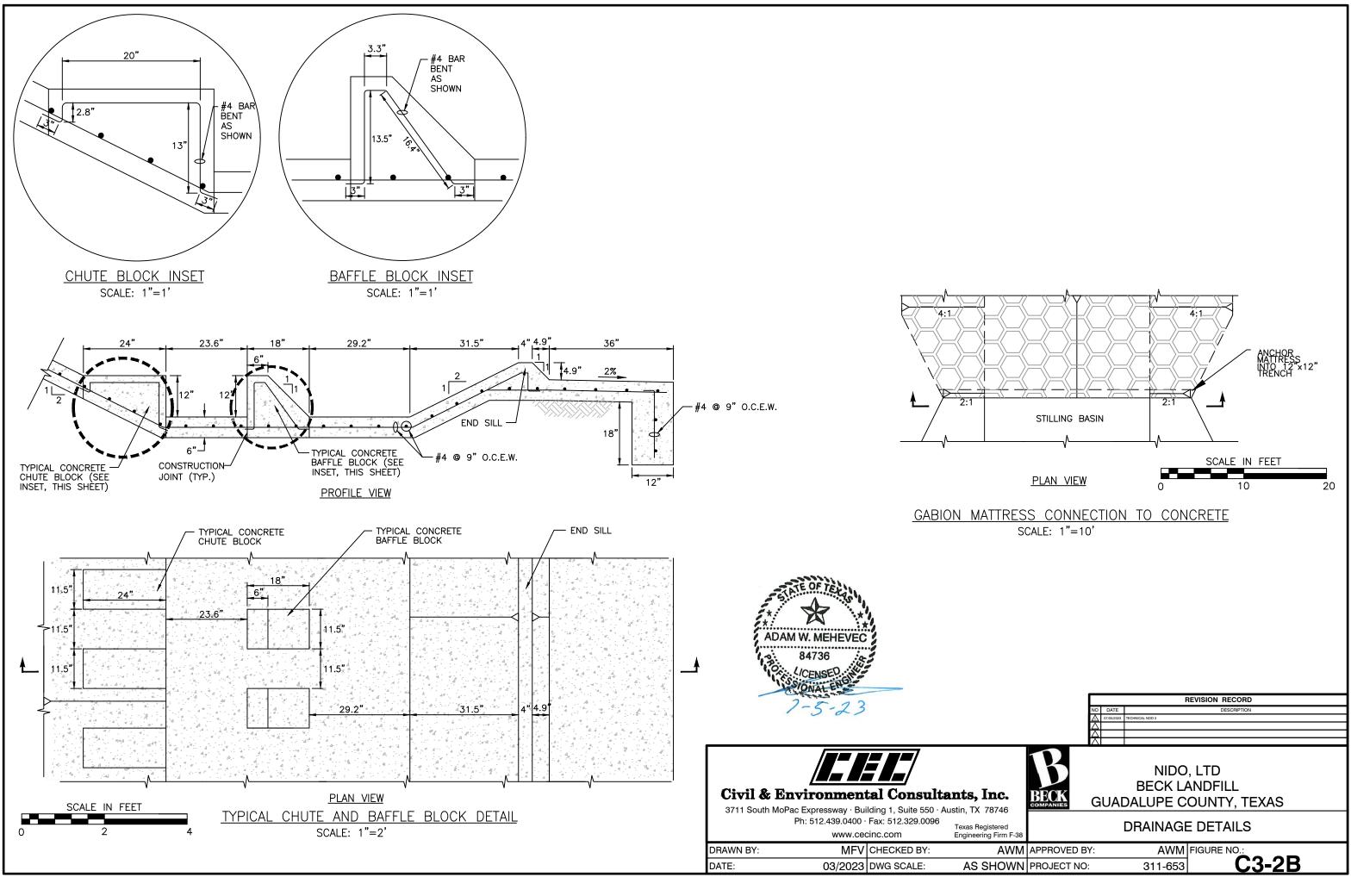


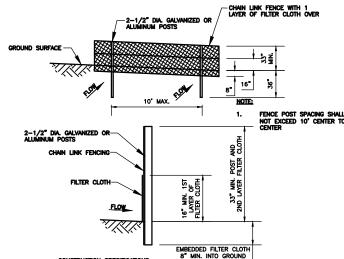
Beck Landfill Revised (9/23) Part III-Attachment C3











CONSTRUCTION SPECIFICATIONS

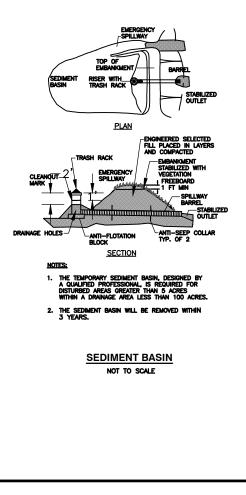
CHAIN LINK FENCING SHALL BE 42" IN HEIGHT. THE SPECIFICATION FOR A 6' FENCE SHALL BE USED SUBSTITUTING 42" FABRIC AND 6' LENGTH POSTS.

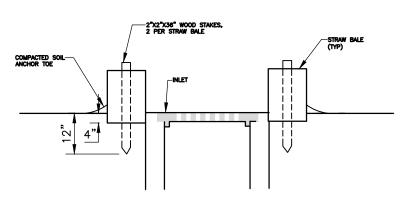
- THE POLES DO NOT NEED TO SET IN CONCRETE.
- CHAIN LINK FENCE SHALL BE FASTENED SECURELY TO THE FENCE POSTS WITH WIRE TIES OR STAPLES.
- ER CLOTH SHALL BE FASTENED SECURELY TO THE CHAIN LINK FENCE WITH TIES CED EVERY 24" AT THE TOP AND MID SECTION.
- FILTER CLOTH SHALL BE EMBEDDED A MINIMUM OF 8" INTO THE GROUND
- WHEN TWO SECTIONS OF FILTER CLOTH ADJOIN EACH OTHER, THEY SHALL BE OVERLAPPED BY 6" AND FOLDED. 5.
- MAINTENANCE SHALL BE PERFORMED AS NEEDED AND SILT BUILDUPS REMOVED WHEN "BULGES" DEVELOP IN THE SILT FENCE.

REFERENCE:

U.S. DEPARTMENT OF AGRICULTURE SOIL CONSERVATION SERVICE MARYLAND DEPARTMENT OF ENVIRONMENT WATER MANAGEMENT

SUPER SILT FENCE NOT TO SCALE

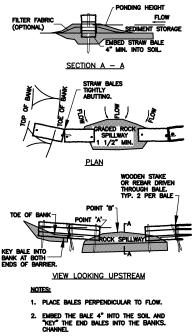




NOTES

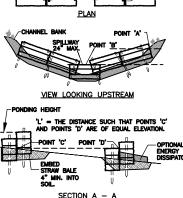
- PLACE STRAW BALES AROUND PERIMETER OF INLET. WEDGE LOOSE STRAW BETWEEN BALES AND PACK TIGHTLY.
- THE TOP OF THE BARRIER SHALL ENCIRCLE THE INLET AND BE LEVEL AND 2.
- L BE ANCHORED WITH MINIMUM 38-INCH LONG WOOI EXTEND 18 INCHES BELOW THE GROUND SURFACE. PRACTICAL THE CONTRACTOR SHALL THE THE BALES MOVEMENT OR OPENINGS IN THE BARRIER.
- HALL REPLACE THE STRAW BALES EVERY 3 MONTHS OR E BALES DETERIORATE AND BECOME INEFFECTIVE.
- HALL INSPECT THE STRAW BALES AFTER EVERY PRECIPITAT TRAW BALES SHALL BE RESET, STAKED AND BACKFILLED TRACTOR SHALL REPLACE ALL CLOGGED OR INOPERATIVE
- HALL REMOVE ACCUMULATED SEDIMENTS AS REQUIRED TU FUNCTIONAL. IN ALL CASES, THE CONTRACTOR SHALL THERE ACCUMULATIONS REACH ONE-THIRD THE ABOVE THE BARRIER.
- THE CONTRACTOR SHALL REPAIR ALL UNDERCUTTING AND EROSION OF THE ANCHOR TOE IMMEDIATELY WITH COMPACTED BACKFILL MATERIAL. 7.
- EXISTING CURB INLETS SHALL HAVE STRAW BALE BARRIERS PLACED BEHIND THE CURB. NO BARRIERS ARE TO BE PLACED ON THE ROADWAY.

STRAW BALE INLET PROTECTION NOT TO SCALE



- 3. BALES PLACED IN A ROW WITH ENDS TIGHTLY ABUTTING, USE STRAW, ROCKS OR FILTER FABRIC TO FILL ANY GAPS BETWEEN BALES AND TAMP BACKFILL MATERIALS TO PREVENT EROSION OR FLOW AROUND THE
- 4. POINT "A" SHALL BE HIGHER THAN POINT
- 5. SPILLWAY SHALL NOT EXCEED 24".

SEMI-PERVIOUS STRAW BALE SEDIMENT BARRIER NOT TO SCALE

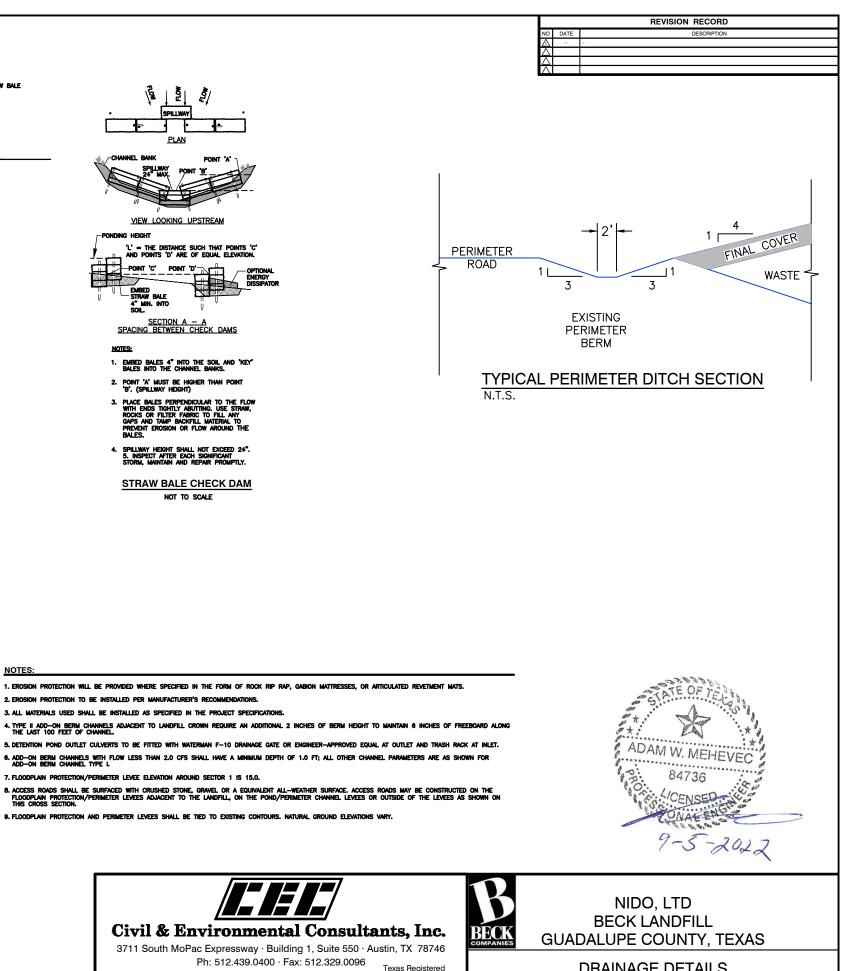


- THE

NOTES

1. EROSION PROTECTION WILL BE PROVIDED WHERE SPECIFIED IN THE FORM OF ROCK RIP RAP. GABION MATTRESSES, OR ARTICULATED REVETMENT MATS.

- 3. ALL MATERIALS USED SHALL BE INSTALLED AS SPECIFIED IN THE PROJECT SPECIFICATIONS.
- 5. DETENTION POND OUTLET CULVERTS TO BE FITTED WITH WATERMAN F-10 DRA
- 7. FLOODPLAIN PROTECTION/PERIMETER LEVEE ELEVATION AROUND SECTOR 1 IS 15.0.
- 9. FLOODPLAIN PROTECTION AND PERIMETER LEVEES SHALL BE TIED TO EXISTING CONTOURS. NATURAL GROUND ELEVATIONS VAR

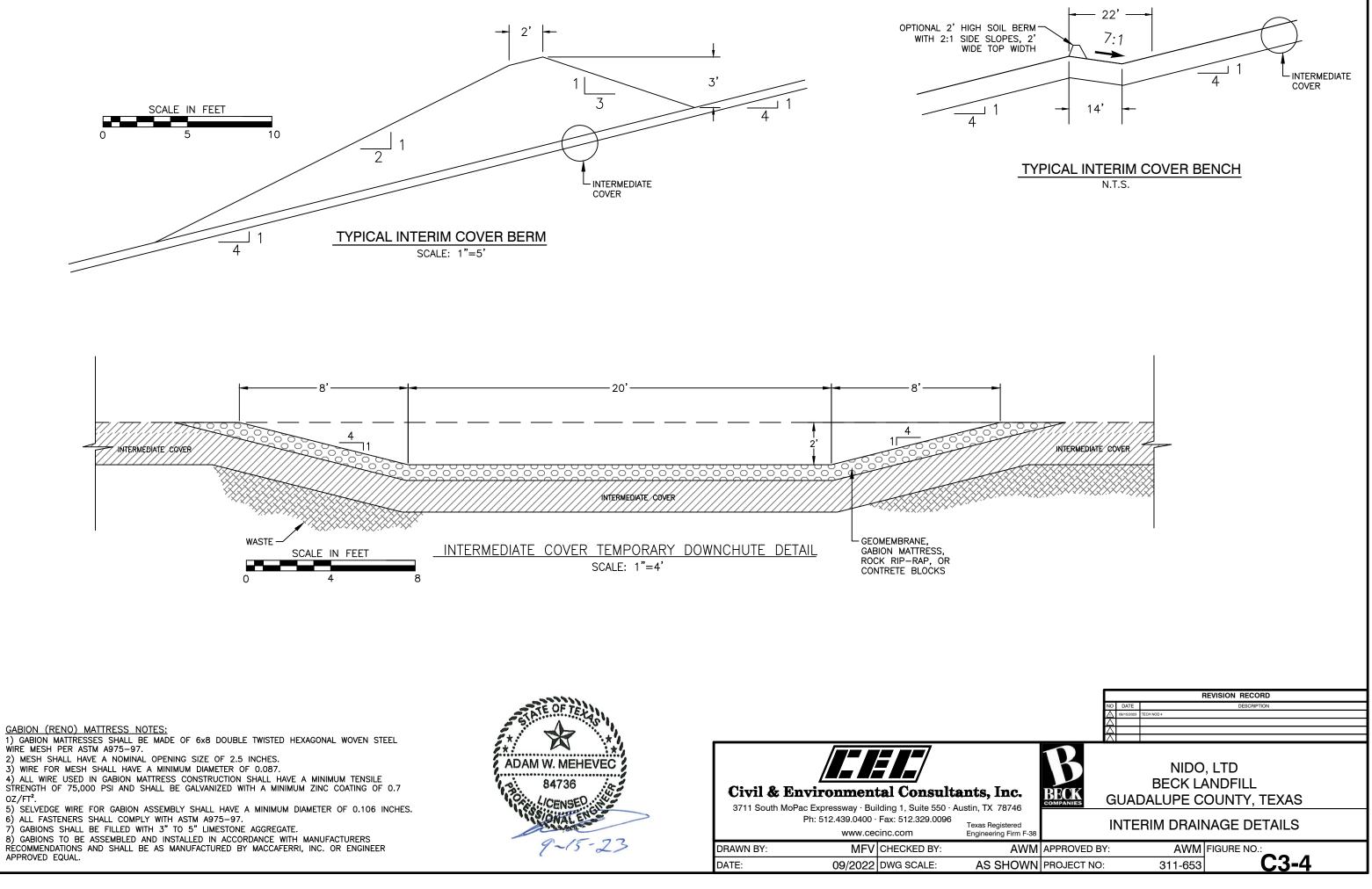


| | www.cecinc.com | | Texas Registered Engineering Firm F-38 |
|-----------|----------------|-------------|---|
| DRAWN BY: | MFV | CHECKED BY: | AWM |
| DATE: | 08/2022 | DWG SCALE: | AS SHOWN |

DRAINAGE DETAILS

WM APPROVED BY: OWN PROJECT NO:

AWM FIGURE NO .: **C3-3** 311-653



GABION (RENO) MATTRESS NOTES:

1) GABION MATTRESSES SHALL BE MADE OF 6x8 DOUBLE TWISTED HEXAGONAL WOVEN STEEL WIRE MESH PER ASTM A975-97. 2) MESH SHALL HAVE A NOMINAL OPENING SIZE OF 2.5 INCHES. 3) WIRE FOR MESH SHALL HAVE A MINIMUM DIAMETER OF 0.087.

OZ/FT². 5) SELVEDGE WIRE FOR GABION ASSEMBLY SHALL HAVE A MINIMUM DIAMETER OF 0.106 INCHES.

RÉCOMMENDATIONS AND SHALL BE AS MANUFACTURED BY MACCAFERRI, INC. OR ENGINEER

APPROVED EQUAL.

